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FILE: ENG.EGEO03422-01.012
Via Email: paul.lach@edmonton.ca

Attention: Dr. Paul R. Lach, Ph.D., P.Eng.

Subject: Preliminary Geotechnical Assessment Report
North Shore Promenade
River Bank between Walterdale Bridge and Groat Road Bridge, Edmonton, Alberta

1.0 INTRODUCTION

Tetra Tech Canada Inc. (Tetra Tech) was retained by the City of Edmonton (COE) to provide geotechnical engineering services for the Touch The Water Promenade (TTWP) and North Shore Promenade (NSP) projects. The Request for Proposal (RFP) for the geotechnical services of TTWP and NSP was received from the COE on August 30, 2018. The detailed scope of services was described in a proposal issued on September 19, 2018 (Reference No. PENG.EGEO03422-01) in response to the RFP from COE. Authorization to proceed with this work was provided on October 31, 2018 by Dr. Paul Lach, P.Eng. of COE under Reference Code C#4000003242 Line # 1 and 2.

As part of the work scope of the initial stage, Tetra Tech conducted a preliminary geotechnical assessment for the project areas. The work included a review of existing available borehole data, published geological information, historical aerial photographs, and records of existing structures relevant to the geotechnical aspects of the site, site reconnaissance and the preparation of this preliminary geotechnical assessment report. The objective of the preliminary geotechnical report is to summarize the collected relevant information, interpret the geological setting, and identify the geotechnical constraints and hazards.

This report presents the findings of Tetra Tech's preliminary geotechnical assessment for the NSP area and is subject to the limitations on the use of this report attached in Appendix A. The preliminary geotechnical assessment report for the TTWP is provided separately.

Figure 1 shows the study area and the proposed locations of the TTWP and NSP Projects at the time of the proposal. Based on direction from the COE, two retaining walls located north of River Valley Road between the High Level Bridge and the Legislature Power Plant should be added to the NSP Project. The additional area where these two retaining walls are located is shown on Figure 1.

2.0 PROJECT BACKGROUND

The NSP Project aims to create an iconic public space along the north shore of the river bank of the North Saskatchewan River, between the Walterdale Bridge and about 250 m west of Groat Road Bridge in Edmonton, Alberta. Based on information provided by the COE, the NSP project limits consist of a narrow strip of land between the top of the river bank where an existing paved walking trail is located and the toe of the river bank at the river level. The total length of the NSP area is approximately 2.9 km.

The west end of the area is at the west side of the existing Groat Road Bridge which is undergoing rehabilitation works. The east end of the project area is connected to the newly constructed trail at the north abutment of the Walterdale Bridge. The area north of the existing trail is bounded by the existing River Valley Road. The project area is bounded by the North Saskatchewan River along the south side. The exposed shoreline area will change at different times of the year based on the variable water level and flow in the river.

Preliminary information available from the COE shows that the promenade may include terraces, walkways and viewing decks within the proposed site area.

A meeting was held with the COE, the design team and Tetra Tech on July 29, 2019 to discuss the preliminary geotechnical issues and concerns of the TTWP and NSP projects. Based on these discussions, it is understood the design team and the COE are still at the early stage of the design development. The locations of the proposed walkways and viewing decks are yet to be determined and will go through public consultations in early 2020. Tetra Tech was requested to proceed with the preliminary geotechnical assessment report without specific details of the proposed developments.

3.0 DESKTOP STUDY

Tetra Tech has conducted a detailed desktop review of the existing available borehole data, current and historical aerial photographs, LIDAR survey and published geological maps. The following sections summarize the findings from the desktop study for the NSP area.

3.1 Geological Review

Tetra Tech conducted a search of published geological maps for the site area. A publication titled Urban Geology of Edmonton prepared by C.P. Kathol and R.A McPherson, under Bulletin 32 of the Alberta Research Council, dated 1975, provided a variety of surficial and bedrock information.

Based on Surficial Geological Map of Edmonton (Figure 23 of Bulletin 32), the surficial geology near the west end of the project area, around the Groat Road Bridge, and near the east end of the project area, west of Walterdale Bridge, is described as gully, creek valley and scarp materials, which consist of thin colluvium, thin alluvium, and mixed glacial and bedrock materials. The central portion of the project area is mainly river terrace deposits comprising alluvial gravel, sand and silt from the North Saskatchewan River. The Geological Section No.15 on Figure 26 of Bulletin 32 crosses the project area and the stratigraphy indicates approximately 6 m of alluvium originating from river terrace and flood plain deposits consisting of clay, silt and gravel, underlain by bedrock.

According to the Bedrock Topography Map on Figure 20 of Bulletin 32, the top of the bedrock near the project area is at an approximate elevation of 616 m. The bedrock is part of the Edmonton Formation which consists of interbedded bentonitic shales and sandstones with numerous coal seams.

3.2 Aerial Photo Review

Aerial photographs of varying scales were obtained from the COE library spanning a period from 1978 to 2009 at an approximate interval of 10 years. The last aerial photograph is at a scale of 1:20,000 and was taken in 2014.

The aerial photographs are presented on Figures 3 to 7, appended to this report.

The primary purpose of reviewing the aerial photographs was to determine locations of any discernible river bank instabilities, caused by either construction or erosion of the shoreline.

The following key points have been identified from the review:

- For the portion of the North Saskatchewan River where the proposed NSP project is located, the flow in the river is generally from west to east. The shoreline near the Groat Road bridge is located on the outside bend of the river and more susceptible to river erosion impacts. The shoreline from Victoria Golf course to Royal Glenora Club is a moderate inside bend and deposition of river deposits has occurred along the toe of the bank slope leading to shallow deposits and formation of a sand bar that are apparent on aerial photographs. From Royal Glenora Club to the Walterdale Bridge, the river bank is on a gradual outside bend and deposition along the shoreline for this portion is apparently less;
- The aerial photographs showed changes between 1978 and 1982 for the Government House Park area west of the Groat Road Bridge and the Groat Road Bridge North Abutment, and through to 1997. This area was also the east end of the MacKinnon Ravine Freeway development project which began in late 1960's with tree clearing within the MacKinnon Ravine. Fill was end dumped off the river bank as part of the earthworks for the freeway. However, the MacKinnon Freeway development project was terminated in early 1970's. The freeway was never built, and the area has become a multi-use trail and park area;
- The multi-use trail along River Valley Road east of Groat Road Bridge extended to the entrance of Victoria Park Golf Course by 1978, and was linked to the MacKinnon Ravine trail commencing from Government House Park as mentioned above between 1982 and 1997;
- The outfall locations as presented on Figure 2 are not readily visible from the aerial photographs except for what appears to be evidence of significant discharge near Outfall #175 and #176 in 1978;
- Erosion mitigation using rip rap protection is evident in the 2014 aerial photograph near Outfall #33;
- Localized bank erosion downstream from outfall locations can be expected during significant discharge events;
- Works for the construction of the new Walterdale Bridge began in 2013 and are evident in the 2014 photograph, and;
- There are currently ongoing construction changes as part of the Groat Road Bridge Rehabilitation Project. Observations made during site reconnaissance are presented in Section 5.0 of this report.

3.3 Existing Report Review

Tetra Tech reviewed 35 reports obtained from the COE Engineering Services Library, adjacent to the NSP subject site. Many of these reports either did not contain boreholes, had illegible site plans and/or no coordinate or borehole location information, and many were significantly north of the Top of Bank (TOB). Seven reports provided both site plans and relevant geotechnical boreholes close to the TOB and for the additional area east of the High Level Bridge.

The above noted seven reports are listed on Table 1, appended to this report, and excerpts from these reports have also been presented in Appendix B. The project locations and associated boreholes are shown on Figure 8. Several other reports utilize this information, and a full list of the 35 reports is shown in Table 2, appended to this report.

In general, the subsurface conditions from TOB consist of fills underlain by fluvial deposits, overlying bedrock of the Edmonton Formation. The thickness of the fills and fluvial deposits typically range between 1 m and 7 m, and the bedrock is expected to be encountered below these surficial deposits at an approximate elevation of 616 m (with variance of a couple metres based on the boreholes closest to the TOB). Top of bedrock generally increases in elevation based on boreholes north of River Valley Road and east of the High Level Bridge. The subsurface conditions described in the previous applicable seven reports are summarized below. All depths are in metres below existing ground surface on the terrace lands unless stated otherwise.

3.3.1 Project Number 931-36-16-01 322 (Borehole T85-N4, N5, N7 and R1)

This geotechnical report was completed in 1985 for the South Light Rail Transit (SLRT) Extension Phase II project. The following borehole information near the river bank was extracted and would be relevant at corresponding locations near the existing SLRT Bridge.

Borehole T85-N4 was drilled at the TOB and indicated a clay fill layer extending to 1.8 m overlaid sand and silt to approximately 11.6 m (elevation 613.1 m), underlain by very weak bedrock to the termination depth of 24 m. The bedrock comprised claystone interbedded with sandstone, siltstone and bentonitic layers. A 200 mm thick bentonite layer was encountered at approximately 605.9 m.

Groundwater was recorded at 12.6 m within the bedrock and is approximated to be at an elevation of 612.1 m.

Borehole T85-R1 was drilled near river level and indicated bedrock at an elevation of 612 m underlying a 2 m thick gravel layer.

Based on the request to include the retaining walls north of the River Valley Road east of the High Level Bridge, T85-N5 and T85-N7 had also been included in Appendix B and Figure 8.

Borehole T85-N5 was located close mid-height of the slope between River Valley Road and Fortway Drive. The borehole log indicated fill to approximately 3 m below grade (elevation of 620.2 m), underlain by clay, silt, and clay till to an approximate elevation of 617.5 m where it encountered claystone bedrock. The borehole was terminated at 10.4 m below grade.

Borehole T85-N7 was located close to Fortway Drive and indicated clay fill from ground surface to 7 m below grade. The clay fill was underlain by claystone. The borehole was terminated at 21 m. Ground elevation was not provided for this borehole.

3.3.2 Project Number 931-36-16-18 1816 (Borehole 87-1 to 87-5)

This geotechnical investigation report was completed in 1987 for a portion of the River Valley Road between High Level Bridge and 105 Street. These boreholes were drilled east of the High Level Bridge, north of the River Valley Road, south of Fortway Drive, and on the east side and west side of the Legislature Power Plant. Surficial deposits comprising fill, clay, sand and gravel are encountered from surface to depths between 1.5 m and 5 m. Bedrock was encountered from an approximate elevation between 631 and 635 m. Groundwater level readings taken a month after drilling completion varied between elevations of 629 m and 623 m. Original ground varied between elevations 638 m and 634 m along the roadway alignment. No recovery zones were encountered in all boreholes at elevation between 626 m to 633 m. Slope inclinometers were installed in Boreholes 87-2, 87-4 and 87-5. The report also provided information for existing inclinometers and past instability at an area approximately 50 m east of the High Level Bridge and south of Fortway Drive (Inclinometer TILT115). Some of the existing monitoring readings indicated movements occurred at approximately 8.8 m below grade.

3.3.3 Project Number 931-36-16-24 6141 (Borehole 10-01)

This report was completed in 2011 for a slope Inclinometer installation on Fortway Drive east of the High Level Bridge. This borehole was drilled on Fortway Drive, situated immediately east of the High Level Bridge to replace an existing inclinometer (SI110) that was destroyed. Previous inclinometer readings indicated movement at approximately 5 m below existing grade. The ground elevation of Borehole 10-01 was 642.6 m, which was about 15 m above River Valley Road. Clay fill underlying asphalt extended to approximately 3.5 m (or elevation of 639 m). Bedrock from the Edmonton Formation underlies the fill, and extended to the termination depth of the borehole of 21.4 m (elevation 621.2 m).

3.3.4 Project Number 934-32-02-23 5585 (Borehole 09-11 to 09-13)

The geotechnical report was completed for the Government House Park in 2010 located west of Groat Road and Groat Road Bridge North Abutment. The boreholes located near the river bank encountered topsoil or asphalt at the surface, underlain by surficial fill (clay and/or gravel) that extended up to a depth of 2.1 m. The fill was underlain by native clay, silt and sand, overlying hard clay shale bedrock. The bedrock was encountered at depths of 6.7 m to 7.0 m (at an approximate elevation of 618.2 m to 619.7 m). Groundwater was noted at 617 m to 619.8 m near the top of the bedrock.

3.3.5 Project Number 934-32-02-57 8838 (Borehole 16-2)

This is a 2017 report for the Groat Road Bridge Rehabilitation Project. Although it was an Environmental Impact Assessment, it was appended with a geotechnical investigation report completed in 2016. Borehole 16-2 is located immediately east of the Groat Road Bridge North Abutment. Topsoil was encountered at surface, underlain by clay extended to an approximate elevation of 620.2 m, which overlaid gravel to 615 m. Bedrock which underlied the gravel was described as very hard, and the groundwater level was measured at an elevation of 618 m, approximately one month after completion of drilling.

3.3.6 Project Number 931-36-16-02 367 (Borehole T88-N25 and T88-N26)

This is a monitoring report for the SLRT Phase II completed in 1992. Two additional inclinometers were found in this report east of the existing SLRT Bridge, north of River Valley Road and south of Fortway Drive which is close to the additional area requested by COE. In Borehole T88-N25, gravel fill was encountered at surface underlain by sand that extended to an approximate elevation of 614.9 m, where claystone bedrock was encountered. The borehole was terminated at 32 m below grade. An inclinometer was installed in this borehole. In Borehole T88-N26, clay fill was encountered at the ground surface and was underlain by sand to about 615.0 m. Sand was underlain by clay till to 614.4 m where siltstone bedrock was encountered. Borehole was terminated at 24.6 m below grade. Thin bentonite seam was encountered approximately at elevation of 612.6 m. A vibrating wire piezometer was installed in this borehole.

3.3.7 Project Number 19-598-370 (Borehole TH12-14)

This geotechnical investigation was completed in 2013 for the Walterdale Bridge Replacement Project. One borehole located west of the north abutment of the new Walterdale Bridge Project was found relevant to the NSP Project. Topsoil and clay fill was encountered from the surface to an approximate elevation of 625.4 m, overlying silt fill to elevation of 624.6 m, overlying silt to 618.1 m, and gravel and sand with some clay to 616.3 m. Clay shale was encountered at 616.3 m, with occasional sandstone layers, to the termination depth of the borehole at 603.2 m. Groundwater was recorded at elevation 616 m, measured approximately one month after drilling completion.

3.4 Existing Timber Retaining Wall West of Legislature Power Plant

In addition to the reports described in Section 3.3, photo records of a timber retaining wall (or timber parapet wall) located west of the Legislature Power Plant provided by COE are also presented in Appendix B. Based on the photo records, the timber retaining wall height was highest in the middle and lower at the east and west ends. The wall height varied from 0.5 m to 1.4 m above the trail elevation. Since the top of the wall was higher than the soil retained behind, the maximum retained soil height was in the order of 0.3 m to 0.8 m. The depth of embedment and foundation type were unknown.

Based on observations made by COE in 2017, the wall appeared to be a timber retaining wall structure. The portion of the wall exposed above grade appeared to be in relatively good condition, other than a pronounced lean of the

wall to the south. No advanced rot or broken timbers were observed at the time of the site inspection. The eastern and western ends showed very little lean. The major lean was situated in the middle portion of the wall. There were signs of accumulated run off and snow retention behind the wall that might have contributed to the leaning. According to COE, existing geotechnical instrumentations located approximately 50 m west and 150 m east of the wall had showed signs of a deep-seated instability in the past, but had not exhibited further movement since approximately 1996 to 2000. Based on field review, the portion of the slope behind the wall might have exhibited a slow and shallow creep movement. In general, the wall condition appeared to be in a usable state but should be reviewed and confirmed by a structural engineer. Long-term maintenance and/or visual inspection were recommended.

4.0 SUBSURFACE DATA GAP

Figure 8 shows the locations of existing boreholes from the seven applicable previous reports discussed in Section 3.3.

Tetra Tech conducted a geotechnical investigation at the Royal Glenora Club in 2008. The locations of the three boreholes are also shown on Figure 8. Based on these boreholes, in general the bedrock was encountered at an elevation from 615 m, underlying clay and silt from surface. Groundwater level measurements were recorded at elevations ranging from 612 m to 617 m.

Tetra Tech double checked the reports available from COE Engineering Services Library and confirmed that there was no additional monitoring stations found between Groat Road Bridge and LRT Bridge along the TOB in the existing reports or observed on site.

The most significant investigative data gap identified was the lack of geotechnical information along the TOB between Groat Road Bridge and the LRT Bridge, and along the shoreline for the entire NSP project extent. There is no current access route to allow drilling equipment to reach or work on the shoreline. However, the locations of the geotechnical investigations and the required access will depend on the types and locations of the promenade structures proposed by the project team. If drilling close to the shoreline is required, cut lines or benches may be formed to allow cleared paths or work areas to locations closer to the river. The locations of these cut lines and benches may coincide with the future accesses to the proposed promenade structures to minimize disturbance to the existing river bank slope and existing trees.

If drilling along the river's edge is considered critical, another option would involve drilling in the winter and include constructing an ice bridge at Emily Murphy Park near the south abutment of the Groat Road bridge. This would allow the drill to traverse the river and then travel along the river's edge supported by grounded shore ice.

Access to and drilling at the edge of the river would be difficult and very costly. The most cost effective approach at this stage would be to drill boreholes near the TOB. This will involve some cutting of trees, however, it is likely that the stratigraphy at the TOB and river edge will not vary greatly.

5.0 SITE RECONNAISSANCE

Tetra Tech conducted a site reconnaissance of the TTWP project area on November 14, 2018. During the site visit, the weather conditions were partly cloudy and -1 °C in the morning and 1 °C in the afternoon. Most of the ground surface was clear, although some of the ground surface was lightly covered by snow. The following summarized the key observations made during the site reconnaissance:

- There are outfalls at various locations along the project area. According to a drawing provided by COE, there should be 15 outfalls along the riverbank between Groat Road Bridge and Walterdale Bridge. During the site visit, some of the outlet pipes of the outfalls were visible but some were not. The position outlet points of the

outfalls varied and some of them were at mid-height of the river bank slope as shown on Photo 1. Gullies and eroded channels were formed below the outlet pipes on the river bank slope surface (Photo 2). The exception is Outfall No. 33 which is located about 280 m west of the High Level Bridge. The area downstream of the pipe at Outfall No. 33 was protected by riprap (Photo 3);

- The first northern pier of Groat Road Bridge was located at the slope toe of the river bank slope (Photo 4). The bridge structure spanned over the multiuse trail and River Valley Road, and was supported on the north abutment of the Groat Road Bridge. At the time of the site visit, construction work for a rehabilitation project of Groat Road Bridge and River Valley Road was in progress;
- On the east side of the Groat Road Bridge, the existing multi-use trail was supported on a gabion wall. The gabion wall was located near the top of the river bank slope and was covered in heavy vegetation (Photo 5). The length and dimensions of the gabion wall were uncertain, and the wall was estimated to be approximately 1.5 m high and 100 m in length;
- There were four existing viewing areas along the multi-use trail at the top of the river bank slope at approximately 190 m, 240 m, 280 m and 320 m east of the Groat Road Bridge. These viewing areas were generally level graded surfaces at the approximate elevation of the multi-use trail (Photos 6 and 7). The river bank slope supporting or immediately next to the viewing areas was relatively steep locally and was estimated to be around 1 Horizontal to 1 Vertical (i.e. 1H:1V) as shown on Photo 8.
- In general, the river bank slope angle between Groat Road Bridge to Walterdale Bridge varied between approximately 2H:1V and 3H:1V;
- At various locations along the river bank slope from about 100 m east of Groat Road Bridge North Abutment to approximately the access road of Victoria Golf Course, large blocks of broken concrete were observed at mid-slope (Photos 9 and 10). Large blocks of concrete were observed close to river level from east of High Level Bridge to about 105 Street and were likely used as erosion protection (Photos 11, 12 and 13). Other portions of the river bank slope that were heavily vegetated and not accessible at the time during site reconnaissance may also have large blocks of broken concrete on the slope surface;
- Towards the east side of the project limits and about 720 m west of the Walterdale Bridge, there is a Light Rail Transit (LRT) bridge across the North Saskatchewan River. The LRT bridge pier was located on the river bank slope. Adjacent to this LRT bridge pier was a spiral ramp leading to the footbridge underneath the LRT bridge. The spiral ramp structure was supported on multiple piers (Photos 14 and 15);
- About 70 m east of the LRT Bridge is the High Level Bridge. The bridge pier of the High Level Bridge was located near the top of the river bank slope (Photo 16). A concrete retaining wall is located at the toe of the slope between River Valley Road and Fortway Drive as shown on Photo 16 immediately east of High Level Bridge. The maximum wall height of this retaining wall is about 4 m. The west end of the retaining wall is below the High Level Bridge and the east end of the retaining wall is about 100 m east of the High Level Bridge. The existing report mentioned in Section 3.3.2 (Project no. 931-36-16-18 1816) recommended a pile wall with tie-back anchors near this location;
- At the east end of the project area, the existing paved trail connects to the newly constructed retaining wall and trail of the Walterdale Bridge (Photo 17). The retaining wall was approximately 2 m in height. The headslope of the Walterdale Bridge North Abutment was protected with rip rap armouring (Photo 18), and;
- Evidence of a major slope failure was not observed during the site visit. Minor cracks were observed on the paved trails occasionally that may be associated with creep slope movement. Active erosion was observed along the river bank slopes at several locations with exposed tree roots as shown in Photo 19.

6.0 GEOHAZARDS AND CONCERNS

Based on the information collected in this preliminary geotechnical assessment report, the following potential geohazards and concerns have been identified at the NSP project area. These geohazards and concerns may not

become a significantly adverse issue for the project depending on the final locations and extents of the proposed developments.

- At the west end of the project area, any new development must take into account or be integrated with the existing pier of the Groat Road Bridge. The proposed foundations of the promenade should not affect or be affected by the existing foundation, based on a geotechnical evaluation
- At the Groat Road Bridge, the updated records of the ongoing road and bridge rehabilitation works should be reviewed and evaluated as existing structures may have been altered due to the rehabilitation works.
- If the existing gabion wall east of Groat Road Bridge is to remain after the rehabilitation works, and it is part of the promenade development, then a geotechnical evaluation should be conducted to investigate the area and to check for stability. Potentially, upgrading work or stabilization work might be required as part of the NSP development.
- The steep slopes below the existing viewing areas should be investigated and checked for stability and stabilization requirements.
- If fill construction is proposed along the toe of the riverbank, some form of stabilization such as geogrid reinforcement supplemented by erosion protection measures, such as rip rap armouring, will be required to provide stability and erosion protection.
- The proposed foundation of the promenade must not affect or be affected by the existing piers and associated headslope area of the LRT Bridge, ramp structure of the existing pedestrian footbridge, and the High Level Bridge, based on a geotechnical evaluation.
- If the proposed development requires new structures to be constructed along the river bank slope crest or slope toe, additional geotechnical investigation should be conducted to obtain geotechnical design parameters. Currently, there is no access to the river bank slope toe for drilling rigs and there is no work area along the river bank slope toe. Depending on the type and location of the proposed promenade structures, drilling from the top of the bank to obtain geotechnical information for deep foundation design may potentially be an alternative to forming cut lines on the existing river bank slope.
- Significant quantities of concrete blocks or fragments placed as part of historical bank erosion protection measures may obstruct future geotechnical investigations and any proposed development. The presence of these existing large pieces of concrete, including buried pieces, should be addressed in the construction contract. It will be important to recognize that this concrete debris is likely providing significant erosion protection for the existing riverbank and therefore would be of benefit to leave in place.
- If the bottom of the river bank along the project area is to be investigated, multiple access locations using cut lines or benches may be necessary to provide drill rig access to the slope toe or mid-slope areas. If these access locations can be planned such that they are at the same locations of the future public access routes to the new development at river level, it would reduce the amount of tree clearing and disturbance to the river bank. All of these investigative requirements are an important consideration for future geotechnical work and must be evaluated based on information to be provided concerning the proposed development.
- Eroded slope surfaces and unstable slopes along the river bank should be reviewed to determine whether slope stabilization works are required to improve public safety if the new development is to provide public access to the slope toe area at the river level.
- Many portions of the lower slopes are eroded with very steep or almost vertical slopes. Construction of a trail near the river level will result in excavation of the river bank that will likely require some type of stabilization measures (such as soil nails or anchors) above the proposed trail.
- Unstable trees, impacted by river erosion, may require removal as part of the permanent design if they are close to the proposed promenade due to public safety.

- Where existing outfall structures discharge on the middle or upper portion of the river bank, these outlets may need to be extended down to river level. For outfalls that exit close to river level, it would be advisable to raise the elevation of the promenade to be founded above the outfalls. Additional erosion protection and stabilization measures may be required where development is planned near the outfall locations.
- The new NSP development design must not adversely affect the stability of the newly constructed headslope, retaining wall and abutment foundations of the Walterdale Bridge, based on a geotechnical evaluation.
- The slope area east of the High Level Bridge, west of the Legislature Power Plant, north of the River Valley Road currently and south of Fortway Drive has two existing retaining walls where slope movement has occurred in the past. The cause of the movement may be due to deep-seated failure along existing weak bentonite seams. If the NSP Project includes proposed structures on this slope surface, the design must incorporate and mitigate the short-term and long-term stability of the slope. Methods to integrate, modify or reconstruct the existing retaining walls may be needed.
- Existing fill was encountered in many of the existing boreholes. The extent and depths of the existing fill should be investigated based on the proposed promenade locations.

7.0 SUMMARY

Based on the review data and findings presented in this preliminary geotechnical assessment report, the proposed promenade development is considered geotechnically feasible provided that the geotechnical constraints and concerns presented in this report are appropriately addressed. These geotechnical constraints and concerns include bank slope stability, existing and proposed foundations and structures, long-term erosion, and presence of existing fill. Other factors that require further geotechnical investigation include deep seated instability and other unexpected obstructions. The detailed geotechnical investigations and evaluations should be based on the locations of the proposed promenade structures. At the time of this report, the proposed designs are still under development. Once the proposed design has been determined, a review of the locations and the types of geotechnical foundations required to support the proposed designs should be conducted and a geotechnical evaluation should be planned and implemented accordingly.

It is understood hydrogeology, archeology and environmental engineering support will be provided by the design team. It is expected that other hazards such as flood mitigation, presence of historic artifacts, former coal mines, past land use impacts and other environmental issues such as contaminations will be addressed by the design team.

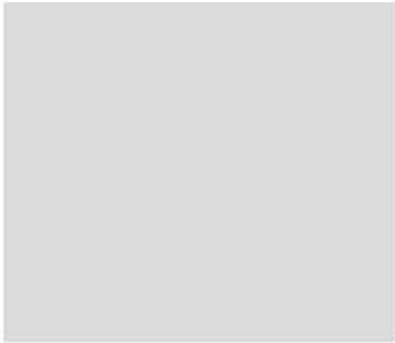
8.0 LIMITATIONS OF REPORT

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9.0 CLOSURE

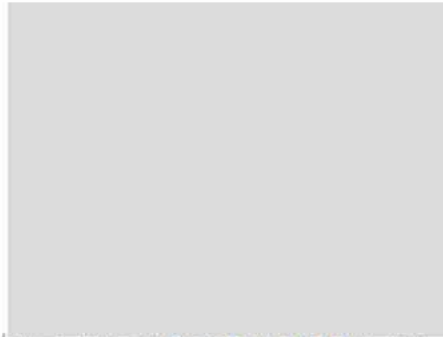
We trust this document meets your present requirements. If you have any questions or comments, please contact the undersigned.

Tetra Tech Canada Inc.



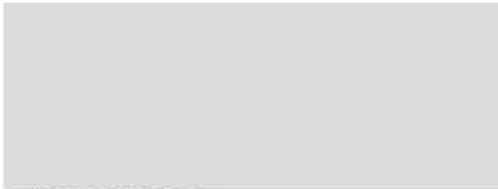
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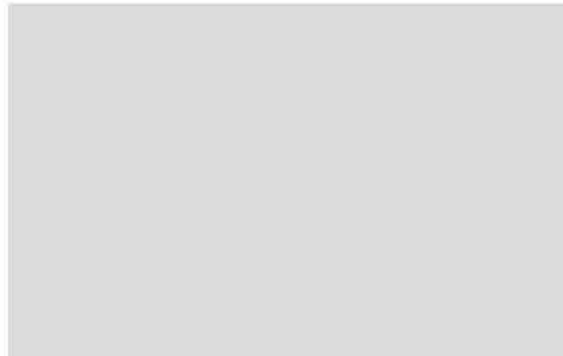
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TABLES

Table 1	Existing Reports as Presented on Figure 8
Table 2	List of Reviewed Reports

Table 1 – Existing Reports as presented on Figure 8

City of Edmonton Accession Number or Report Number	Author	Title	Date
931-36-16-01 322	Thurber Consultants Ltd.	South Light Rail Transit Extension Phase II, North River Bank to University Station, Subsurface Conditions from Station 301+070 to 302+560, Geotechnical Report No. 1, Volume 1 & Volume 2	August 1985
931-36-16-02 367	Thurber Consultants Ltd.	South Light Rail Transit Extension - Phase II, North Valley Slope and Portal Area, Slope Stability and Monitoring Summary	August 1985
931-36-16-18 1816	Thurber Consultants Ltd.	River Valley Road Upgrading, Geotechnical Investigation	May 1997
934-32-02-23 5585	City of Edmonton, Engineering Services	Proposed Groat Surface Wetland Geotechnical Investigation Government House Park Southwest of Groat Road at Victoria Park Road	February 2010
931-36-16-24 6141	City of Edmonton, Engineering Services	Slope Inclinator Installation - Fortway Drive near 109 Street, East of the High Level Bridge	February 2011
934-32-02-57 8838	Spencer Environmental Management Services Ltd	Groat Road Bridges Rehabilitation Project, Roadworks at Groat Road Interchange, Environmental Impact Assessment- Draft Report	March 2017
Thurber Report #: 19-598-370	Thurber Consultants Ltd.	Walterdale Bridge Replacement Edmonton, Alberta, Geotechnical Investigation	January 2013

Table 2 – List of Reviewed Reports

City of Edmonton Accession Number or Report Number	Author	Title	Date
931-32-21-11 8503	EPCOR	EPCOR Distribution & Transmission Inc., River Valley Splice Repair	December 2014
931-36-16-01 322 Volume 1 & 2 *	Thurber Consultants Ltd.	South Light Rail Transit Extension Phase II, North River Bank to University Station, Subsurface Conditions from Station 301+070 to 302+560, Geotechnical Report No. 1, Volume 1 & Volume 2	August 1985
931-36-16-02 367 *	Thurber Consultants Ltd.	South Light Rail Transit Extension - Phase II, North Valley Slope and Portal Area, Slope Stability and Monitoring Summary	April 1992
931-36-16-03 2385	Kipen Gibbs Landscape Architects Ltd.	High Level Bridge Rehabilitation, Environmental Screening Report	September 1994
931-36-16-05 636	Thurber Consultants Ltd.	South Light Rail Transit - Phase II Geotechnical Evaluation - North Portal, Geotechnical Report No. 8	April 1997
931-36-16-06 617	Thurber Consultants Ltd.	SLRT Extension - Phase II, North River Bank to University Station, North Valley Slope Stability Analysis Geotechnical Report No. 4	January 1996
931-36-16-07 616	Thurber Consultants Ltd.	South Light Rail Transit Extension - Phase II North Valley Slope and Portal Area - Supplementary Geotechnical Evaluation	March 1989
931-36-16-08 1338	City of Edmonton, Materials & Testing	Slope Indicator / Standpipe Installation Fortway Drive December 1978, July 1979, September 1980, April 1983, November 1985	December 1993
931-36-16-09 1406	City of Edmonton, Materials & Testing	Subsoil Investigation of the River Road East of the High Level Bridge	October 1965
931-36-16-11 1583	R.M. Hardy & Associates Ltd.	Soils Report RE: Proposed Hill-Side Road, 97 Avenue and 110 Street to Riverside Road	May 1959

City of Edmonton Accession Number or Report Number	Author	Title	Date
931-36-16-16 1802	City of Edmonton, Materials & Testing	Government Centre Generating Plant Seepage in Slope South	December 1974
931-36-16-17 1804	Thurber Consultants Ltd.	River Valley Road	July 1987
931-36-16-18 1816 *	Thurber Consultants Ltd.	River Valley Road Upgrading, Geotechnical Investigation	May 1987
931-36-16-19 1884	Thurber Consultants Ltd.	Fortway Drive Relocation, Stability Evaluation and Recommendations	August 1986
931-36-16-22 321	Hardy BBT Ltd.	Repairs to existing instability, 109 Street North of Walterdale Hill Road - Volume 1	December 1987
931-36-16-24 6141 *	City of Edmonton, Engineering Services	Slope Inclinator Installation - Fortway Drive near 109 Street, East of the High Level Bridge	February 2011
931-36-16-33 6435	Stantec Consulting Ltd.	Outfall 33 Revitalization and Repair, Environmental Screening Report, Edmonton, Alberta	August 2011
931-36-16-34 6458	Stantec Consulting Ltd.	Outfall 33 Revitalization and Repair, Environmental Screening Report, Edmonton, Alberta	August 2011
931-36-16-37 6505	Stantec Consulting Ltd.	Outfall 33 Revitalization and Repair, Environmental Screening Report, Edmonton, Alberta (Revised)	September 2011
931-36-25-03 118	Hardy Associates (1978) Ltd.	Stage II Interim Geotechnical Report South LRT Extension Corona Station to the North Bank of the North Saskatchewan River	October 1985
931-36-25-09 5084	EBA Engineering Consultants Ltd.	Phase I Environmental Site Assessment, 11160 River Valley Road, Blocks B and C, Plan 445MC, Edmonton, Alberta	September 2008

City of Edmonton Accession Number or Report Number	Author	Title	Date
931-36-25-10 1613	Hardy Associates (1978) Ltd.	Interim Engineering Report for Large Diameter Hole (LDH-I) Investigation, 110 Street, South of 97 Avenue	March 1986
931-36-25-11 5085	EBA Engineering Consultants Ltd.	Royal Glenora Club - Redevelopment Plan 2008, Environmental Screening Report	October 2008
931-36-25-14 1764	Thurber Consultants Ltd.	SLRT Phase II, North Portal Instrumentation	January 1991
931-36-25-15 1761	Thurber Consultants Ltd.	South Light Rail Transit Extension Phase II North Tunnel Instrumentation and Monitoring, Grandin Station to Crossover Cavity, Instrumentation Report No. 2	July 1988
931-36-25-20 1785	Thurber Consultants Ltd.	South Light Rail Transit (SLRT) - Phase II, North Portal Substation, Temporary/Permanent Retaining Wall (14-31-54)	August 1988
931-36-25-23 1837	R.M. Hardy & Associates Ltd.	Soils Report, Proposed Hillside Road, 97 Avenue and 110 Street to Riverside Road	April 1959
934-32-02-14 1704	EBA Engineering Consultants Ltd.	Proposed Space Sciences Centre Government Hill Site, Edmonton, Alberta (Includes Addendum No. 1 of August 1981)	June 1981
934-32-02-23 5585 *	City of Edmonton, Engineering Services	Proposed Groat Surface Wetland Geotechnical Investigation Government House Park Southwest of Groat Road at Victoria Park Road	February 2010
934-32-02-42 7151	CT & Associates Engineering Inc.	Geotechnical Evaluation, Victoria Promenade, Shallow Slope Failure Rehabilitation, Viewpoint at 100 Avenue and 121 Street, Edmonton, Alberta	November 2012
934-32-02-56 8837	Spencer Environmental Management Services Ltd.	Site Location Study for Groat Road Bridges Rehabilitation Project: Roadworks at Groat Road Interchange Draft Report	March 2017

City of Edmonton Accession Number or Report Number	Author	Title	Date
934-32-02-57 8838 *	Spencer Environmental Management Services Ltd	Groat Road Bridges Rehabilitation Project, Roadworks at Groat Road Interchange, Environmental Impact Assessment- Draft Report	March 2017
934-32-02-59 8983	Spencer Environmental Management Services Ltd.	Groat Road Bridges Rehabilitation Project: Groat Road Bridge over North Saskatchewan River (B059), Groat Road Bridge over Victoria Park Road (B060) and Emily Murphy Park Road Bridge over Groat Road (B099) Environmental Impact Assessment- Draft Report	April 2017
934-32-02-61 9294	CT & Associates Engineering Inc.	DIGITAL COPY ONLY: Geotechnical Investigation, Victoria Golf Course Renewal, 12030 River Valley Road NW, Edmonton, Alberta	April 2018
Thurber File #: 19-598-370 *	Thurber Consultants Ltd.	Walterdale Bridge Replacement Edmonton, Alberta, Geotechnical Investigation	January 2013

Note: * One of the seven reports summarized in Section 3.3, Table 1, and Figure 8

FIGURES

Figure 1	Site Location Plan
Figure 2	NSP Outfall location
Figure 3	Aerial Photograph 1978
Figure 4	Aerial Photograph 1982
Figure 5	Aerial Photograph 1997
Figure 6	Aerial Photograph 2009
Figure 7	Aerial Photograph 2014
Figure 8	Existing Borehole Locations for NSP



NOTE:
 1. THE ABOVE LAYOUT PLAN WAS EXTRACTED FROM CITY OF EDMONTON WEB SITE.
 2. ADDITIONAL AREA TO BE INCLUDED FOR NORTH SHORE PROMENADE BASED ON EMAIL ON SEPTEMBER 11, 2019

CLIENT:

CITY OF EDMONTON



**TOUCH THE WATER AND NORTH SHORE
 PROMENADE PROJECT, EDMONTON, AB**

SITE LOCATION PLAN

PROJECT: ENG.EGEO03422-01	DGN: TT	RVW: TR	PMT: AO	REV: 1
OFFICE: EDMONTON	DATE: SEPTEMBER 2019			

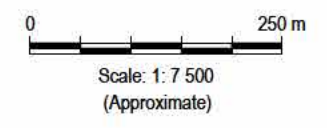
FIGURE 1

Q:\Edmonton\Drafting\PROJECTS\704-ENG-EGEO\ENG-EGEO\03422-01-Rossdale\01203_Aerial\ENG-EGEO\03422-01-012\Figure 2_NSP.dwg [FIGURE 2] August 16, 2019 - 1:05:34 pm (BY: DAS, DEBASIS)



LEGEND:
 ● - OUTFALL LOCATION

NOTE:
 BASE IMAGE IS TAKEN FROM GOOGLE EARTH
 IMAGERY YEAR: AUGUST 2017



CLIENT



**NORTH SHORE PROMENADE
 EDMONTON, ALBERTA**



OUTFALL LOCATIONS

PROJECT NO. ENG.EGEO03422.01.012	DWN DBD	CKD KJ	REV 0
OFFICE EDM	DATE August 2019		

Figure 2



LEGEND

From City of Edmonton Library

NOTES

STATUS
FOR INTERNAL USE ONLY

CLIENT



**NORTH SHORE PROMENADE
EDMONTON, ALBERTA**

**AERIAL PHOTOGRAPH
1978**

PROJECT NO. ENG EGEO03422-01	DWN	CKD	APVD	REV
OFFICE EBA-EDM	DATE August 15, 2019	KJ		

Figure 3



LEGEND

From City of Edmonton Library

NOTES

STATUS
FOR INTERNAL USE ONLY

CLIENT



**NORTH SHORE PROMENADE
EDMONTON, ALBERTA**

**AERIAL PHOTOGRAPH
1982**

PROJECT NO. ENG EGEO03422-01	DWN	CKD	APVD	REV
OFFICE EBA-EDM	DATE August 15, 2019	KJ		

Figure 4



LEGEND

From City of Edmonton Library

NOTES
SCALE 1:5,000

STATUS
FOR INTERNAL USE ONLY

CLIENT



**NORTH SHORE PROMENADE
EDMONTON, ALBERTA**

**AERIAL PHOTOGRAPH
1997**

PROJECT NO. ENG EGEO03422-01	DWN KJ	CKD	APVD	REV
OFFICE EBA-EDM	DATE August 15, 2019			

Figure 5



LEGEND

From City of Edmonton Library

NOTES
SCALE 1:5,000

STATUS
FOR INTERNAL USE ONLY

CLIENT



**NORTH SHORE PROMENADE
EDMONTON, ALBERTA**

**AERIAL PHOTOGRAPH
2009**

PROJECT NO. ENG EGEO03422-01	DWN	CKD	APVD	REV
OFFICE EBA-EDM	DATE August 15, 2019	KJ		

Figure 6



LEGEND

From City of Edmonton Library

NOTES
SCALE 1:20,000

STATUS
FOR INTERNAL USE ONLY

CLIENT



**NORTH SHORE PROMENADE
EDMONTON, ALBERTA**

**AERIAL PHOTOGRAPH
2014**

PROJECT NO. ENG EGEO03422-01	DWN	CKD	APVD	REV
OFFICE EBA-EDM	DATE August 15, 2019	KJ		

Figure 7

C:\Edmonton\Drafting\PROJECTS\704-ENG-EGEO\ENG-EGEO03422-01-012\Figure 8_NSP_Rev 1.dwg [FIGURE 8] October 02, 2019 - 9:53:04 am (BY: DAS, DEBASIS)



- LEGEND:**
- - BOREHOLE LOCATION (PROJECT 322)
 - - BOREHOLE LOCATION (PROJECT 367)
 - - BOREHOLE LOCATION (PROJECT 1816)
 - - BOREHOLE LOCATION (PROJECT 5585)
 - - BOREHOLE LOCATION (PROJECT 6141)
 - - BOREHOLE LOCATION (PROJECT 8838)
 - - BOREHOLE LOCATION (PROJECT 598-370)
 - - BOREHOLE LOCATION (EBA PROJECT - ROYAL GLENORA CLUB)

NOTE:
 BASE IMAGE IS TAKEN FROM GOOGLE EARTH
 IMAGERY YEAR: AUGUST 2017

0 250 m

Scale: 1: 7 500
 (Approximate)

CLIENT 		NORTH SHORE PROMENADE EDMONTON, ALBERTA		
		EXISTING BOREHOLE LOCATIONS FOR NSP		
PROJECT NO. ENG.EGEO03422.01.012	DWN DBD	CKD KJ	REV 1	Figure 8
OFFICE EDM	DATE September 2019			



Photo 1: Outfall 178 at Mid-height of River Bank Slope



Photo 2: Outfall 33 with Rip Rap Protection



Photo 3: Eroded Channel on River Bank Slope



Photo 4: Groat Road Bridge Pier at Slope Toe



Photo 5: Existing Buried Gabion Wall at Top of River Bank Slope



Photo 6: Existing Viewing Areas



Photo 7: Existing Viewing Areas



Photo 8: Steep Slope in Front of Viewing Areas



Photo 9: Large Concrete Blocks on River Bank Slope



Photo 10: Large Concrete Blocks on River Bank Slope

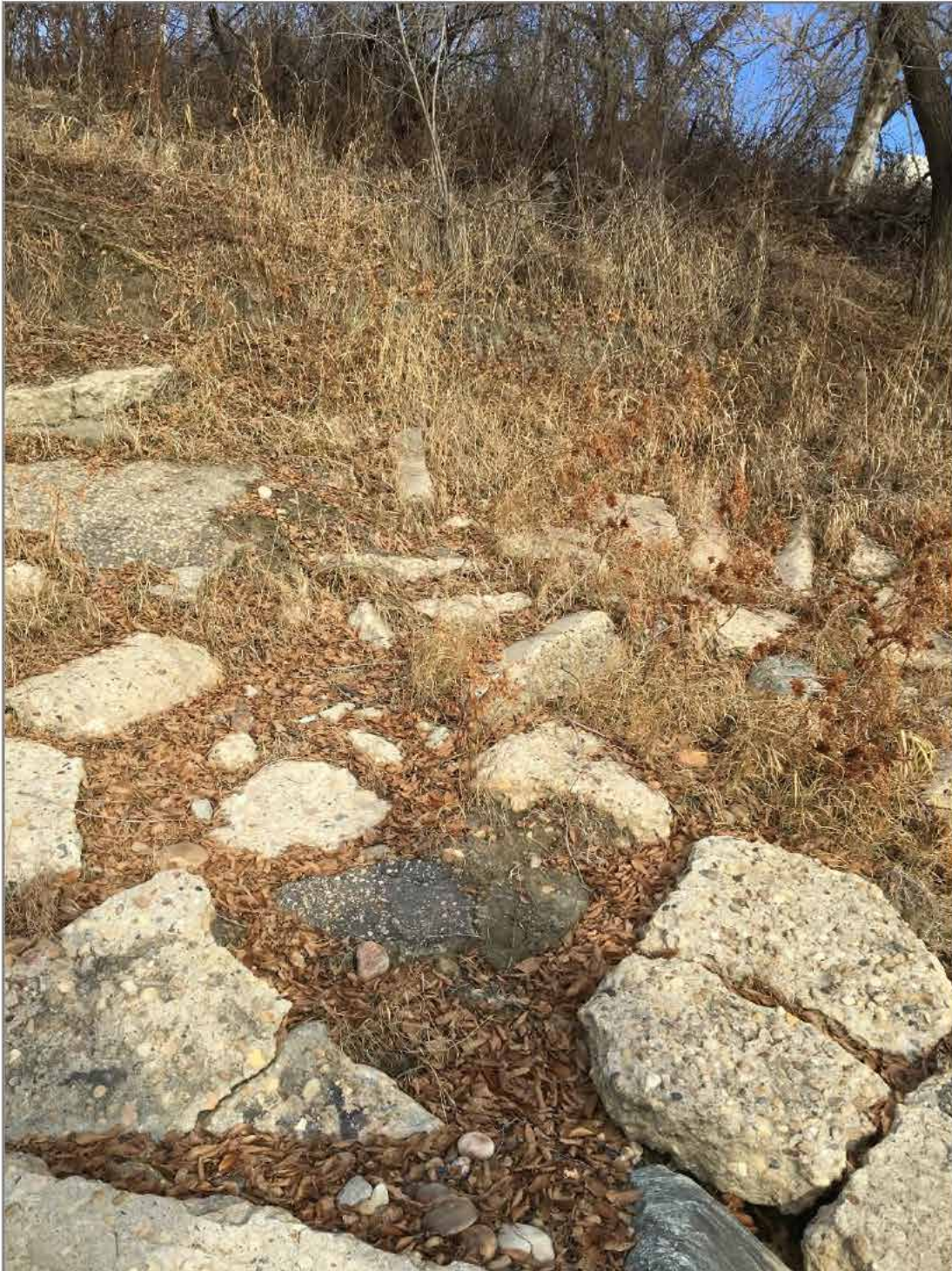


Photo 11: Large Concrete Blocks on River Bank Slope



Photo 12: Large Concrete Blocks close to River Level



Photo 13: Large Concrete Blocks close to River Level



Photo 14: Piers of Existing Footbridge and LRT Bridge



Photo 15: Piers of Existing Footbridge and LRT Bridge



Photo 16: High Level Bridge Pier, Existing Concrete Retaining Wall and River Bank Slope



Photo 17: Existing Retaining Wall and Trail near Waltherdale Bridge (Looking West)



Photo 18: Rip Rap at Walterdale Bridge Abutment



Photo 19: Eroded River Bank Slope and Exposed Tree Roots

APPENDIX A

TETRA TECH'S LIMITATIONS ON THE USE OF THIS DOCUMENT

LIMITATIONS ON USE OF THIS DOCUMENT

GEOTECHNICAL

1.1 USE OF DOCUMENT AND OWNERSHIP

This document pertains to a specific site, a specific development, and a specific scope of work. The document may include plans, drawings, profiles and other supporting documents that collectively constitute the document (the "Professional Document").

The Professional Document is intended for the sole use of TETRA TECH's Client (the "Client") as specifically identified in the TETRA TECH Services Agreement or other Contractual Agreement entered into with the Client (either of which is termed the "Contract" herein). TETRA TECH does not accept any responsibility for the accuracy of any of the data, analyses, recommendations or other contents of the Professional Document when it is used or relied upon by any party other than the Client, unless authorized in writing by TETRA TECH.

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Where TETRA TECH submits electronic file and/or hard copy versions of the Professional Document or any drawings or other project-related documents and deliverables (collectively termed TETRA TECH's "Instruments of Professional Service"), only the signed and/or sealed versions shall be considered final. The original signed and/or sealed electronic file and/or hard copy version archived by TETRA TECH shall be deemed to be the original. TETRA TECH will archive a protected digital copy of the original signed and/or sealed version for a period of 10 years.

Both electronic file and/or hard copy versions of TETRA TECH's Instruments of Professional Service shall not, under any circumstances, be altered by any party except TETRA TECH. TETRA TECH's Instruments of Professional Service will be used only and exactly as submitted by TETRA TECH.

Electronic files submitted by TETRA TECH have been prepared and submitted using specific software and hardware systems. TETRA TECH makes no representation about the compatibility of these files with the Client's current or future software and hardware systems.

1.3 STANDARD OF CARE

Services performed by TETRA TECH for the Professional Document have been conducted in accordance with the Contract, in a manner consistent with the level of skill ordinarily exercised by members of the profession currently practicing under similar conditions in the jurisdiction in which the services are provided. Professional judgment has been applied in developing the conclusions and/or recommendations provided in this Professional Document. No warranty or guarantee, express or implied, is made concerning the test results, comments, recommendations, or any other portion of the Professional Document.

If any error or omission is detected by the Client or an Authorized Party, the error or omission must be immediately brought to the attention of TETRA TECH.

1.4 DISCLOSURE OF INFORMATION BY CLIENT

The Client acknowledges that it has fully cooperated with TETRA TECH with respect to the provision of all available information on the past, present, and proposed conditions on the site, including historical information respecting the use of the site. The Client further acknowledges that in order for TETRA TECH to properly provide the services contracted for in the Contract, TETRA TECH has relied upon the Client with respect to both the full disclosure and accuracy of any such information.

1.5 INFORMATION PROVIDED TO TETRA TECH BY OTHERS

During the performance of the work and the preparation of this Professional Document, TETRA TECH may have relied on information provided by third parties other than the Client.

While TETRA TECH endeavours to verify the accuracy of such information, TETRA TECH accepts no responsibility for the accuracy or the reliability of such information even where inaccurate or unreliable information impacts any recommendations, design or other deliverables and causes the Client or an Authorized Party loss or damage.

1.6 GENERAL LIMITATIONS OF DOCUMENT

This Professional Document is based solely on the conditions presented and the data available to TETRA TECH at the time the data were collected in the field or gathered from available databases.

The Client, and any Authorized Party, acknowledges that the Professional Document is based on limited data and that the conclusions, opinions, and recommendations contained in the Professional Document are the result of the application of professional judgment to such limited data.

The Professional Document is not applicable to any other sites, nor should it be relied upon for types of development other than those to which it refers. Any variation from the site conditions present, or variation in assumed conditions which might form the basis of design or recommendations as outlined in this document, at or on the development proposed as of the date of the Professional Document requires a supplementary exploration, investigation, and assessment.

TETRA TECH is neither qualified to, nor is it making, any recommendations with respect to the purchase, sale, investment or development of the property, the decisions on which are the sole responsibility of the Client.

1.7 ENVIRONMENTAL AND REGULATORY ISSUES

Unless stipulated in the report, TETRA TECH has not been retained to explore, address or consider and has not explored, addressed or considered any environmental or regulatory issues associated with development on the subject site.

1.8 NATURE AND EXACTNESS OF SOIL AND ROCK DESCRIPTIONS

Classification and identification of soils and rocks are based upon commonly accepted systems, methods and standards employed in professional geotechnical practice. This report contains descriptions of the systems and methods used. Where deviations from the system or method prevail, they are specifically mentioned.

Classification and identification of geological units are judgmental in nature as to both type and condition. TETRA TECH does not warrant conditions represented herein as exact, but infers accuracy only to the extent that is common in practice.

Where subsurface conditions encountered during development are different from those described in this report, qualified geotechnical personnel should revisit the site and review recommendations in light of the actual conditions encountered.

1.9 LOGS OF TESTHOLES

The testhole logs are a compilation of conditions and classification of soils and rocks as obtained from field observations and laboratory testing of selected samples. Soil and rock zones have been interpreted. Change from one geological zone to the other, indicated on the logs as a distinct line, can be, in fact, transitional. The extent of transition is interpretive. Any circumstance which requires precise definition of soil or rock zone transition elevations may require further investigation and review.

1.10 STRATIGRAPHIC AND GEOLOGICAL INFORMATION

The stratigraphic and geological information indicated on drawings contained in this report are inferred from logs of test holes and/or soil/rock exposures. Stratigraphy is known only at the locations of the test hole or exposure. Actual geology and stratigraphy between test holes and/or exposures may vary from that shown on these drawings. Natural variations in geological conditions are inherent and are a function of the historical environment. TETRA TECH does not represent the conditions illustrated as exact but recognizes that variations will exist. Where knowledge of more precise locations of geological units is necessary, additional exploration and review may be necessary.

1.11 PROTECTION OF EXPOSED GROUND

Excavation and construction operations expose geological materials to climatic elements (freeze/thaw, wet/dry) and/or mechanical disturbance which can cause severe deterioration. Unless otherwise specifically indicated in this report, the walls and floors of excavations must be protected from the elements, particularly moisture, desiccation, frost action and construction traffic.

1.12 SUPPORT OF ADJACENT GROUND AND STRUCTURES

Unless otherwise specifically advised, support of ground and structures adjacent to the anticipated construction and preservation of adjacent ground and structures from the adverse impact of construction activity is required.

1.13 INFLUENCE OF CONSTRUCTION ACTIVITY

Construction activity can impact structural performance of adjacent buildings and other installations. The influence of all anticipated construction activities should be considered by the contractor, owner, architect and prime engineer in consultation with a geotechnical engineer when the final design and construction techniques, and construction sequence are known.

1.14 OBSERVATIONS DURING CONSTRUCTION

Because of the nature of geological deposits, the judgmental nature of geotechnical engineering, and the potential of adverse circumstances arising from construction activity, observations during site preparation, excavation and construction should be carried out by a geotechnical engineer. These observations may then serve as the basis for confirmation and/or alteration of geotechnical recommendations or design guidelines presented herein.

1.15 DRAINAGE SYSTEMS

Unless otherwise specified, it is a condition of this report that effective temporary and permanent drainage systems are required and that they must be considered in relation to project purpose and function. Where temporary or permanent drainage systems are installed within or around a structure, these systems must protect the structure from loss of ground due to mechanisms such as internal erosion and must be designed so as to assure continued satisfactory performance of the drains. Specific design details regarding the geotechnical aspects of such systems (e.g. bedding material, surrounding soil, soil cover, geotextile type) should be reviewed by the geotechnical engineer to confirm the performance of the system is consistent with the conditions used in the geotechnical design.

1.16 DESIGN PARAMETERS

Bearing capacities for Limit States or Allowable Stress Design, strength/stiffness properties and similar geotechnical design parameters quoted in this report relate to a specific soil or rock type and condition. Construction activity and environmental circumstances can materially change the condition of soil or rock. The elevation at which a soil or rock type occurs is variable. It is a requirement of this report that structural elements be founded in and/or upon geological materials of the type and in the condition used in this report. Sufficient observations should be made by qualified geotechnical personnel during construction to assure that the soil and/or rock conditions considered in this report in fact exist at the site.

1.17 SAMPLES

TETRA TECH will retain all soil and rock samples for 30 days after this report is issued. Further storage or transfer of samples can be made at the Client's expense upon written request, otherwise samples will be discarded.

1.18 APPLICABLE CODES, STANDARDS, GUIDELINES & BEST PRACTICE

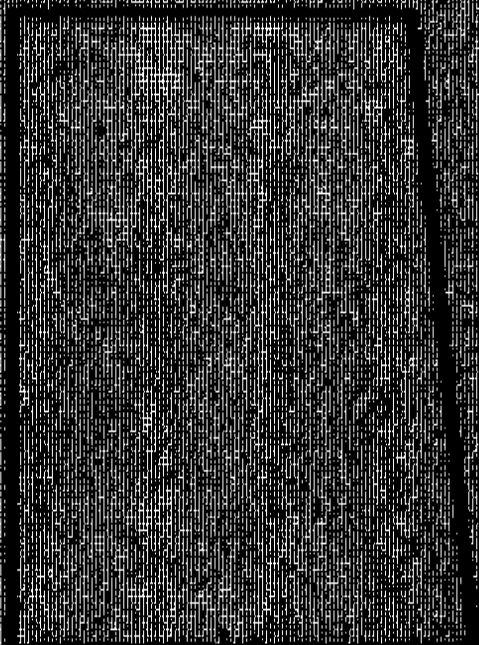
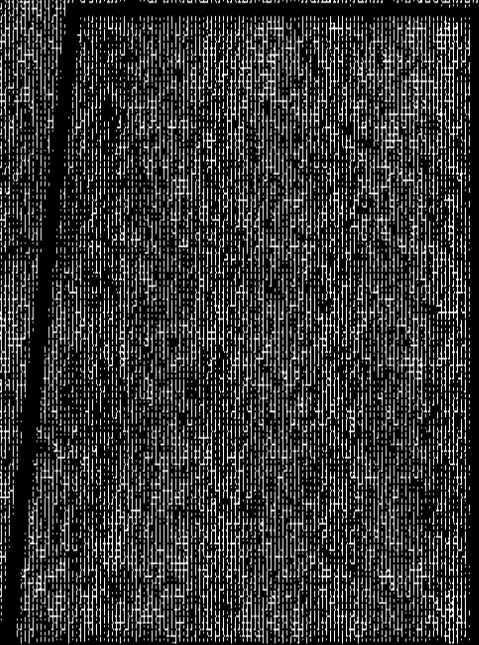
This document has been prepared based on the applicable codes, standards, guidelines or best practice as identified in the report. Some mandated codes, standards and guidelines (such as ASTM, AASHTO Bridge Design/Construction Codes, Canadian Highway Bridge Design Code, National/Provincial Building Codes) are routinely updated and corrections made. TETRA TECH cannot predict nor be held liable for any such future changes, amendments, errors or omissions in these documents that may have a bearing on the assessment, design or analyses included in this report.

APPENDIX B

EXTRACTED RELEVANT BOREHOLE INFORMATION

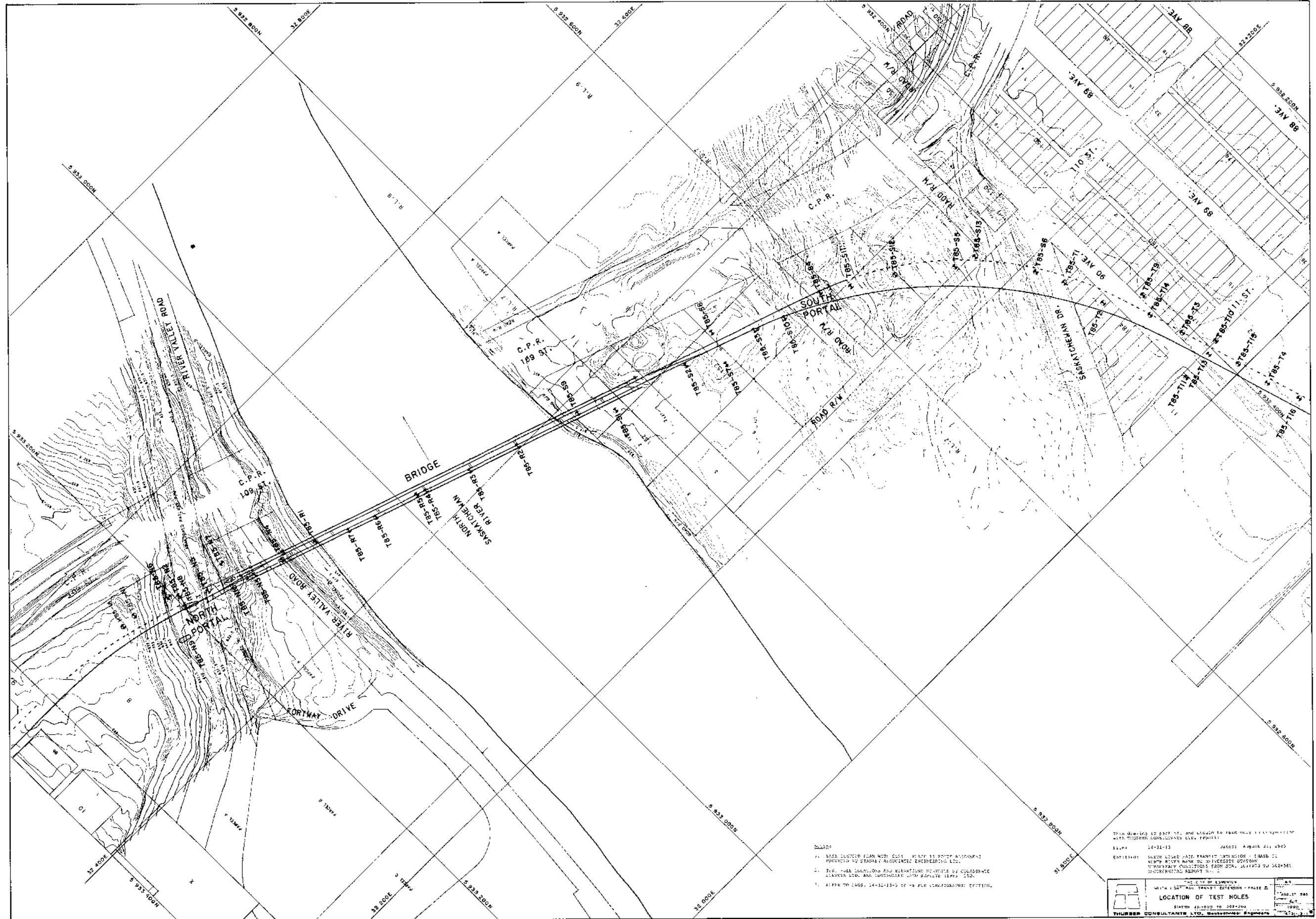
UNITED STATES GOVERNMENT
OFFICE OF THE SECRETARY OF DEFENSE
WASHINGTON, D. C. 20301

Approved Release Under Executive Order 13526, dated 05-08-2011
Authority: 48 CFR 101-11.6, 101-11.7, 101-11.8, 101-11.9, 101-11.10, 101-11.11, 101-11.12, 101-11.13, 101-11.14, 101-11.15, 101-11.16, 101-11.17, 101-11.18, 101-11.19, 101-11.20, 101-11.21, 101-11.22, 101-11.23, 101-11.24, 101-11.25, 101-11.26, 101-11.27, 101-11.28, 101-11.29, 101-11.30, 101-11.31, 101-11.32, 101-11.33, 101-11.34, 101-11.35, 101-11.36, 101-11.37, 101-11.38, 101-11.39, 101-11.40, 101-11.41, 101-11.42, 101-11.43, 101-11.44, 101-11.45, 101-11.46, 101-11.47, 101-11.48, 101-11.49, 101-11.50, 101-11.51, 101-11.52, 101-11.53, 101-11.54, 101-11.55, 101-11.56, 101-11.57, 101-11.58, 101-11.59, 101-11.60, 101-11.61, 101-11.62, 101-11.63, 101-11.64, 101-11.65, 101-11.66, 101-11.67, 101-11.68, 101-11.69, 101-11.70, 101-11.71, 101-11.72, 101-11.73, 101-11.74, 101-11.75, 101-11.76, 101-11.77, 101-11.78, 101-11.79, 101-11.80, 101-11.81, 101-11.82, 101-11.83, 101-11.84, 101-11.85, 101-11.86, 101-11.87, 101-11.88, 101-11.89, 101-11.90, 101-11.91, 101-11.92, 101-11.93, 101-11.94, 101-11.95, 101-11.96, 101-11.97, 101-11.98, 101-11.99, 101-11.100



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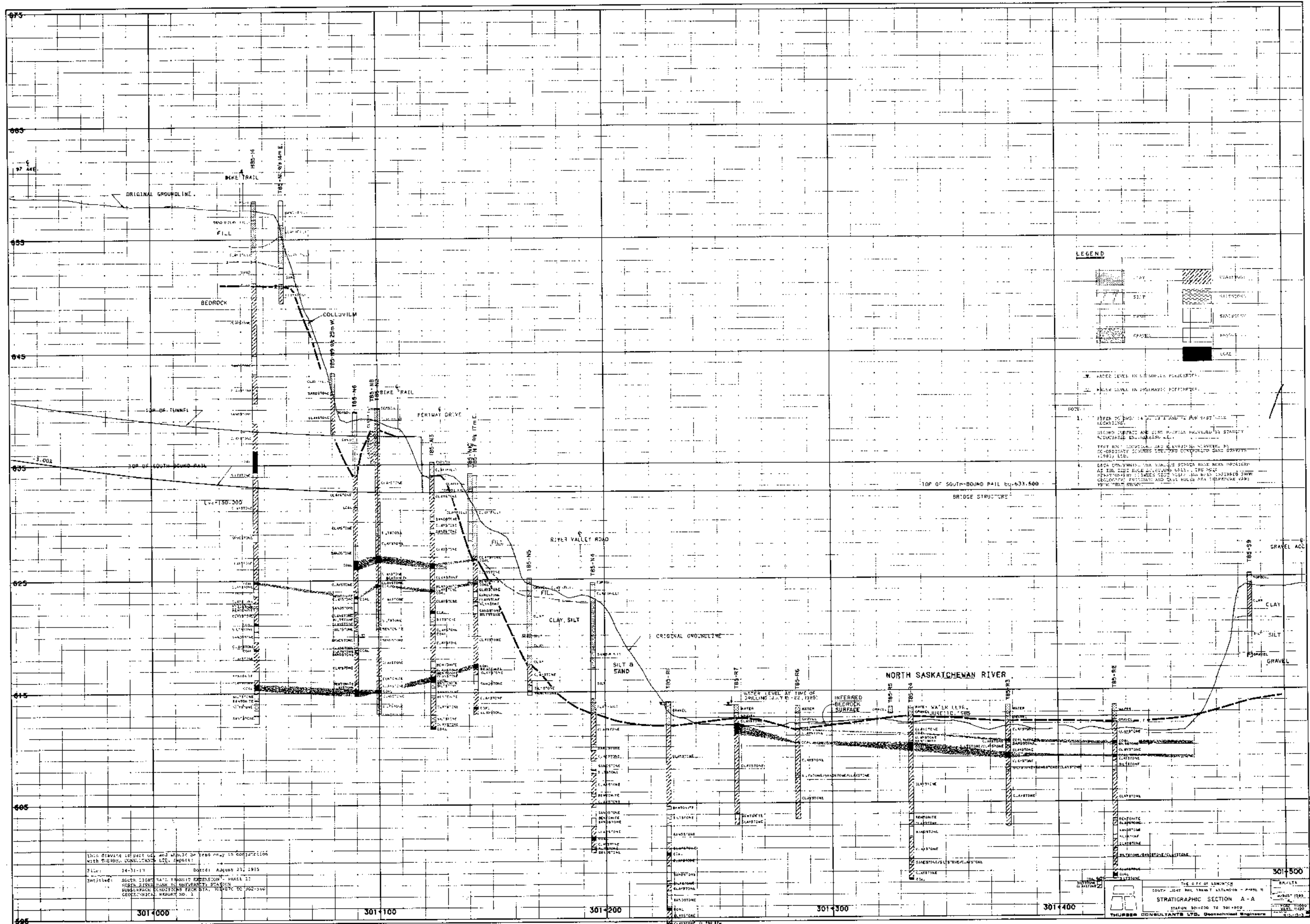
UNCLASSIFIED CONFIDENTIAL



- Notes:
1. SEE LOCATION PLAN WITH THIS PLAN FOR PORTAL ALIGNMENT AND APPROXIMATE DIMENSIONS.
 2. THE -0.60 METER ELEVATION IS THE FINISHED GRADE ELEVATION AND NOT THE NATURAL GROUND ELEVATION.
 3. REFER TO DRAWING 14-31-33-5 FOR PLAN DIMENSIONS OF BRIDGE.

This drawing is part of the contract for the construction of the Saskatoon River Valley Road Bridge. It is to be used in conjunction with the contract documents and specifications. Issue: 14-31-13. Date: August 23, 1965. Engineer: Bruce Lloyd and Frank J. Goss. Station: 14-31-33-5. Project: Saskatoon River Valley Road Bridge. Drawing: LOCATION OF TEST HOLES.

THE CITY OF SASKATOON		Scale: 1" = 100'
Saskatoon River Valley Road Bridge - Phase B		Sheet: 14-31-33-5
LOCATION OF TEST HOLES		Station: 14-31-33-5
THURBER CONSULTANTS LTD., Geotechnical Engineers		1965



LEGEND

[Symbol]	CLAY	[Symbol]	CLAYSTONE
[Symbol]	SILT	[Symbol]	SANDSTONE
[Symbol]	GRAVEL	[Symbol]	GRAVEL
[Symbol]	WATER LEVEL IN UNSATURATED ZONE	[Symbol]	WATER LEVEL IN SATURATED ZONE

1. REFER TO DRAWING 14-101-100 TO LOCATE THIS SECTION.

2. SECOND SURFACE AND GROUND SURFACE PROVIDED BY STAFFED SURVEYING ENGINEERING CO.

3. TEST AND ANALYSIS REPORT BY STAFFED SURVEYING ENGINEERING CO. (1983) LTD.

4. LOGS CONTAINING DATA FROM STRONG WERE REVIEWED AND FOUND TO BE CORRECT. THE LOGS WERE PREPARED BY STAFFED SURVEYING ENGINEERING CO. (1983) LTD. AND WERE CHECKED BY GEOTECHNICAL ENGINEERS AND CIVIL ENGINEERS FROM STAFFED SURVEYING ENGINEERING CO. (1983) LTD.

THIS DRAWING IS FOR USE AND SHOULD BE READ ONLY IN CONNECTION WITH THE REPORT CONSULTANTS LTD. REPORT.

File: 14-101-100 Date: August 23, 1983

Project: SOUTH LIGHT RAIL TRANSIT EXPANSION - PHASE 12

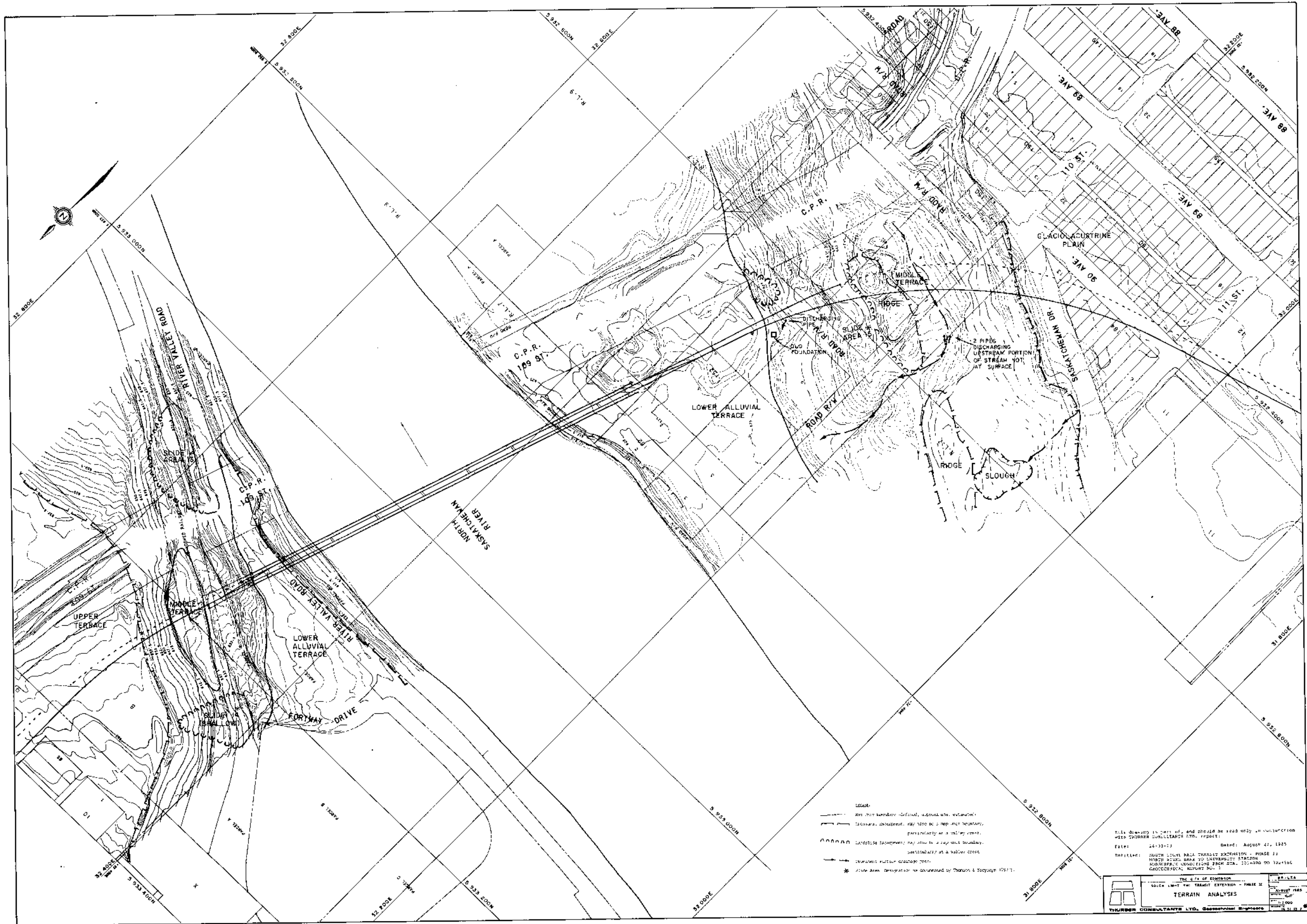
Sub-project: NORTH RIVER VALLEY STATION

Geotechnical Consultant: STAFFED SURVEYING ENGINEERING CO. (1983) LTD.

301+500

THE CITY OF LONDON
SOUTH LIGHT RAIL TRANSIT EXPANSION - PHASE 12
STRATIGRAPHIC SECTION A-A
STATION 301+000 TO 301+500

THURBER CONSULTANTS LTD. Geotechnical Engineers



- Legend:**
- Lot boundaries (defined, assumed, extended)
 - Drainage (assumed, may also be a property boundary, particularly at a valley crest)
 - Landslide boundaries (may also be a property boundary, particularly at a valley crest)
 - Stream flow direction
 - * Zone Area (designated by Thomson & Spayke 1971)

This drawing is part of, and should be read only in conjunction with the REPORT DATED 1985.

Date: 24-11-85 Drawn: August 22, 1985

Project: NORTH SASKATCHEWAN RIVER VALLEY ROAD - PHASE II
 NORTH SASKATCHEWAN RIVER VALLEY ROAD - PHASE II
 SUBSIDIARY CONSULTING ENGINEERS FROM STA. 10+00 TO 10+50
 GEOGRAPHICAL REPORT No. 1

THE CITY OF EDMONTON		PLATE 1
SOUTH SASKATCHEWAN RIVER VALLEY ROAD - PHASE II		PLATE 1
TERRAIN ANALYSIS		PLATE 1
THOMSON CONSULTANTS LTD., Geotechnical Engineers		PLATE 1

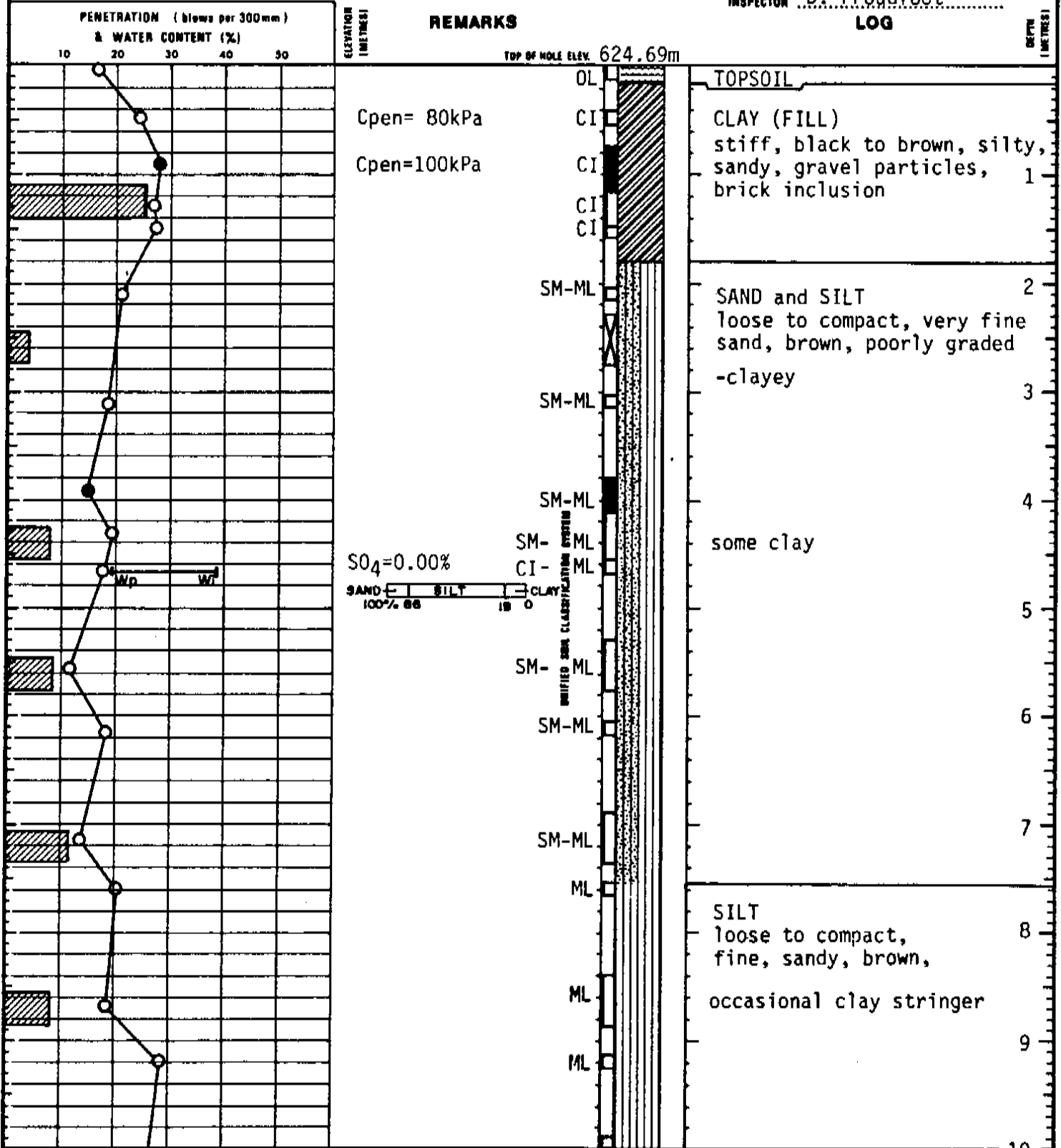
LOG OF TEST HOLE

LOCATION
N5933109.4, E32479.6

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT
NORTH VALLEY & PORTAL

DATE May 3/85
METHOD B-61 Solid Stem
DRILLING CO Mobile Augers
INSPECTOR D. Proudfoot

LEGEND:
SAMPLED: Disturbed Undisturbed No recovery
WATER CONTENT:
WATER LEVEL
LIQUID LIMIT
PLASTIC LIMIT



LOG OF TEST HOLE

LOCATION

.....

.....

CLIENT THE CITY OF EDMONTON

PROJECT SLRT PROJECT
NORTH VALLEY & PORTAL

DATE May 3/85

METHOD B-61 Solid Stem

DRILLING CO Mobile Augers

INSPECTOR D. Proudfoot

LEGEND:

- SAMPLED: Disturbed Undisturbed No recovery
- WATER CONTENT:
- WATER LEVEL ∇
- LIQUID LIMIT W_L
- PLASTIC LIMIT W_p

PENETRATION (blows per 300 mm)
& WATER CONTENT (%)

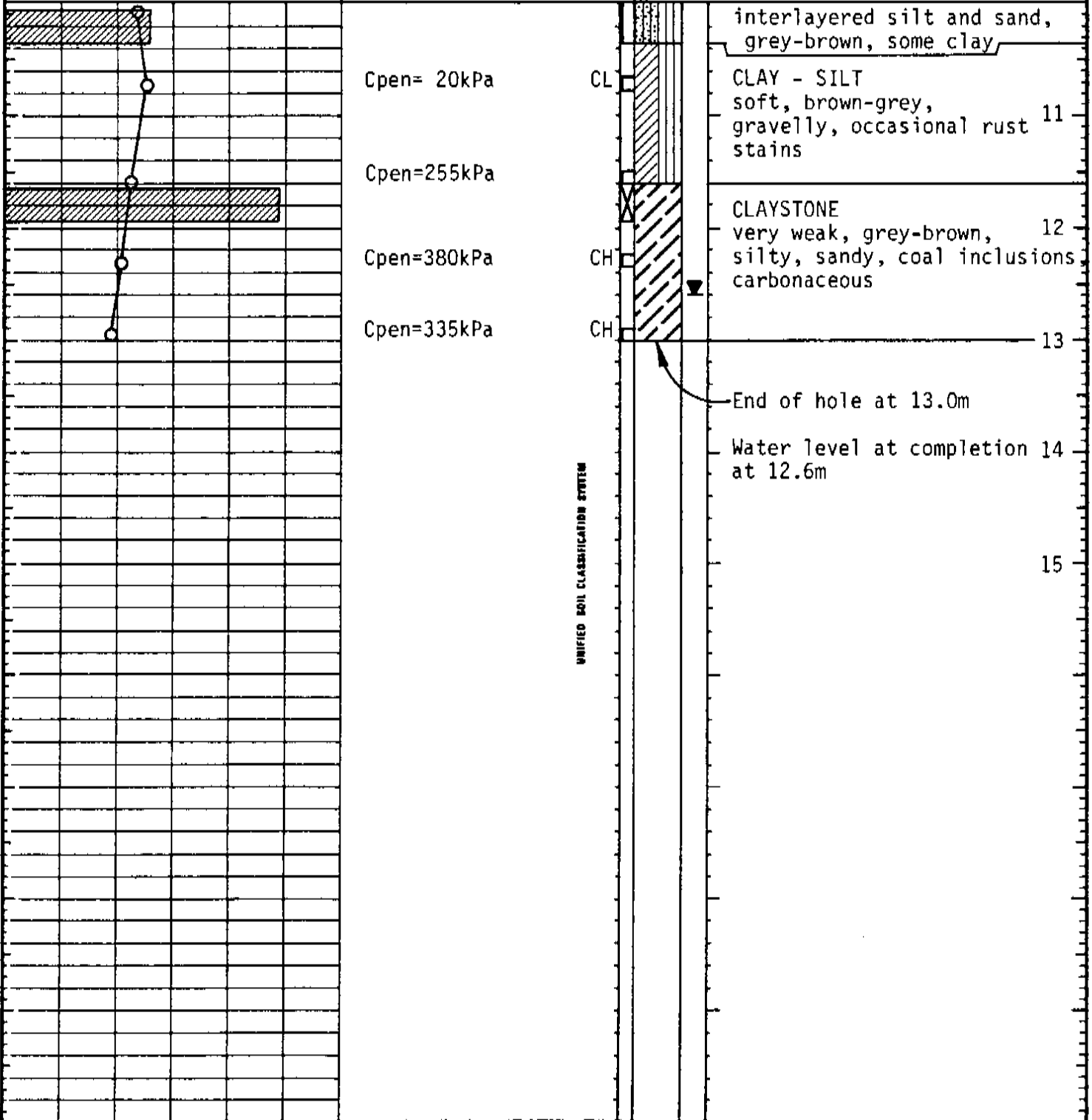
10 20 30 40 50

ELEVATION
(METRES)

REMARKS

TOP OF HOLE ELEV.

DEPTH
(METRES)



LOG OF TEST HOLE CORING

LOCATION
 N5933109.4, E32479.6
 RIG TYPE Cyclone 300
 BIT
 CORE BARREL Christiansen
 GROUND ELEV. 624.69m

CLIENT THE CITY OF EDMONTON
 PROJECT SLRT PROJECT
 NORTH VALLEY & PORTAL
 DATE May 8/85
 DRILLING CO. Garrity & Baker
 INSPECTOR D. Proudfoot

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	W _n (%)	TEST RESULTS	DEPTH (METRES)
11								11
12								12
13	T85-N4 START OF CORING AT 13.0m				13.0			13
14	CLAYSTONE very weak, silty, moderately weathered, occasional coal stringer, dark grey			-bedding plane fracture, horizontal	66 (66) 13.5	29.1		14
	-sandstone stringer, 30mm			-thickly bedded -bedding plane fracture		20.2		
	SANDSTONE, weak, very fine, moderately weathered, grey				97 (61)	24.0		
15	CLAYSTONE weak, silty, slightly weathered, some sandstone stringers and ironstone, dark grey			-vertical fracture: closed	15.0	21.9		15
	SANDSTONE weak, silty, bentonitic, slightly weathered, light grey			-medium bedded		18.1		
16	SILTSTONE, weak, some sand, bentonitic, slightly weathered, grey				104 (100)	14.9		16
17	CLAYSTONE weak, silty, slightly weathered, some siltstone laminations and ironstone nodules, dark grey			-bedding about 10° to horizontal		18.9		17
18	-carbonaceous			-fracture: 60°, planar		18.1		
	BENTONITE, light grey, weak			-subvertical fracture, 90mm long -rubbly core	18.0	18.8		18
	CLAYSTONE weak, silty, trace of sand, moderately weathered, some coal stringers					15.4		
19				-thickly bedded		18.3		19
20				-coal parting, 10° to horizontal	102 (100)	60.3 18.9	C _{pen} =142kPa C _{pen} = 73kPa W _p =41% W _L =547% I _p =506%	20

LOG OF TEST HOLE CORING

LOCATION

CLIENT THE CITY OF EDMONTON

PROJECT SLRT PROJECT

RIG TYPE

NORTH VALLEY & PORTAL

BIT

CASING DIA.

DATE May 8/85

CORE BARREL

CORE DIA.

DRILLING CO. Garrity & Baker

GROUND ELEV.

WATER LEVEL

INSPECTOR D. Proudfoot

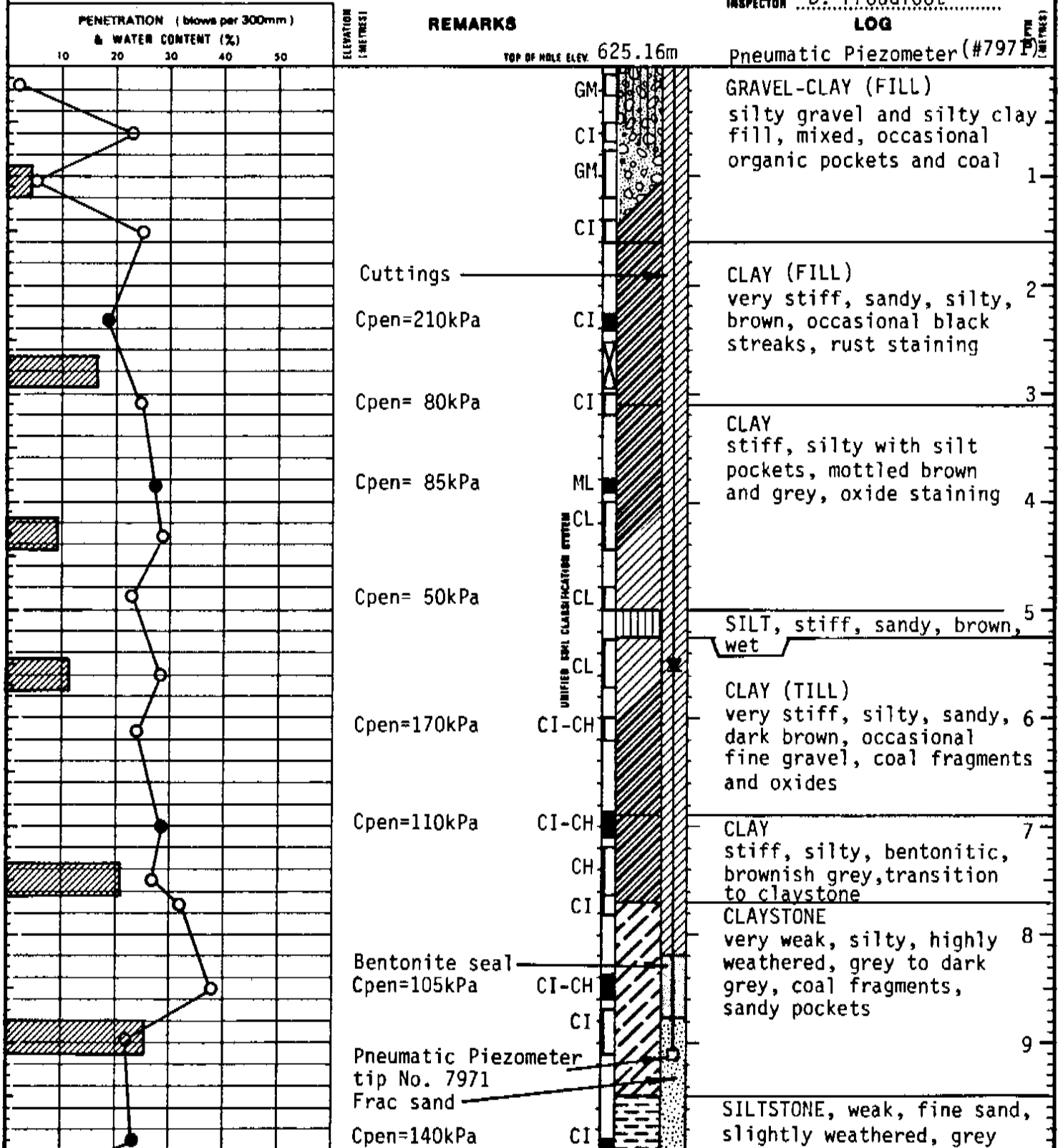
DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
21	SANDSTONE very weak, silty, bentonitic, moderately to slightly weathered, light grey -very weak, occasional iron-stone nodules and coal parting -calcareous			-coal parting, 10° to horizontal -subvertical fracture, 80mm long -thin bentonite seam, 20mm thick -bedding: 20° to horizontal	21.0	16.0 14.7 6.1 17.4 16.2		21
22	CLAYSTONE very weak, silty, bentonitic, slightly weathered, dark grey			-thickly bedded		16.1		22
	COAL, black, slightly weathered			-vertical fracture, entire thickness of seam	97 (97)	16.2		
23	CLAYSTONE weak, very silty, slightly weathered, grey			-23.3-23.4: joints, slickensided 30°-35°		21.6		23
24	SILTSTONE, very weak, trace of fine sand, bentonitic, grey SANDSTONE, very weak, silty, bentonitic, grey			-coal parting	24.0	16.9 15.5 14.4		24
	End of hole at 24.0m							
25								25

LOG OF TEST HOLE

LOCATION N5933136.7, E32487.0

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT
NORTH VALLEY & PORTAL
DATE July 11/85
METHOD B-61 Solid Stem
DRILLING CO Mobile Augers
INSPECTOR D. Proudfoot

LEGEND:
SAMPLES:
Disturbed (open square)
Undisturbed (filled square)
No recovery (cross-hatched square)
WATER CONTENT:
Liquid Limit (open circle)
Plastic Limit (filled circle)
WATER LEVEL (inverted triangle)
LIQUID LIMIT (line with open circle)
PLASTIC LIMIT (line with filled circle)



LOG OF TEST HOLE

LOCATION

.....

.....

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT
NORTH VALLEY & PORTAL
DATE July 11/85
METHOD B-61 Solid Stem
DRILLING CO Mobile Augers
INSPECTOR D. Proudfoot

LEGEND:

SAMPLER: Disturbed Undisturbed No recovery

WATER CONTENT:

WATER LEVEL ∇

w_L LIQUID LIMIT

w_p PLASTIC LIMIT

PENETRATION (blows per 300mm)
& WATER CONTENT (%)

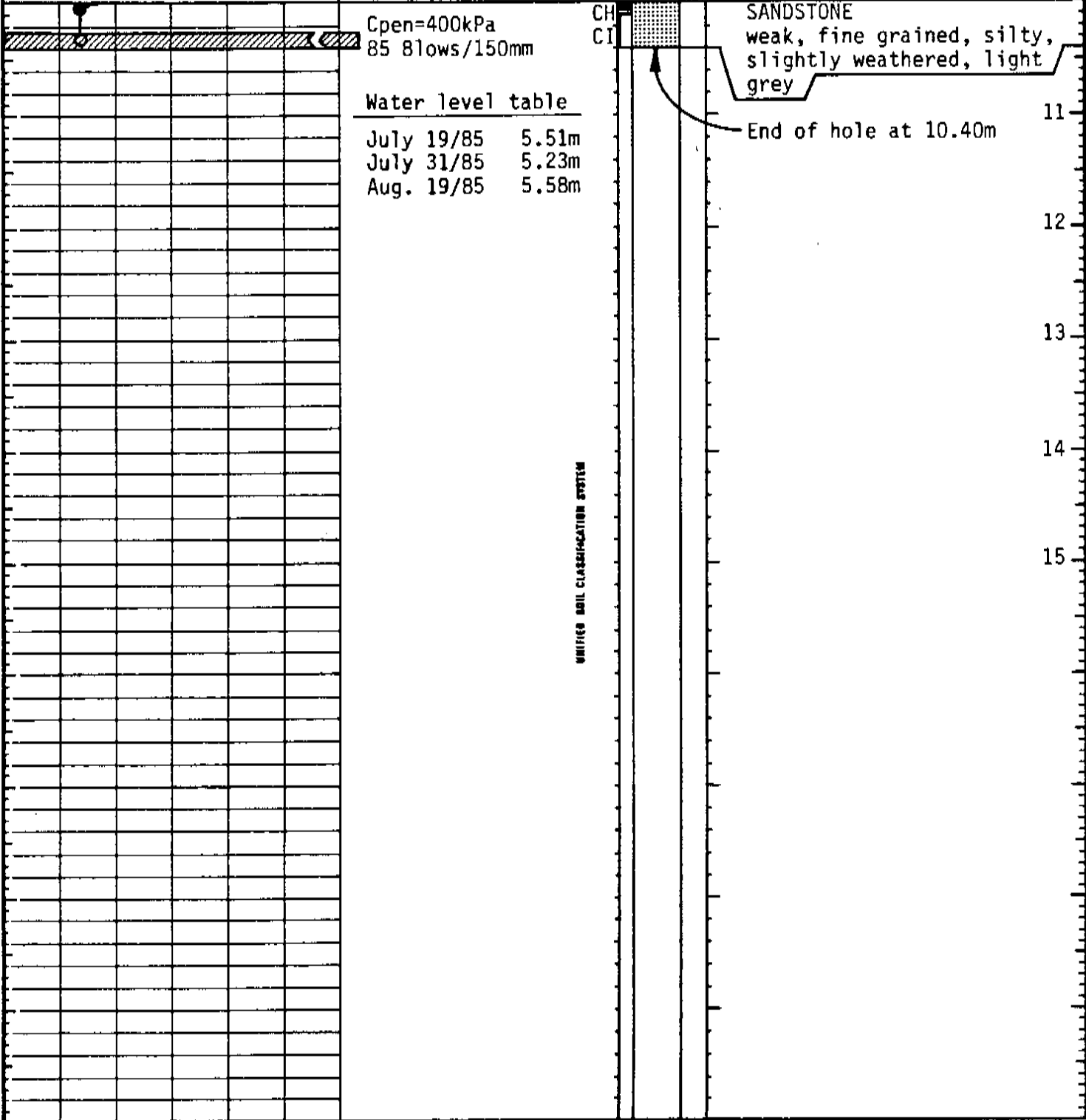
10 20 30 40 50

ELEVATION
(METRES)

REMARKS

TOP OF HOLE ELEV.

DEPTH
(METRES)



C_{pen}=400kPa
85 Blows/150mm

Water level table

July 19/85	5.51m
July 31/85	5.23m
Aug. 19/85	5.58m

CH
CI

SANDSTONE
weak, fine grained, silty,
slightly weathered, light
grey

End of hole at 10.40m

UNIFIED SOIL CLASSIFICATION SYSTEM

LOG OF TEST HOLE

LOCATION

.....

.....

CLIENT THE CITY OF EDMONTON

PROJECT SLRT PROJECT

NORTH VALLEY & PORTAL

DATE Aug. 13/85

METHOD Mayhew 100 Wet Rotary

DRILLING CO Garrity & Baker

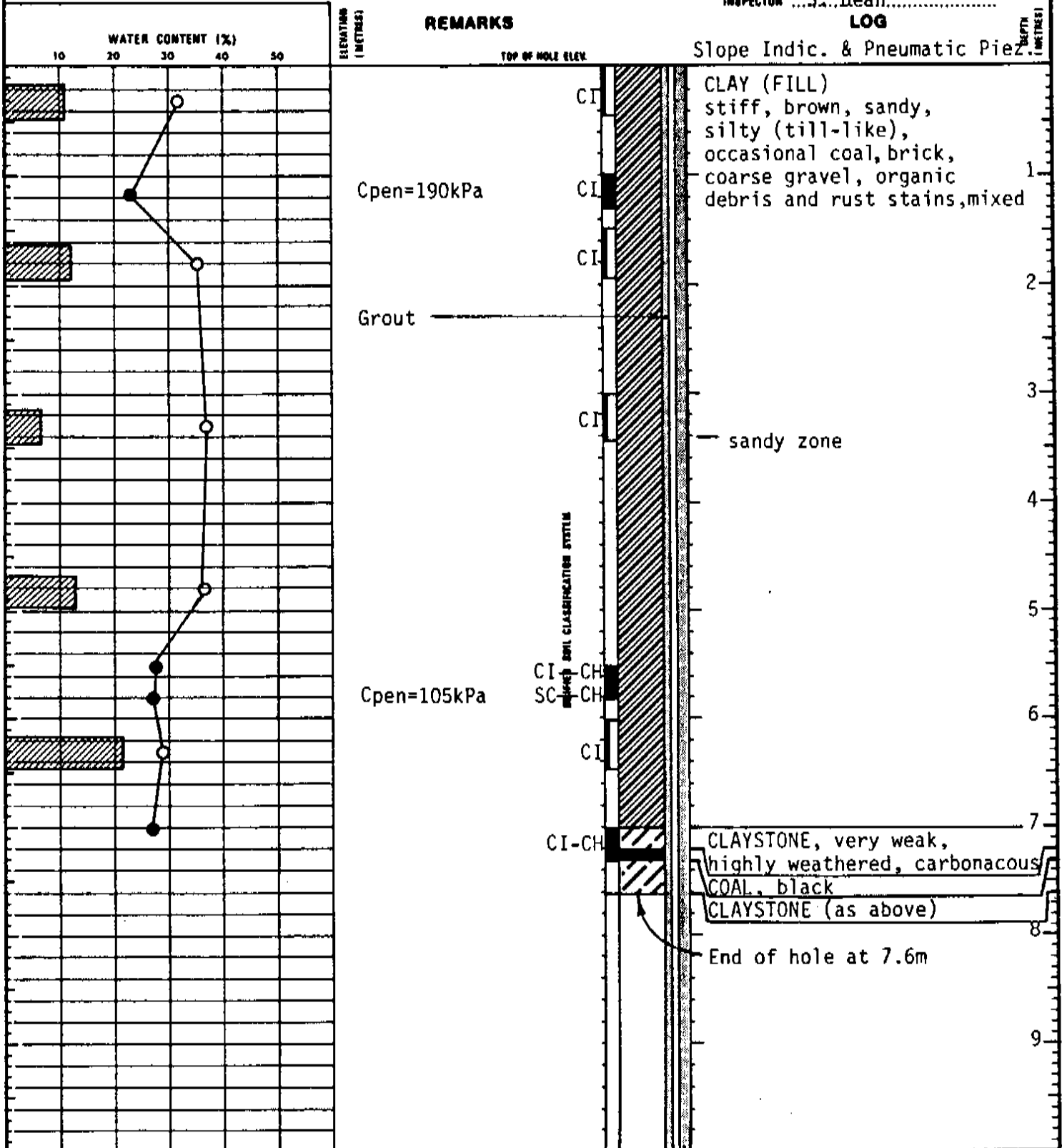
INSPECTOR S. Bean

LEGEND:

SAMPLES:
 □ Disturbed
 ■ Undisturbed
 ⊠ No recovery

WATER CONTENT:
 ○
 ●

↓ WATER LEVEL
 L LIQUID LIMIT
 P PLASTIC LIMIT



LOG OF TEST HOLE CORING

LOCATION CLIENT THE CITY OF EDMONTON
 PROJECT SLRT PROJECT
 RIG TYPE Mayhem 1000 NORTH VALLEY & PORTAL
 BIT CASING DIA. DATE Aug. 13/85
 CORE BARREL Christiansen CORE DIA. 75mm DRILLING CO. Garrity & Baker
 GROUND ELEV. WATER LEVEL INSPECTOR S. Bean

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (ROD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
1								1
2								2
3								3
4								4
5								5
6								6
7								7
7.6	T85-N7 START CORING AT 7.6m		Grout Slope Indicator & Adjac. Pneumatic Piezometer Installation (#7961)		7.6			7.6
8	CLAYSTONE, very weak, moderately weathered, very silty, brown, carbonaceous SANDSTONE, weak, moderately weathered, fine grained, grey, very calcareous			-thinly bedded		22.1		8
9	CLAYSTONE, as above, some siltstone laminations			-medium bedded, rubbly zone -coal seam: 30mm horizontal	63 (53)	23.7		9
9.2					9.2	18.4		9.2
10	BENTONITE, very weak, white COAL, weak, slightly weathered, black, shiny CLAYSTONE, weak, sl. weath., br., carbonaceous, occas. coal frag.			-thinly bedded, highly fractured -shear: 40°, planar, medium bedded -shear: 50°, planar	96 (89)	59.4		10
	-bentonitic and silty zones					17.8		

LOG OF TEST HOLE CORING

LOCATION
 CLIENT THE CITY OF EDMONTON
 PROJECT SLRT PROJECT
 RIG TYPE Mayhew 1000
 NORTH VALLEY & PORTAL
 BIT CASING DIA.
 DATE Aug. 13/85
 CORE BARREL Christiansen CORE DIA. 75mm
 DRILLING CO. Garrity & Baker
 GROUND ELEV. WATER LEVEL
 INSPECTOR S. Bean

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	CLAYSTONE							
	SANDSTONE, weak, sl. weathered, bentonitic, med. gr., light grey, silty, calcareous, occas. coal laminations			-medium bedded	96 (89)	14.3		
11	CLAYSTONE, weak, slightly weathered, silty, carbonaceous			-coal parting -coal seam: 60mm, horizontal	11.0	19.8		11
	SILTSTONE, moderately weak, slightly weathered, light brown					9.9		
12	SANDSTONE moderately weak, slightly weathered, medium grained, light grey, very calcareous			-thickly bedded	100 (89)	17.3		12
	SILTSTONE, moderately strong, slightly weathered, grey-brown, calcareous			-medium bedded, rubbly core -thickly bedded, rubbly zones	12.2	4.7		
13	CLAYSTONE weak, slightly weathered, silty, brown, carbonaceous, some sandy lenses, locally bentonitic zones			Grout		18.0		13
				Slope Indicator & Adjac. Pneumatic Piezometer Installation	92 (82)	20.5		
14	CLAYSTONE/SANDSTONE interbedded beds 1-25mm thick			-very thinly bedded, random spacing		15.7		14
15	CLAYSTONE weak, slightly weathered, silty, grey, occasional siltstone lamination			-thickly bedded, rubbly zone		33.1		15
	extremely bentonitic (15.2-16.2) -occasional bentonite stringer				15.2	39.2		
16						40.4		16
	COAL, very weak, slightly weathered, black, very pyritic			-medium bedded, highly fractured	93 (83)	23.3		
17	CLAYSTONE, weak, sl. weathered, dark brown, very carbonaceous, thin bentonitic laminat. (16.95)			-Pneumatic Piezometer Tip #7961 Installed in Adjacent Hole to Slope Indicator		14.3		17
18	SANDSTONE weak, slightly weathered, slightly clayey, medium grained, light grey, calcareous, occasional coal fragments and stringers			-thickly bedded	18.3	16.1		18
						13.0		
19	CLAYSTONE weak, slightly weathered, very silty, greyish brown, occasional siltstone layers			-thickly bedded, rubbly zone	98 (91)	14.8		19
20	-siltstone layer (30mm)					13.7		20

LOG OF TEST HOLE CORING

LOCATION CLIENT THE CITY OF EDMONTON
 PROJECT SLRT PROJECT
 RIG TYPE Mayhew 1000 NORTH VALLEY & PORTAL
 BIT CASING DIA. DATE Aug. 13/85
 CORE BARREL Christensen CORE DIA. .75mm DRILLING CO. Garrity & Baker
 GROUND ELEV. WATER LEVEL INSPECTOR S. Bean

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	CLAYSTONE (continued)			Grout Slope Indicator	98 (91)	16.2		
	COAL, v. weak, s.l., weathered, bl.							
21	CLAYSTONE, as above			-thinly bedded, highly fr. -medium bedded	21.0	15.4		21
	End of hole at 21.0m							
22	<u>Water level table</u> Aug. 19/85 9.4m							22
23								23
24								24
25								25

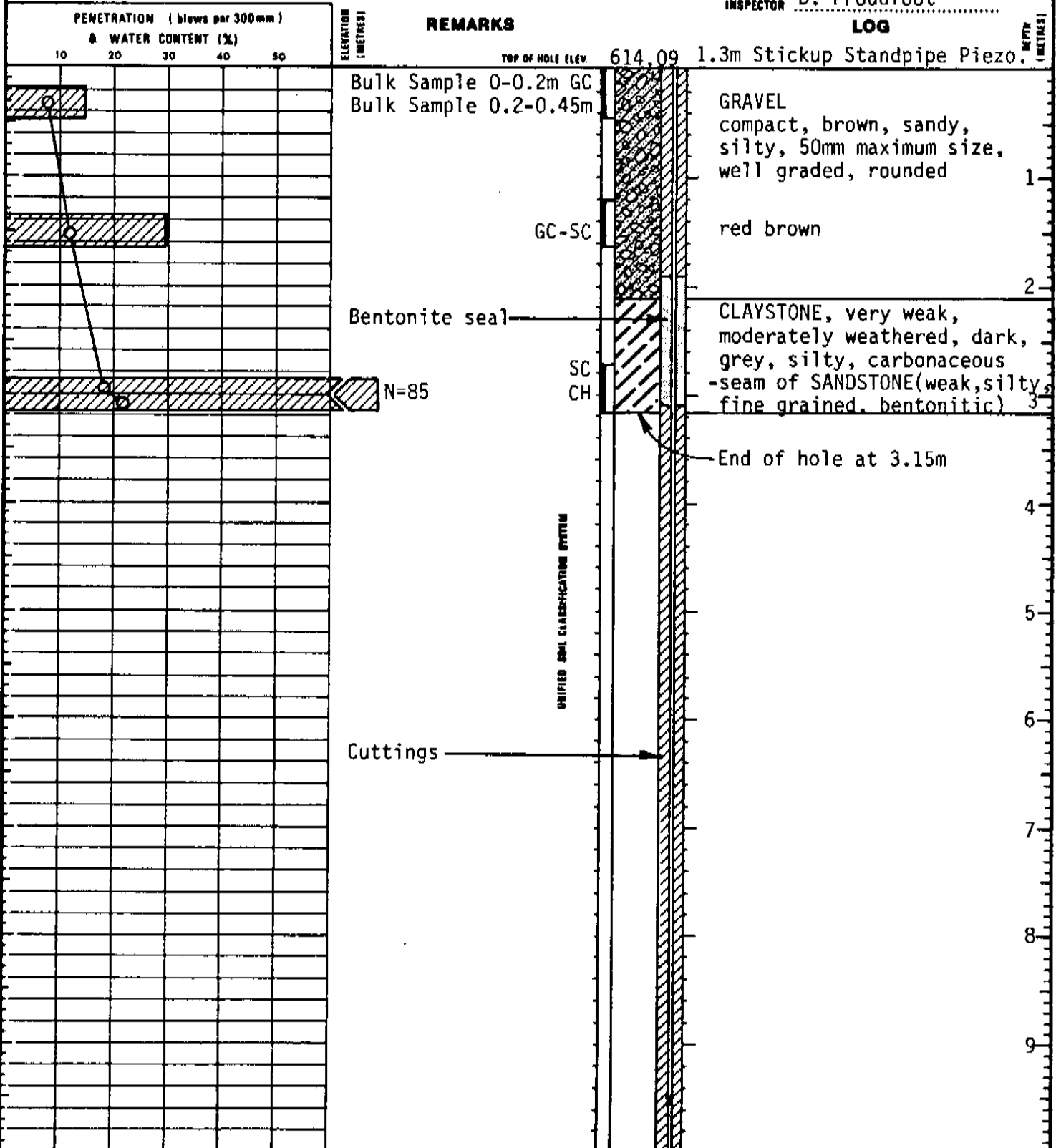
LOG OF TEST HOLE

LOCATION
N5933077.8, E32469.1

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT - NORTH
SASKATCHEWAN RIVER CROSSING

LEGEND:
SAMPLES: Disturbed Undisturbed No recovery
WATER CONTENT:
WATER LEVEL
LIQUID LIMIT
PLASTIC LIMIT

DATE May 16/85
METHOD Mayhew 1000-Mud Rotary
DRILLING CO Garrity and Baker
INSPECTOR D. Proudfoot



LOG OF TEST HOLE CORING

LOCATION	N5933077.8, E32469.1	CLIENT	THE CITY OF EDMONTON
RIG TYPE	Mayhew 1000	PROJECT	SLRT PROJECT
BIT	143mm Tricone	DATE	May 16/85
CASING DIA.	171mm @ to 4.0m	DRILLING CO.	Garrity & Baker
CORE BARREL	Christiansen	CORE DIA.	75mm
GROUND ELEV.	614.09m	INSPECTOR	D. Proudfoot
WATER LEVEL			

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INST. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
1				Standpipe Piezometer Installation 1.3m Stickup				1
2				Bentonite seal				2
3				Cuttings				3
4	T85-R1 START OF CORING AT 4.34m				4.34			4
5	CLAYSTONE very weak, silty, moderately weathered, occasional coal parting and siltstone/ironstone stringers, dark grey			-horizontal bedding, occasional vertical fractures -fracture: 55°, planar, closed -shear: 35°, slickensided	58 (58)	16.2 16.8	Wp=23%, W _L =121% Ip=98%	5
6				-thickly bedded			%SAND= 3.0 %SILT=52.0 %CLAY=45.0 E=375-559MPa Cu=708kPa γ =21.16kN/m ³ SO ₄ =0.00%	6
7	-slightly weathered				6.81	20.3		7
8				-joint: 70°. planar, rough -2 joints: 70°-80°, rough, 1 shear, 50°, slickensided	73 (73)	18.4		8
9	-carbonaceous, black				8.15	17.0		9
	BENTONITE, light grey-green				104 (100)	20.4		
	SILTSTONE			-thinly bedded	9.52	58.2	C _{pen} =70-140kPa W _p =41%, W _L =588% Ip=544%	
10						58.0		10

LOG OF TEST HOLE CORING

LOCATION CLIENT THE CITY OF EDMONTON
 PROJECT SLRT. PROJECT
 NORTH SASKATCHEWAN RIVER CROSSING.
 RIG TYPE
 BIT CASING DIA. DATE May 16/85
 CORE BARREL CORE OIA. DRILLING CO. Garrity & Baker
 GROUND ELEV. WATER LEVEL INSPECTOR D. Proudfoot

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INST. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (ROD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
11	SILTSTONE (continued) very weak, silty to sandy, trace of clay, carbonaceous, slightly weathered, some coal partings, brownish grey			-medium bedded -joint: 70°, planar, rough -joint: 45°, planar, rough -joint: 65°, planar, rough	95 (95)	24.2 10.7 28.5		11
12	SANDSTONE very weak, fine to very fine grained, silty, bentonitic, slightly weathered, light grey -moderately strong				12.57	22.7 5.7		12
13	CLAYSTONE very weak, silty, slightly weathered, some bentonitic partings, dark grey			-horizontal bedding, (some bedding plane fractures)		14.5		13
	COAL, black, claystone seams					14.8		
14	CLAYSTONE very weak, silty, slightly weathered, coal partings, dark brown					28.3		14
				Cuttings	92 (92)	15.9		
15	SANDSTONE very weak, fine to very fine grained, bentonitic, slightly weathered, occasional claystone lamination, light grey			-medium bedded -laminations at 5° to horizontal	15.62	14.3 18.5		15
16	SILTSTONE, very weak, clayey, trace of sand, slightly weathered							16
	CLAYSTONE, very weak, silty, slightly weathered, sandstone layers, 100mm					14.2		
17	SANDSTONE very weak, silty, bentonitic, locally calcareous, slightly weathered, light grey					14.8		17
18				Frac sand		23.3		18
	COAL, black, slightly weathered			-fractured and jointed core	18.66	29.2 27.0		
19	CLAYSTONE very weak, silty, carbonaceous, slightly weathered, coal stringers, dark brown			-thickly bedded -sub-horizontal joint, planar, rough -joints: 100mm intervals, 30°-70°, planar, rough to smooth (to bottom)		20.6		19
20						17.1		20

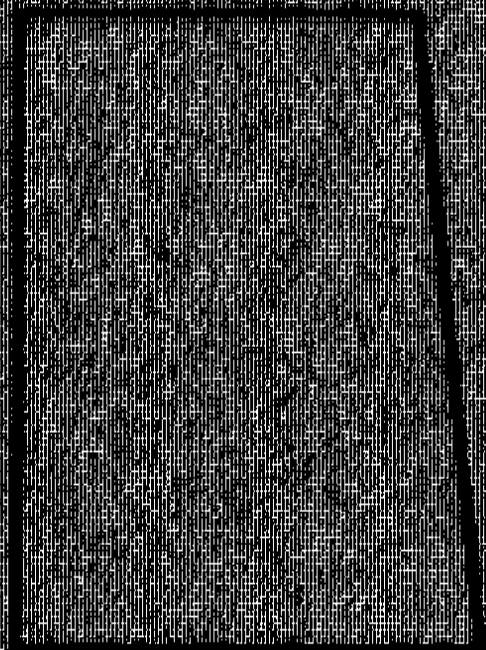
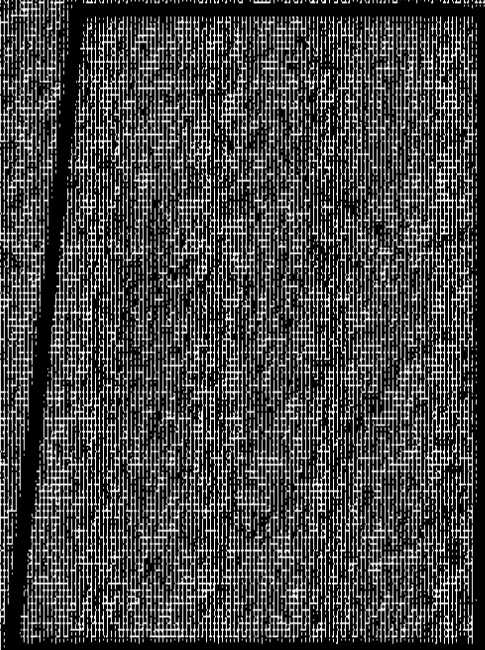
LOG OF TEST HOLE CORING

LOCATION	CLIENT THE CITY OF EDMONTON
.....	PROJECT SLRT PROJECT
RIG TYPE	NORTH SASKATCHEWAN RIVER CROSSING
BIT	DATE May 16/85
CASING DIA.	DRILLING CO. Garrity & Baker
CORE BARREL	INSPECTOR D. Proudfoot
CORE DIA.	
GROUND ELEV.	
WATER LEVEL	

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (ROD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	CLAYSTONE, (continued)			of hole), occasional slickenside	97 (97)	16.0		
	SANDSTONE, very weak, silty, bentonitic			Frac sand -thinly bedded		16.0		
21	CLAYSTONE very weak, silty, slightly weathered, greyish brown			Piezometer tip		17.3		21
				Slough		17.6		
					21.72			
22	End of hole at 21.72m						Water level table	22
							June 7/85 0.0m	
							June 28/85 0.75m above ground surface	
23							July 4/85 0.75m above ground surface	23
							July 19/85 0.75m above ground surface	
24								24
25								25

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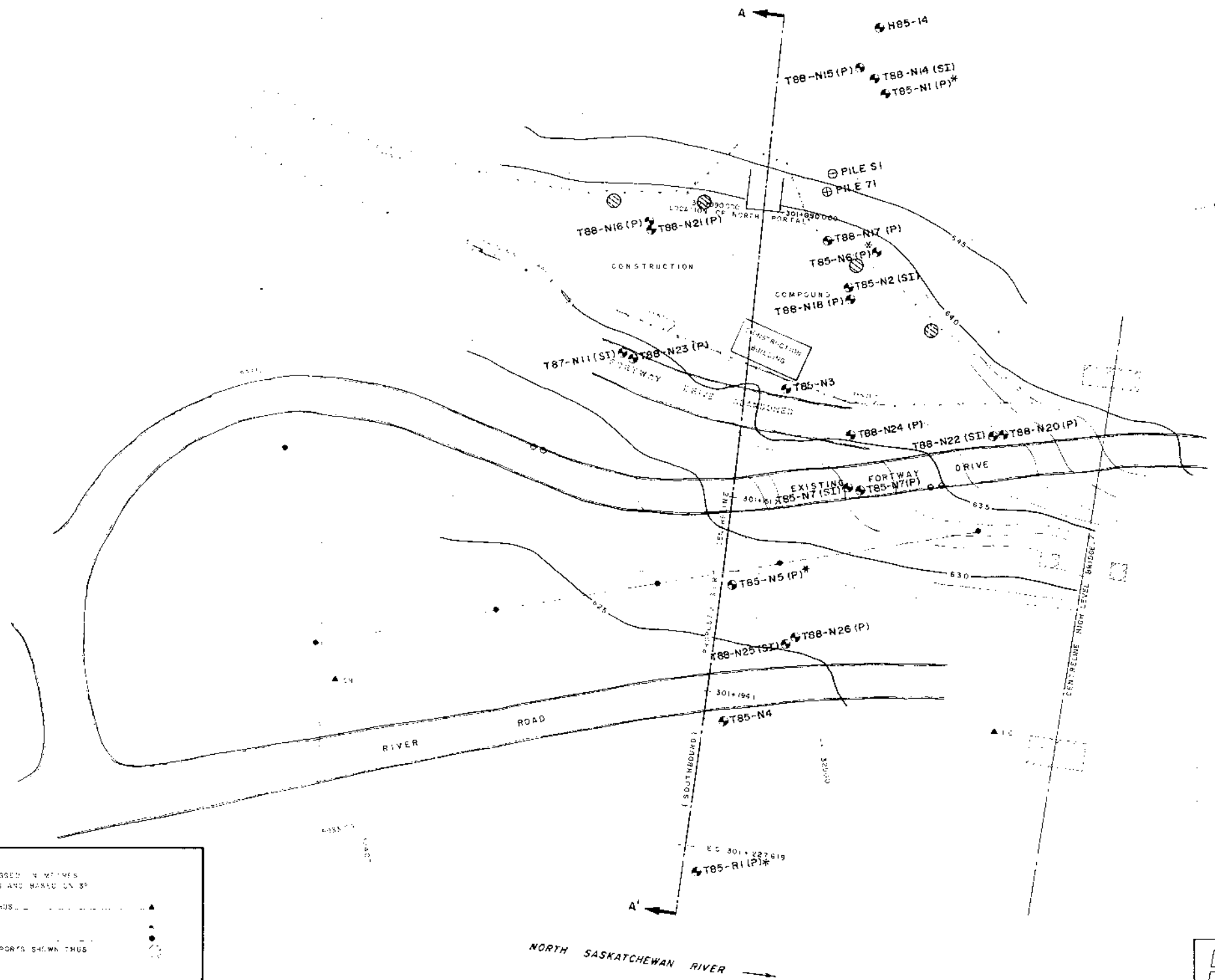
**SOUTH LIGHT RAIL TRANSIT EXTENSION - PHASE
NORTH VALLEY SLOPE AND PORTAL AREA
SLOPE STABILITY AND MONITORING SUMMARY
GEOTECHNICAL REPORT NO. 16**



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THURBER CONSULTANTS



NOTE: TEST HOLE LOCATIONS AND CONTOUR INFORMATION SURVEYED BY COORDINATE SURVEYS LTD. BASE PLAN SUPPLIED BY STANLEY ASSOCIATES ENGINEERING LTD.

- LEGEND:
- ⊕ TEST HOLE LOCATION
 - ⊕ PILE LOCATION (SUBSTATION CONSTRUCTION)
 - (P) PNEUMATIC or STANDPIPE PIEZOMETER INSTALL.
 - * PIEZOMETER NO LONGER BEING MONITORED
 - (SI) SLOPE INDICATOR INSTALLATION
 - ⊗ PROPOSED LOCATION FOR DEWATERING WELL INSTALLATION

LEGEND

ELEVATIONS ARE DECIMAL AND EXPRESSED IN METRES. REFERENCE GRID IS EXPRESSED IN METRES AND BASED ON ST. TRANSVERSE MERCATOR PROJECTION.

SI (SI) CONCRETE MONUMENTS SHOWN THUS

VALVES ARE SHOWN THUS

CATCH BASINS ARE SHOWN THUS

POWER POLES ARE SHOWN THUS

CONCRETE FOUNDATIONS FOR BRIDGE SUPPORTS SHOWN THUS

		THE CITY OF EDMONTON SURT PROJECT-PHASE II NORTH SLOPE - TEST HOLE AND INSTRUMENTATION LOCATIONS NORTH PORTAL SLOPE INVESTIGATION	DATE: Nov. 1988 DRAWN BY: RCC SCALE: 1:500
--	--	---	--

18			9						
17			8						
16			7						
15			6						
14			5						
13			4						
12			3						
11			2						
10			1	ISSUED	5/04/87				
NO.	DESCRIPTION	DATE	APPR.	NO.	DESCRIPTION	DATE	APPR.	NO.	DATE
ISSUE DATE		ISSUE DATE		REVISIONS		BY		APPR.	

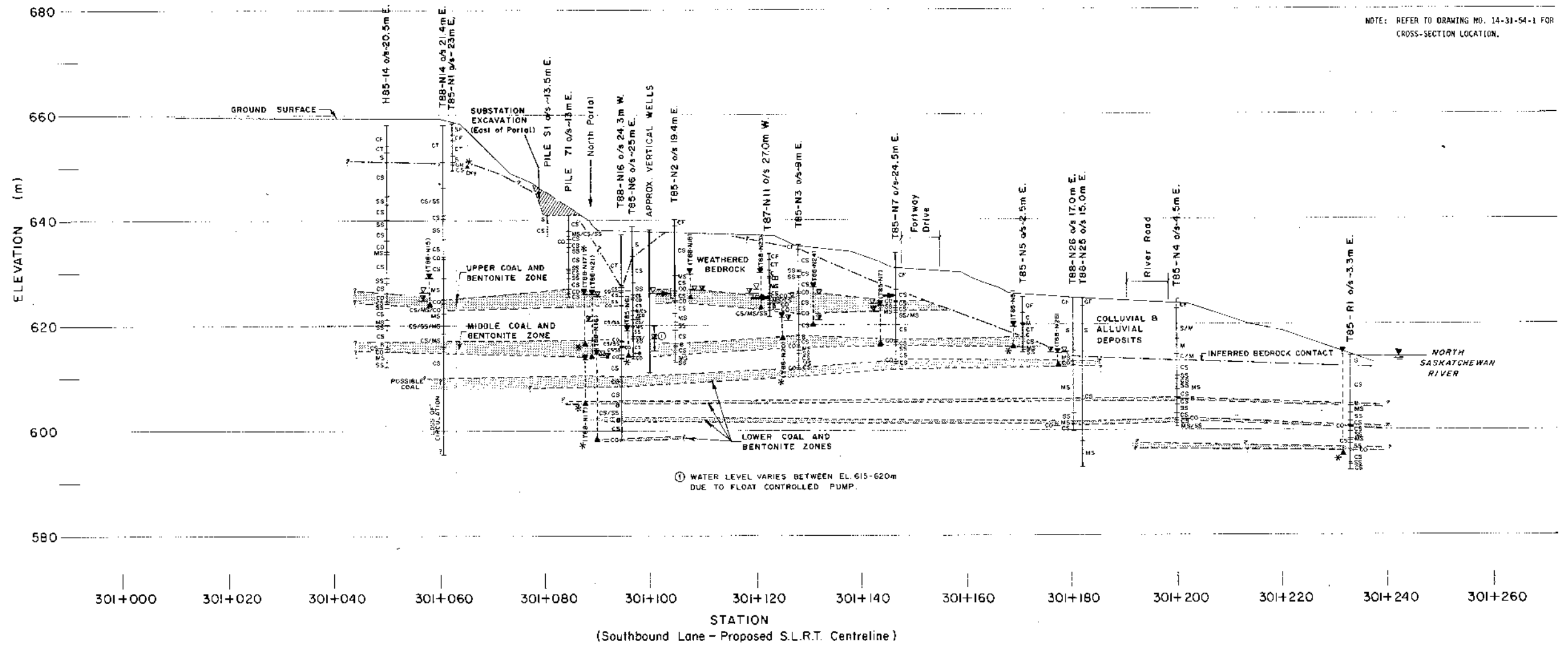
SUB-CONSULTANT	CONSULTANT
	COORDINATE SURVEYS LTD. LAND SURVEYORS
DESIGNED BY:	DATE:
DRAWN BY: R. THORSEN	DATE:
SCALE: 1:500	PERMIT:
CONSULTANT REFERENCE NO.:	SEAL:

STANLEY ASSOCIATES ENGINEERING LTD. Managing Consultants	TRANSPORTATION DEPARTMENT ACCEPTED FOR FINAL DESIGN TRANSIT: _____ TRANSPORTATION PLANNING: _____ L.R.T. PROJECT ADMINISTRATION: _____ BRANCH MANAGER: _____ TRANSPORTATION DEPARTMENT ACCEPTED FOR CONTRACT TENDERING L.R.T. PROJECT ADMINISTRATION: _____ BRANCH MANAGER: _____
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TRANSPORTATION DEPARTMENT ENGINEERING DIVISION DESIGN AND CONSTRUCTION BRANCH	SOUTH LIGHT RAIL TRANSIT - PHASE II TOPOGRAPHIC SURVEY FOR VALLEY STRUCTURES
CONTRACT NO. _____ DRAWING NO. S02-1-P-731 SHEET 01	

LEGEND:	
SYMBOL	DESCRIPTION
C	CLAY
CT	CLAY (FILL)
M	SILT
S	SAND
G	GRAVEL
CF	CLAY FILL
SF	SAND FILL
CS	CLAYSTONE
MS	SILTSTONE
SS	SANDSTONE
CO	COAL
B	BENTONITE
--- ---	INTERBEDDED OR LAYERED STRATA
→	MOVEMENT NOTED SLOPE INDICATOR (SI)
▽	WATER LEVEL OBSERVATION
▲	PIEZOMETER TIP ELEVATION
*	PIEZOMETERS NO LONGER BEING MONITORED

NOTE: REFER TO DRAWING NO. 14-31-54-1 FOR CROSS-SECTION LOCATION.



① WATER LEVEL VARIES BETWEEN EL. 615-620m DUE TO FLOAT CONTROLLED PUMP.

LEGEND FOR PIEZOMETRIC LEVELS

▽	BEFORE WELL INSTALLATION (MARCH-APRIL 1989)
▽	AFTER WELL INSTALLATION (BEFORE PUMPING - JUNE 1989)
▽	AFTER PUMPING (JAN. 1990)

NO	DATE	DESCRIPTION	BY	APPR.
R2	27-02-90	UPDATED PIEZOMETRIC LEVELS	BR	AM
R1	25-01-90	DEEP WELL AS-BUILT LOCATIONS	LMK	AM
NO				

	THE CITY OF EDMONTON	
	SLRT PROJECT - PHASE II	
	NORTH SLOPE -	NOV. 1988
	STRATIGRAPHIC CROSS-SECTION A-A' NORTH PORTAL SLOPE INVESTIGATION	1:400
THURBER CONSULTANTS LTD. Geotechnical Engineers		14-31-54-2 R2

LOG OF TEST HOLE

LOCATION
N5933122.70 E32495.92

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT PHASE II
NORTH SLOPE INVESTIGATION

DATE September 9, 1988

METHOD Wet Rotary

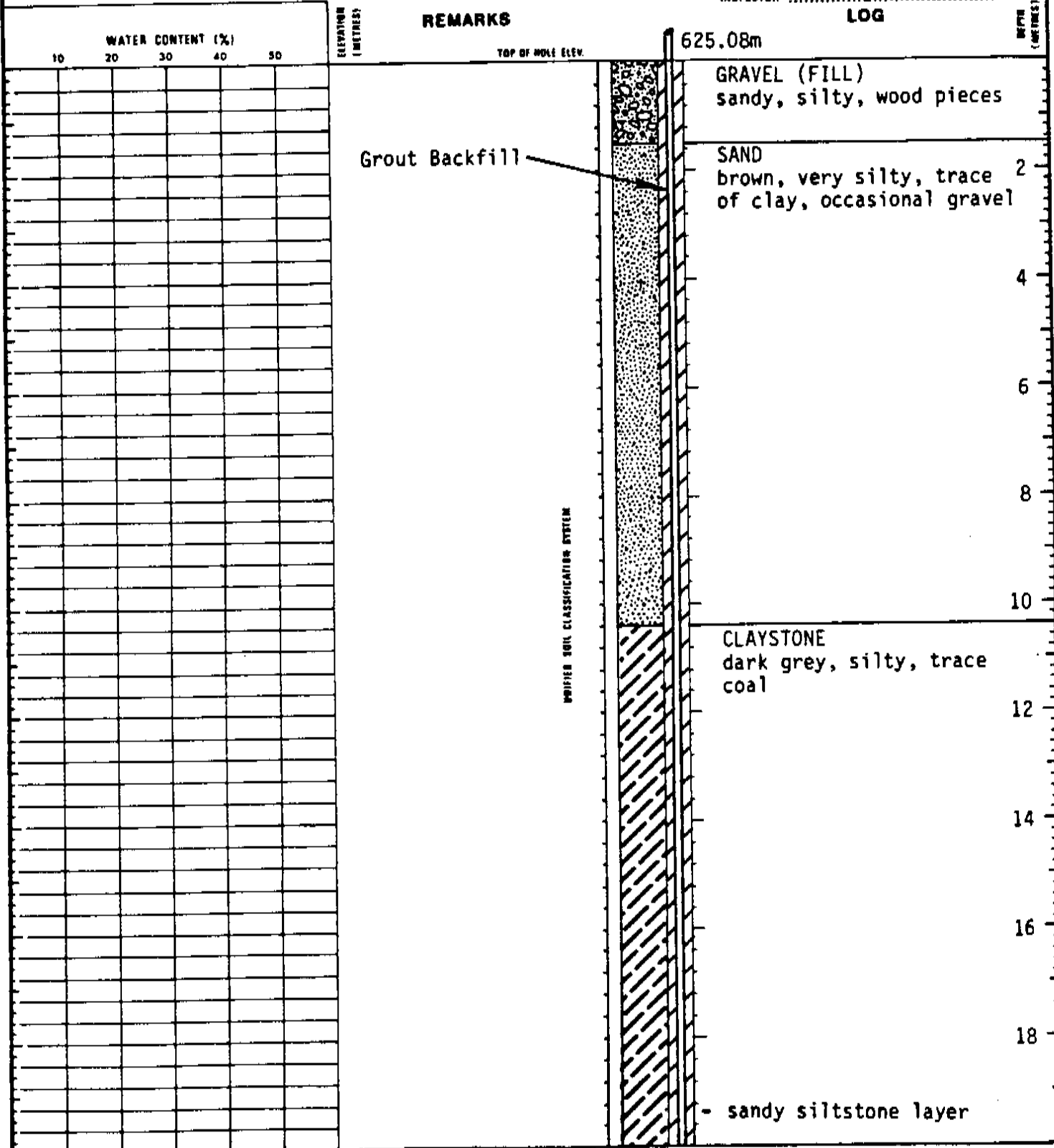
DRILLING BY Garritty & Baker

INSPECTOR J. Craplewe

LEGEND:
 SAMPLES: Disturbed Water Content
 Undisturbed Liquid Limit
 No recovery Plastic Limit
 WATER LEVEL
 LIQUID LIMIT
 PLASTIC LIMIT

REMARKS

LOG



LOG OF TEST HOLE

LOCATION

.....

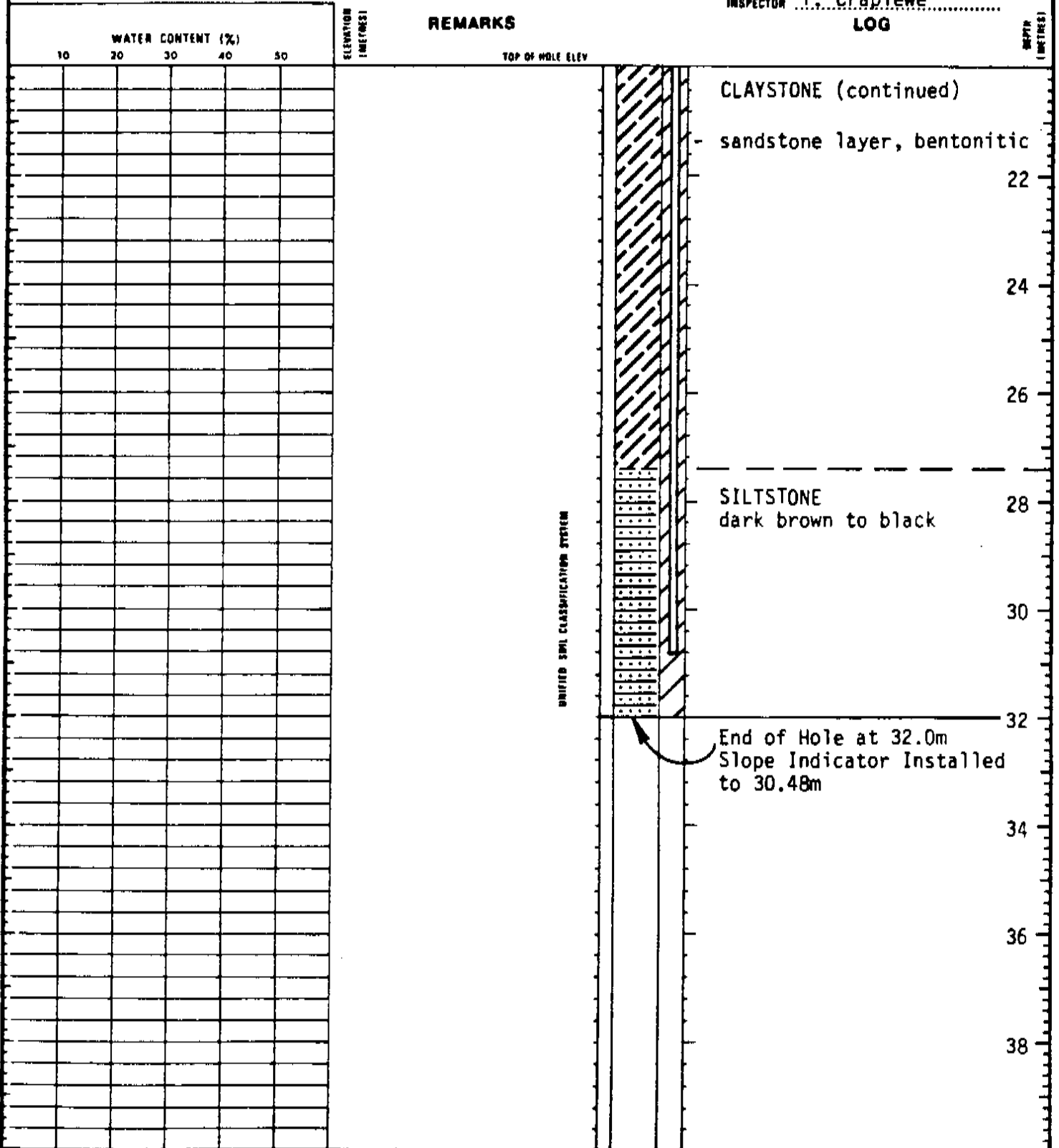
.....

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT PHASE II
NORTH SLOPE INVESTIGATION
DATE September 9, 1988
METHOD Wet Rotary
DRILLING CO Garritty & Baker
INSPECTOR T. Craplewe

- LEGEND:
- SAMPLES: Disturbed Undisturbed No recovery
- WATER CONTENT:
- WATER LEVEL ∇
- W_L LIQUID LIMIT
- W_p PLASTIC LIMIT

REMARKS

LOG



UNITED SOIL CLASSIFICATION SYSTEM

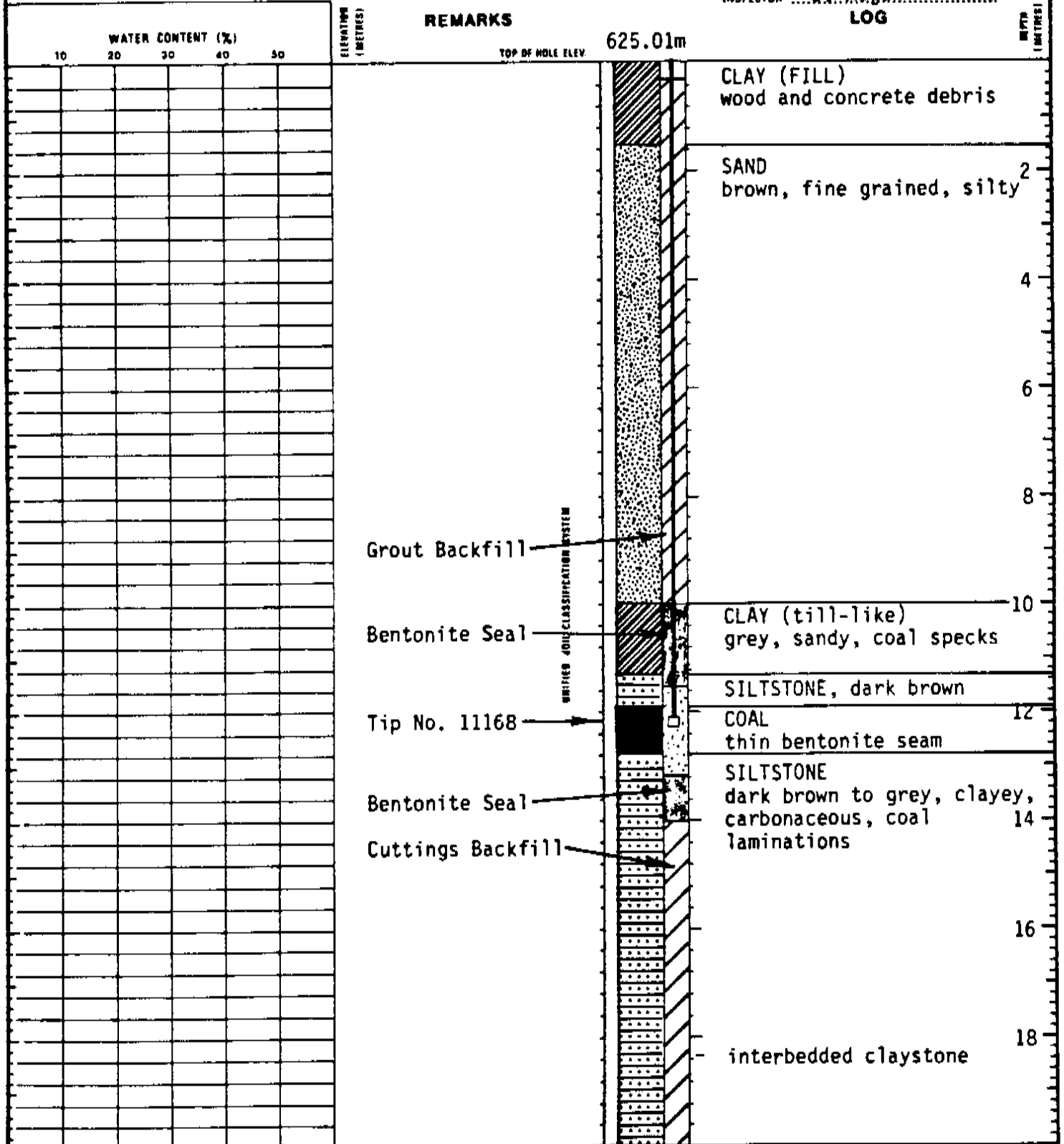
LOG OF TEST HOLE

LOCATION
N5933123.78 E32498.38

CLIENT THE CITY OF EDMONTON
PROJECT SLRT PROJECT PHASE II
NORTH SLOPE INVESTIGATION

DATE September 14, 1988
METHOD Wet Rotary
DRILLING BY Garritty & Baker
INSPECTOR J. Hogan

LEGEND:
SAMPLES: Disturbed Undisturbed No recovery
WATER CONTENT:
WATER LEVEL
LIQUID LIMIT
PLASTIC LIMIT



LOG OF TEST HOLE

LOCATION

.....

.....

CLIENT THE CITY OF EDMONTON

PROJECT SLRT PROJECT PHASE II
NORTH SLOPE INVESTIGATION

DATE September 14, 1988

METHOD Wet Rotary

DRILLING CO Garritty & Baker

INSPECTOR J. Hogan

LOG

LEGEND:

SAMPLES: Disturbed WATER CONTENT: ○

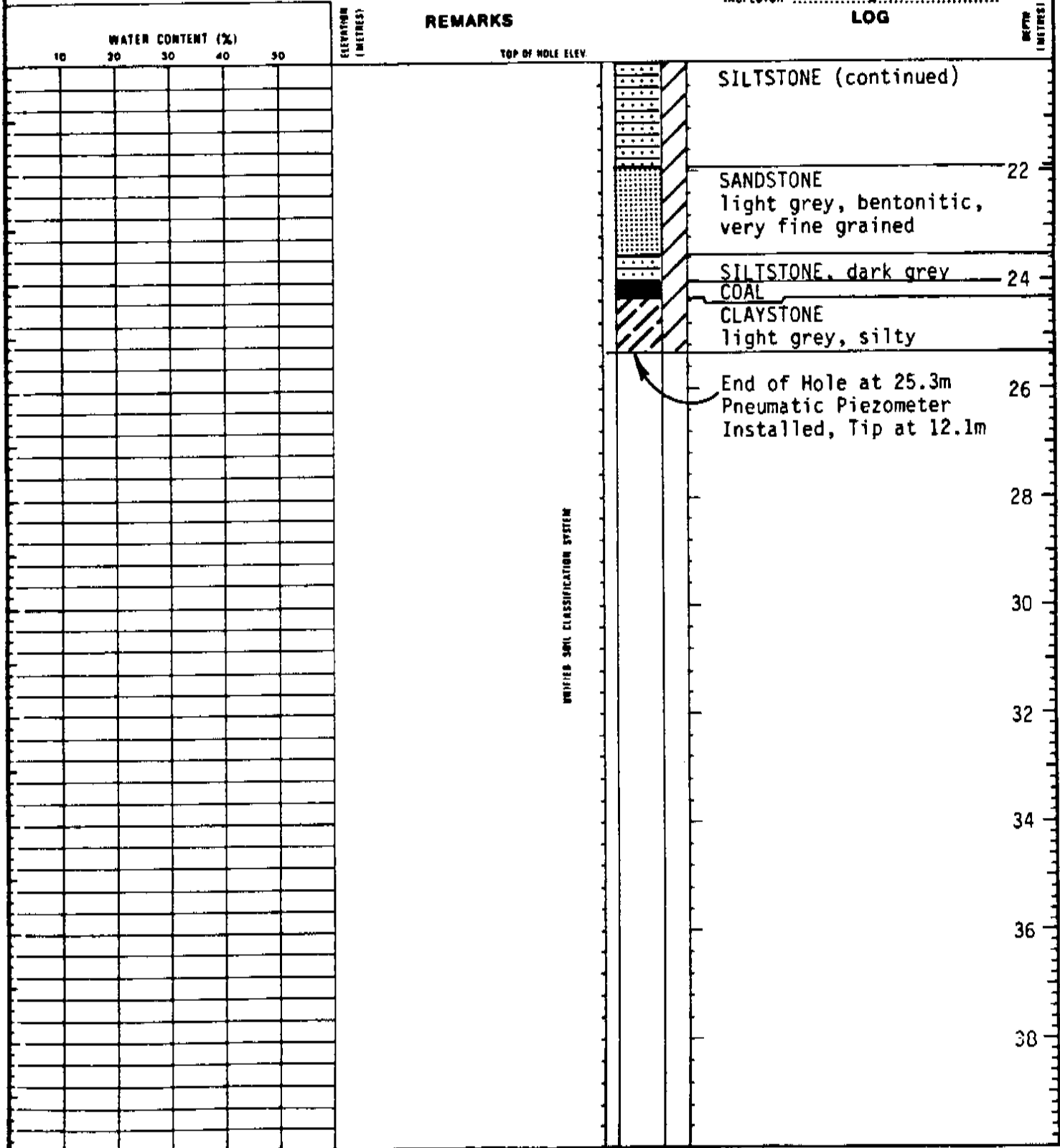
Undisturbed ●

No toughness

⇩ WATER LEVEL

— LIQUID LIMIT

— PLASTIC LIMIT

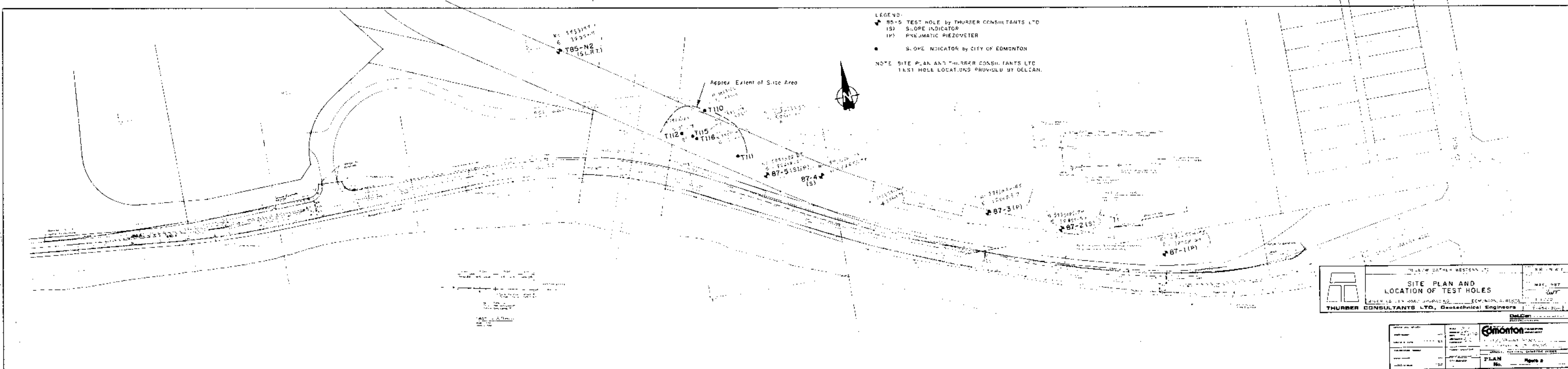


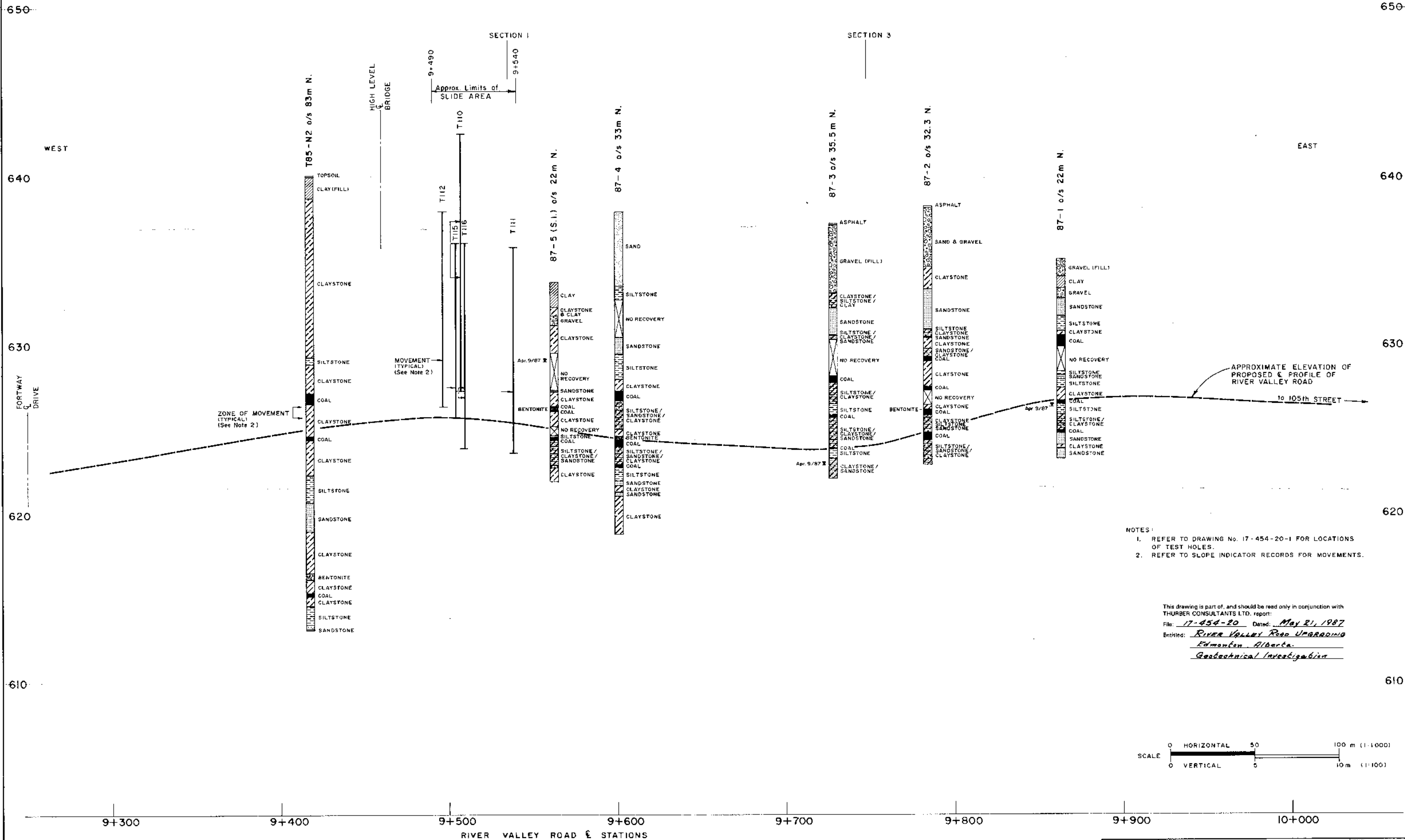
011-36-16-10

RIVER VALLEY ROAD OPERATIONS
EDMONTON, ALBERTA
CONTRACT NO. 011-36-16-10

THORBER CONSULTANTS

011-36-16-10





- NOTES:
1. REFER TO DRAWING No. 17-454-20-1 FOR LOCATIONS OF TEST HOLES.
 2. REFER TO SLOPE INDICATOR RECORDS FOR MOVEMENTS.

This drawing is part of, and should be read only in conjunction with THURBER CONSULTANTS LTD. report:
 File: 17-454-20 Dated: May 21, 1987
 Entitled: RIVER VALLEY ROAD UPGRADE
Edmonton, Alberta.
Geotechnical Investigation



	DELEW, CATHER, WESTERN LTD.	BR/GEG/RWT
	STRATIGRAPHIC PROFILE	
	RIVER VALLEY ROAD UPGRADE	EDMONTON, ALBERTA
	THURBER CONSULTANTS LTD., Geotechnical Engineers	
		DATE: MAY, 1987
		BY: <i>RWT</i>
		AS SHOWN
		17-454-20-2

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1
 N 5932974.95, E 32928.67

CLIENT DELEUW, CATHER, WESTERN LTD.
 PROJECT RIVER VALLEY ROAD UPGRADING

RIG TYPE Mayhew 1500

DATE March 4, 1987

BIT CASING DIA.

DRILLING CO. Garritty & Baker

CORE BARREL Christensen CORE DIA. 75 mm Nom.

INSPECTOR J. Hogan

GROUND ELEV. 635.03m WATER LEVEL

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
1	GRAVEL (FILL) sandy, brown, brick rubble, extensive coal inclusions			Pneumatic Piezometer installation				1
1	CLAY brown, gravelly							
2	GRAVEL, clayey, pebbles to 40mm					13.4	Sample 1 (Tube)	2
3	SANDSTONE bentonitic, silty, grey, fine grained					26.3		3
3.35	START OF CORING AT 3.35m				3.35			
4	SILTSTONE weak, bentonitic, grey, fresh, claystone laminations, coal and sandstone laminations			-randomly jointed -thickly bedded	100 (64)	18.9 15.4		4
4.25	CLAYSTONE, weak, grey, fresh			-medium bedded	4.25			
5	COAL weak, black, fresh, occasional carbonaceous claystone lamin.			-thickly bedded		16.8 23.3		5
6	NO RECOVERY							6
6.65	SILTSTONE, weak, clayey, brown to grey			-very thinly to thinly bedded	6.65			
7	SANDSTONE, weak, silty, f. grain.					14.5		7
8	SILTSTONE, weak, clayey, grey, fresh, claystone laminations					15.4		
8	CLAYSTONE, weak, grey, fresh, carbonaceous -mod. strong ironstone layer				92 (8)	17.1	LL=101.4% PL= 30.7% PI= 71%	8
9	COAL, weak, black, fresh			W.L. Apr. 9/87		24.2		
9	SILTSTONE weak, clayey, grey, fresh, carbonaceous			-medium bedded to thinly bedded	9.1			9
10	SANDSTONE, siltstone laminations					13.4		
10	CLAYSTONE, very silty, grey					16.5		
10	SILTSTONE, weak to moderately strong, clayey, trace f. sand			-medium bedded				10

LOG OF TEST HOLE CORING

LOCATION: See Drawing No. 17-454-20-1.....

CLIENT: DELEUW, CATHER, WESTERN LTD.

PROJECT: RIVER VALLEY ROAD UPGRADING

RIG TYPE: Mayhew 1500

BIT:

CORE BARREL: Christensen

GROUND ELEV:

CASING DIA:

CORE DIA: 75 mm Nom.

WATER LEVEL:

DATE: March 4, 1987

DRILLING CO: Garritty & Baker

INSPECTOR: J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	SILTSTONE (continued)							
	COAL, moderately strong, fresh			-thinly bedded -vertical fracture		18.1		
	SANDSTONE moderately strong, bentonitic, fine grained, grey, fresh			-thickly bedded	99 (41)	14.2		
11	CLAYSTONE			-thinly bedded		12.8		11
	SANDSTONE fine grained, siltstone interbeds			-thickly bedded	11.8	14.9		
12	End of coring at 11.8m			Pneumatic Piezometer Tip No. 7182				12
13								13
14								14
15								15
16								16
17								17
18								18
19								19
20								20

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1
 N. 5933005.74, E. 32857.50
 RIG TYPE Mayhew 150D
 BIT CASING DIA.
 CORE BARREL Christensen CORE DIA. 75 mm Nom.
 GROUND ELEV 638.20m WATER LEVEL

CLIENT DELEUW, CATHER, WESTERN LTD.
 PROJECT RIVER VALLEY ROAD UPGRADING
 DATE March 7, 1987
 DRILLING CO. Garritty & Baker
 INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INST. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
0	ASPHALT							0
1	SAND and GRAVEL silt layers			Slope Indicator Installation				1
2								2
3								3
4	CLAYSTONE, grey, weathered							4
4.9	START OF CORING AT 4.9m				4.9			4.9
5	SANDSTONE weak to moderately strong, bentonitic, silty, fine grained, grey, fresh, coal laminations, occasional claystone lamination			-medium to thickly bedded	83 (83)	16.2 17.3		5
6				-vertical fracture	6.1	17.6		6
7						6.2		7
8	SILTSTONE/CLAYSTONE & SANDSTONE very weak, fresh			-medium bedded	87 (56)	19.1		8
8	CLAYSTONE weak to moderately strong, grey, fresh, siltstone laminations			-thickly bedded -joint, rough, planar, 20° TCA		26.5		8
9	SANDSTONE and CLAYSTONE weak, fresh				8.8			9
9	COAL, black			-rubby core		26.0		9
10	CLAYSTONE weak, silty, grey, fresh, occasional siltstone and sandstone laminations			-thinly to thickly bedded		23.3	LL=102% PL= 24% PI= 78%	10

LOG OF TEST HOLE CORING

LOCATION: See Drawing No. 17-454-20-1

CLIENT: DELEUW, CATHER, WESTERN LTD.
 PROJECT: RIVER VALLEY ROAD UPGRADING

RIG TYPE: Mayhew 1500

DATE: March 7, 1987

BIT: CASING DIA.:

DRILLING CO.: Garritty & Baker

CORE BARREL: Christensen CORE DIA.: 75 mm Nom.

INSPECTOR: J. Hogan

GROUND ELEV.: WATER LEVEL:

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	CLAYSTONE (continued)				15.4		
	-sandstone interbed		-medium bedded				
	COAL			69 (23)	25.0		11
11	NO RECOVERY			11.85			
	CLAYSTONE, weak, silty, fresh				22.8		12
12	BENTONITE				40.0		
	COAL						
	CLAYSTONE/SILTSTONE & SANDSTONE interbedded,		-thinly to medium bedded	92 (56)	17.5		13
13	weak, silty, grey, fresh, carbonaceous				17.4		
	COAL, moderately weak, fresh		-medium bedded	13.65	13.6		
	-siltstone interbed				19.7		14
14	SILTSTONE/SANDSTONE & CLAYSTONE interbedded,		-joint, closed, planar, 80° TCA		16.8		
	weak, bentonitic, sandy, brown and grey, fresh, occasional coal stringer		-joint, closed, planar, 75° TCA	110 (82)	16.5		15
15			-medium to thickly bedded, horizontal	15.3	14.4		
16	End of coring at 15.3m						16
17							17
18							18
19							19
20							20

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1
 N. 5933026.85, E. 32807.37
 RIG TYPE Mayhew 1500
 BIT
 CORE BARREL Christensen
 GROUND ELEV. 637.17m

CLIENT DELEUW, CATHER, WESTERN LTD.
 PROJECT RIVER VALLEY ROAD UPGRADING
 DATE March 6, 1987
 DRILLING CO. Garritty & Baker
 INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INST. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
0	ASPHALT							0
1	GRAVEL (FILL) rubble			Pneumatic Piezometer Installation				1
2								2
3								3
4								4
5	CLAYSTONE/SILTSTONE and CLAY grey START OF CORING AT 5.0m				5.0			5
6	SANDSTONE weak, bentonitic, silty, fine to medium grained, grey, fresh, occasional coal stringer			-thickly bedded -joint 20° TCA	74 (63) 5.95	19.3 17.9		6
7	interlaminated SILTSTONE/CLAYSTONE and SANDSTONE, weak to very weak			-joint 70° TCA -thinly bedded		12.0 20.3		7
8	NO RECOVERY				30 (16)			8
9	COAL moderately weak, fresh				9.0	28.2		9
10	interbedded SILTSTONE & CLAYSTONE weak, silty, clayey, grey, fresh			-medium bedded		17.6 17.7		10

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1

CLIENT DELEUW CATHER WESTERN LTD.
 PROJECT RIVER VALLEY ROAD UPGRADING

RIG TYPE Mayhew 1500

BIT CASING DIA.

CORE BARREL Christensen CORE DIA. 75 mm Nom.

GROUND ELEV. WATER LEVEL

DATE March 6, 1987

DRILLING CO. Garritty & Baker

INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	SILTSTONE and CLAYSTONE (cont.)			-medium bedded to thinly bedded		20.5		
11	SILTSTONE clayey, carbonaceous, grey-brn. completely weathered to fresh			-thickly bedded	89 (33)			11
	COAL			-thinly bedded		18.9		
	SILTSTONE and CLAYSTONE			-thinly bedded				
12	NO RECOVERY				12.05			12
	SILTSTONE weak, clayey, grey, fresh			-medium bedded		16.6		
	SANDSTONE, claystone laminations					15.3		
13	interbedded SILTSTONE & CLAYSTONE weak, clayey, silty, grey, fresh, carbonaceous			-thinly to medium bedded		15.2		13
	COAL				90 (66)			
	SILTSTONE weak, clayey, grey, fresh					15.5		
14	SANDSTONE moderately weak, bentonitic			-medium bedded				14
	CLAYSTONE, very weak			-thinly bedded				
	SANDSTONE, weak, bentonitic			-medium bedded		12.5		
15	CLAYSTONE very weak, silty			-thinly bedded	15.1			15
	End of coring at 15.1m							
16								16
17								17
18								18
19								19
20								20

W.L. Apr. 9/87

Pneumatic Piezometer
Tip No. 9780

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1
 N 5933074.22, E 32693.79
 RIG TYPE Mayhew 1500
 BIT
 CORE BARREL Christensen
 GROUND ELEV. 637.84m

CLIENT DELEUW, CATHER, WESTERN LTD.
 PROJECT RIVER VALLEY ROAD UPGRADING
 DATE March 2, 1987
 DRILLING CO. Garritty & Baker
 INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
1	SAND brown, gravelly			Slope Indicator Installation			Sample 1 (Tube)	1
2								2
3	SAND brown, gravelly layers						Sample 2 (Tube)	3
4						4		
5	SILTSTONE grey, clayey START OF CORING AT 5.2m				5.2			5
6	NO RECOVERY				20 (20)			6
7	IRONSTONE					3.3		7
8	SANDSTONE weak, fine grained, bentonitic, fresh, grey, Siltstone laminations, calcareous			-thinly bedded to medium bedded	7.9	19.0		8
9	SILTSTONE weak, bentonitic, fresh, grey, claystone laminations			-numerous multidirectional closed planar joints		7.5		9
				-medium bedded -horizontal bedding	88 (60)	19.5		
10	CLAYSTONE, weak				9.9	18.3		10

**THURBER CONSULTANTS LTD.,
Geotechnical Engineers**

Sheet 2 of 2

TEST HOLE NO.

87-4

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1

CLIENT DELEUW, CATHER, WESTERN LTD.
PROJECT RIVER VALLEY ROAD UPGRADING

RIG TYPE Mayhew 1500

BIT CASING DIA.

CORE BARREL Christensen CORE DIA. 75 mm Nom.

GROUND ELEV. WATER LEVEL

DATE March 2, 1987

DRILLING CO. Garritty & Baker

INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
	CLAYSTONE (continued) weak, silty, grey to brown, fresh bentonitic, ironstone interbeds			-very thinly bedded to medium bedded		15.9	LL=99% PL=32% PI=67%	
11	COAL weak, black, fresh, bentonitic laminations			-vertical fracture 0° TCA -very thinly bedded to medium bedded		33.3 18.1 47.1 37.3 28.3		
	CLAYSTONE, weak, silty, brown, fresh			-medium bedded	82 (40)	14.6		
	SILTSTONE, weak, clayey, gr. fresh			-thinly bedded		10.5		
12	SANDSTONE, weak, fine grained, bentonitic, grey, fresh							
	interlaminated SILTSTONE/CLAYSTONE and SANDSTONE moderately weak, grey, fresh			-thinly to medium bedded	12.9			
13	CLAYSTONE, weak, silty, grey, fresh, carbonaceous					16.7		
	BENTONITE			-joint 85° planar, rough -joint 80° planar, rough		29.2		
	COAL moderately weak, black, fresh					14.4		
14	SILTSTONE weak, brown, fresh, carbonaceous, occasional coal lens			-vertical fracture -medium bedded	103 (71)	14.0		
	interlaminated SILTSTONE/SANDSTONE and CLAYSTONE, weak, grey			-thinly bedded		21.0		
15	COAL			-very thinly bedded		13.4		
	SILTSTONE, moderately weak, grey, fresh, sandstone and claystone interbeds, trace of fine grained sand				15.9			
16	SANDSTONE, weak, fine grained, grey, fresh					15.4		
	CLAYSTONE, weak, grey, fresh			-rough, planar joints -medium bedded		14.4		
	SANDSTONE, moderately weak					17.0		
17	CLAYSTONE weak, silty, grey, fresh, occasional coal laminations			-numerous multidirectional joints, closed, planar -thinly to thickly bedded	102 (49)	17.4		
18						17.0		
				Slope Indicator Installation		18.9		
19								
	End of coring at 19.1m							
20								

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1
(SI) N 5933082.29, E 32654.21 (PP) N 5933083.86, E 32651.59
RIG TYPE Mayhew 1500
BIT CASING DIA.
CORE BARREL Christensen CORE DIA. 75 mm Nom.
GROUND ELEV for S.I. =633.70m WATER LEVEL
for P.P. =633.81m
CLIENT DELEUW CATHER WESTERN LTD.
PROJECT RIVER VALLEY ROAD UPGRADING
DATE March 3, 1987
DRILLING CO. Garritty & Baker
INSPECTOR J. Hogan

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSITR. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
1	CLAY grey-brown, very silty, trace of fine sand, coal fines			Slope Indicator Installation Pneumatic Piezometer Installation				1
	-thin peat layer				63	30.7	Sample 1	
2	CLAYSTONE and CLAY grey-brown, some coal					17.3		2
	GRAVEL grey-brown, clayey, pebbles to 40mm, asphalt rubble					26.8	Sample 2	
3	CLAYSTONE weak, silty, grey to grey-brown, moderately weathered				57	22.1		3
4	START OF CORING AT 4.0m CLAYSTONE, weak, silty, brown, fresh, coal lenses				4.0			4
				-thinly bedded		25.1 18.2		
5	NO RECOVERY			▼W.L. Apr. 9/87				5
6	SANDSTONE, weak, silty, bentonitic, grey, fresh				8 (6)			6
				-thinly bedded	6.4			
7	CLAYSTONE weak, silty, fresh, carbonaceous			-medium bedded		18.1		7
	COAL			-numerous multidirectional joints		19.4		
	BENTONITE					40.6	LL=361 PL= 39 PI=322	
8	CLAYSTONE weak to moderately weak, silty, fresh, carbonaceous, occasional coal stringer			-thinly bedded -thickly bedded	81 (37)	14.7		8
9	NO RECOVERY							
	SILTSTONE				9.1			9
	COAL			-numerous multidirectional joints		12.4 18.8		
10	interbedded SILTSTONE/CLAYSTONE and SANDSTONE weak, grey fresh			-very thinly bedded to medium bedded		16.8		10

LOG OF TEST HOLE CORING

LOCATION See Drawing No. 17-454-20-1.....

CLIENT DELEUW, CATHER, WESTERN LTD.....
 PROJECT RIVER VALLEY ROAD UPGRADING.....

RIG TYPE Mayhew 1500.....

DATE March 3, 1987.....

BIT CASING DIA.

DRILLING CO. Garritty & Baker.....

CORE BARREL Christensen CORE DIA. 75 mm Nom.

GROUND ELEV. WATER LEVEL

INSPECTOR J. Hogan.....

DEPTH (METRES)	ROCK DESCRIPTION type, strength, grain, size, weathering, colour	ROCK TYPE	INSTA. DETAILS	DISCONTINUITIES DESCRIPTION joints, bedding, seams, faults, spacing, attitude, smoothness	Recovery (RQD) (%)	Wn (%)	TEST RESULTS	DEPTH (METRES)
11	SANDSTONE, weak, silty, bentonitic, grey			-medium bedded		12.7		
	SILTSTONE, moderately weak, clayey, tr. fine gr. sand, gr. fresh							
11	SANDSTONE, strong, silty, grey, fresh					6.6		11
	CLAYSTONE weak, silty, grey, fresh			Slope Indicator Installation	11.8			
12	End of coring at 11.8m							12
13								13
14								14
15								15
16								16
17								17
18								18
19								19
20								20

January 28, 2011

CAD: 931+36+16

TO: Engineering Services Library

FROM: Christina Tatarniuk, P.Eng., Research Engineer
Engineering Services, Transportation Operations

SUBJECT: **Slope Inclinometer Installation**
Fortway Drive near 109 Street
East of the High Level Bridge

INTRODUCTION

A slope inclinometer (SI) was installed by Engineering Services at the above-noted monitoring site on September 16, 2010. The location of the slope inclinometer, denoted SI 10-01, is shown on Figure 1 in Appendix A. SI 10-01 was installed on Fortway Drive, approximately 50m east of the High Level Bridge. This inclinometer was installed to replace SI-110, which was no longer operational. SI 10-01 was installed in the roadway to facilitate monitoring of ground movements below this section of Fortway Drive.

The surveyed coordinates of SI 10-01 were N 5933359.00 and E 32551.27, with a corresponding ground elevation of 642.628 m; the survey data sheet is included in Appendix A and shows the surveyed coordinate information for both SI 10-01 and the original SI-110.

BACKGROUND

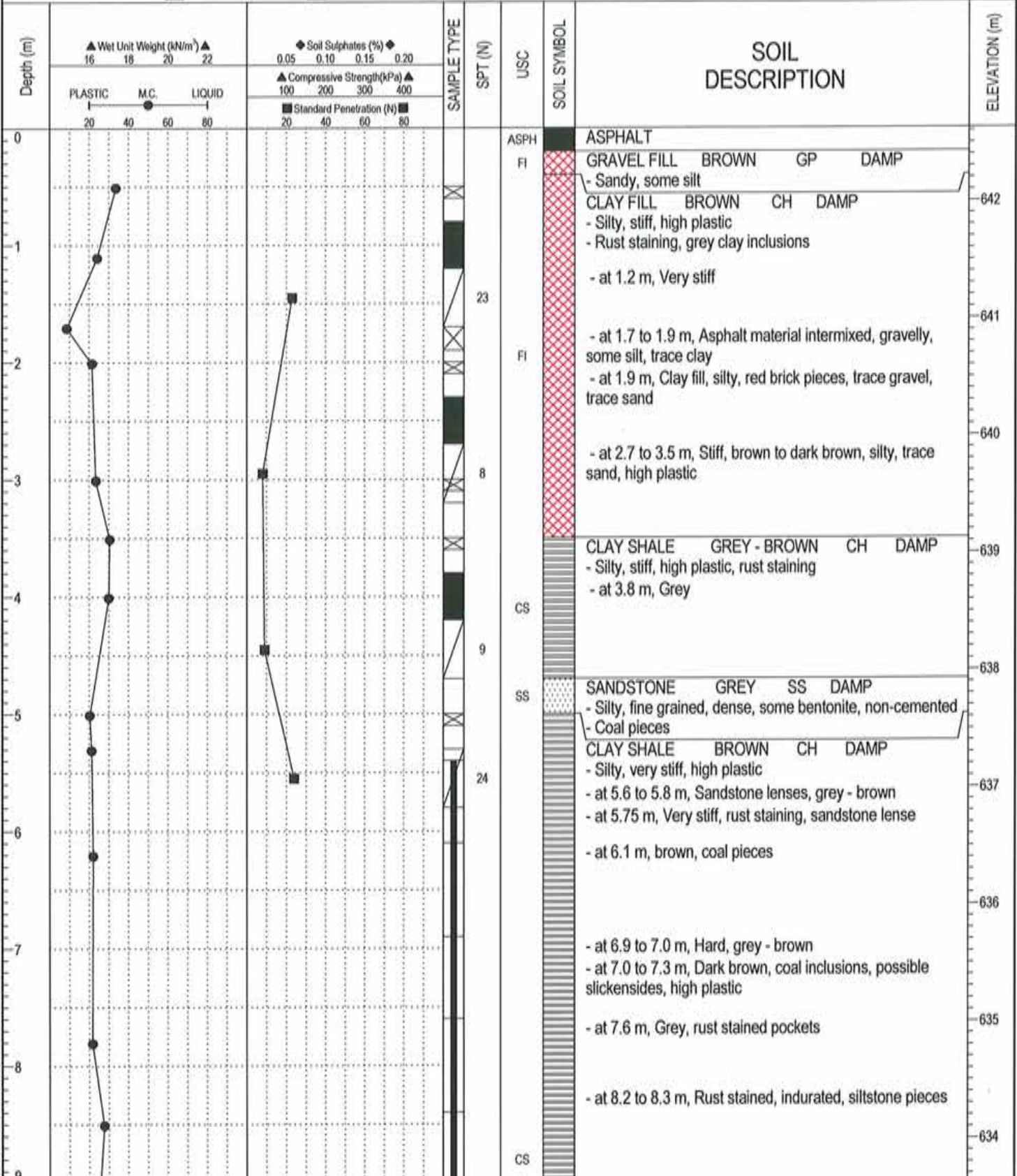
Fortway Drive is a low-volume road which connects River Valley Road to the Legislative Grounds to the north and 107 Street to the east. Fortway Drive traverses along the slopes and an upper terrace level of the North Saskatchewan River valley, upslope of River Valley Road. Records of borehole logs from the Engineering Services Library indicate that slope inclinometers were installed in the area between 1978 and 1985. A slope stability evaluation report for the site was prepared by Thurber Consultants Ltd., dated August 1986.

Engineering Services currently monitors 4 slope inclinometers at the Fortway Drive Site in addition to SI 10-01. These inclinometers were denoted SI-111, SI-113, SI-115, and SI-118. The locations of these remaining operational instruments at the site are also shown on Figure 1 in Appendix A.



Fortway Drive SI 10-01 Installation	Fortway Drive, East of the High Level Bridge	BOREHOLE NO: 10-01
City of Edmonton, Engineering Services	UTM ZONE: - N5933359 E32551.27	PROJECT NO: 50001472-0010
START DATE: 9/15/2010	931+36+16	ELEVATION: 642.628 m

SAMPLE TYPE Shelby Tube Drive Sample Auger Sample No Recovery A-Casing Cored Sample



GEO/TECH SI 10-01.GPJ EDMONTON.GDT 11/27/11



Transportation Department
Engineering Services Section

LOGGED BY: DD

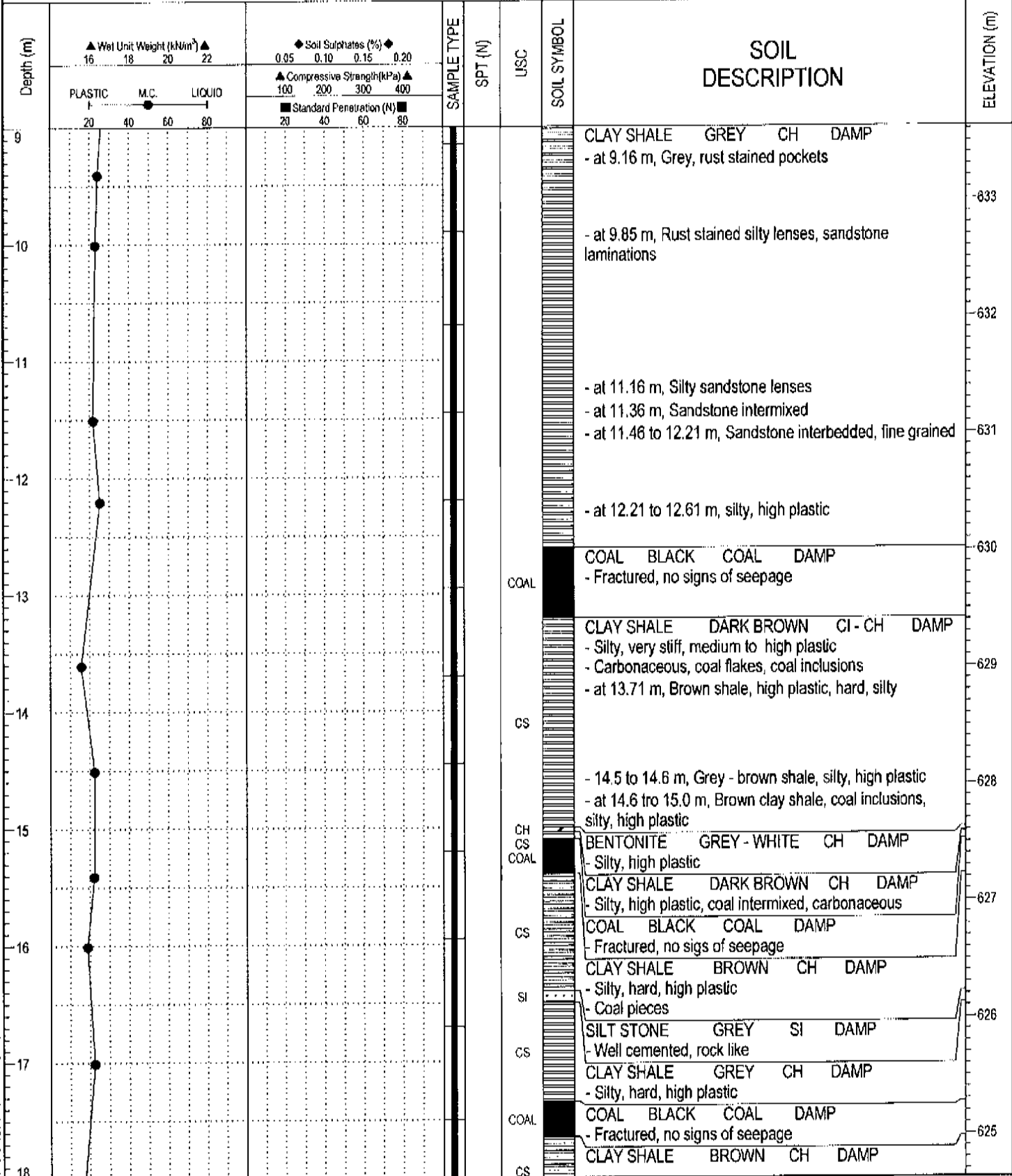
REVIEWED BY: KMT

COMPLETION DEPTH: 21.40 m

COMPLETION DATE: 2010/09/16

Fortway Drive SI 10-01 Installation	Fortway Drive, East of the High Level Bridge	BOREHOLE NO: 10-01
City of Edmonton, Engineering Services	UTM ZONE: - N5933359 E32551.27	PROJECT NO: 50001472-0010
START DATE: 9/15/2010	931+36+16	ELEVATION: 642.628 m

SAMPLE TYPE Shelby Tube Drive Sample Auger Sample No Recovery A-Casing Cored Sample



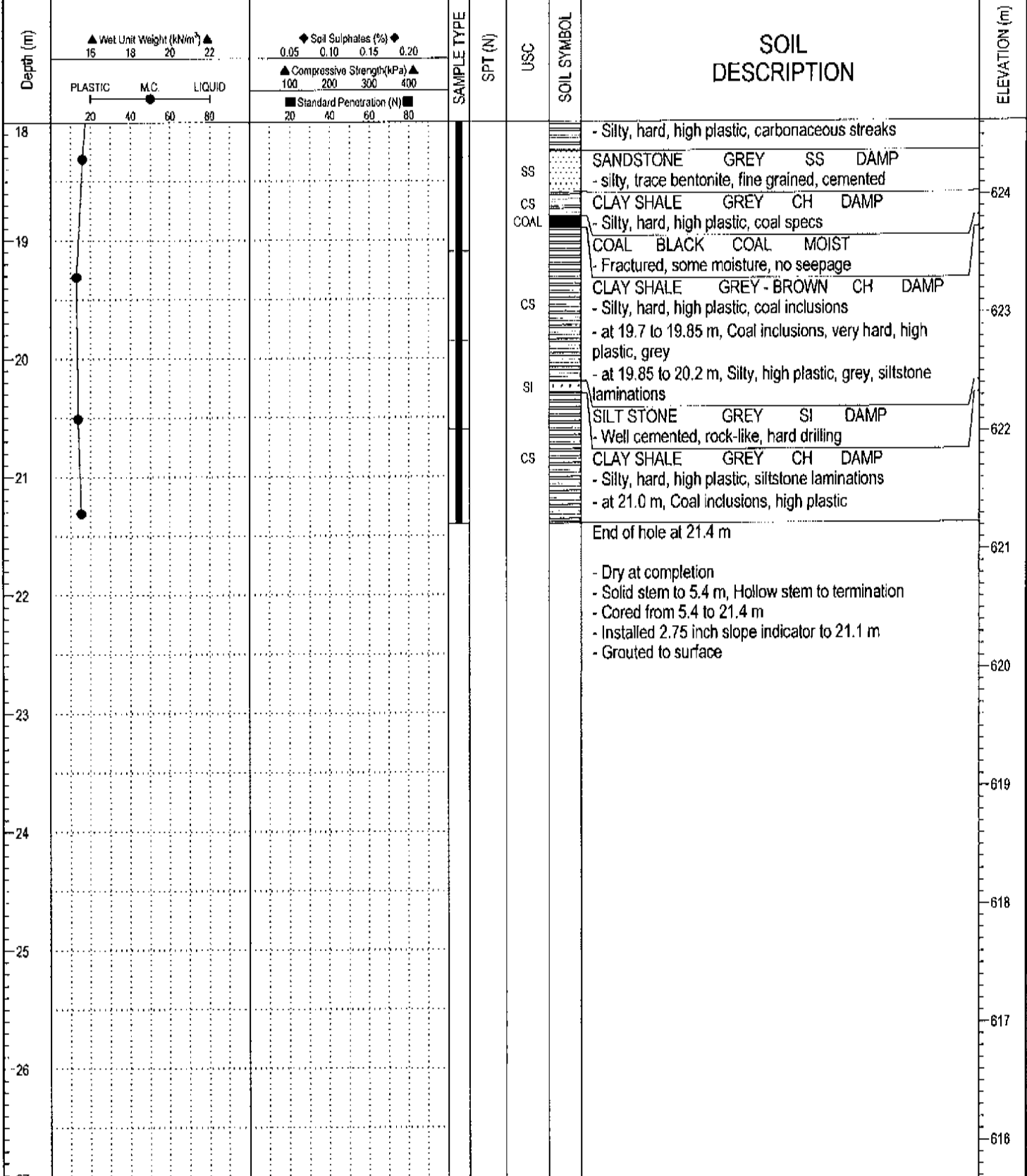
GEOTECH SI 10-01.GPJ EDMONTON.GDT 1/27/11



Transportation Department
Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 21.40 m
REVIEWED BY: KMT	COMPLETION DATE: 2010/09/16

SAMPLE TYPE Shelby Tube Drive Sample Auger Sample No Recovery A-Casing Cored Sample



GEO TECH SI 10-01.GPJ EDMONTON.GDT 1/27/11



Transportation Department
Engineering Services Section

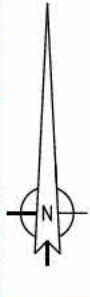
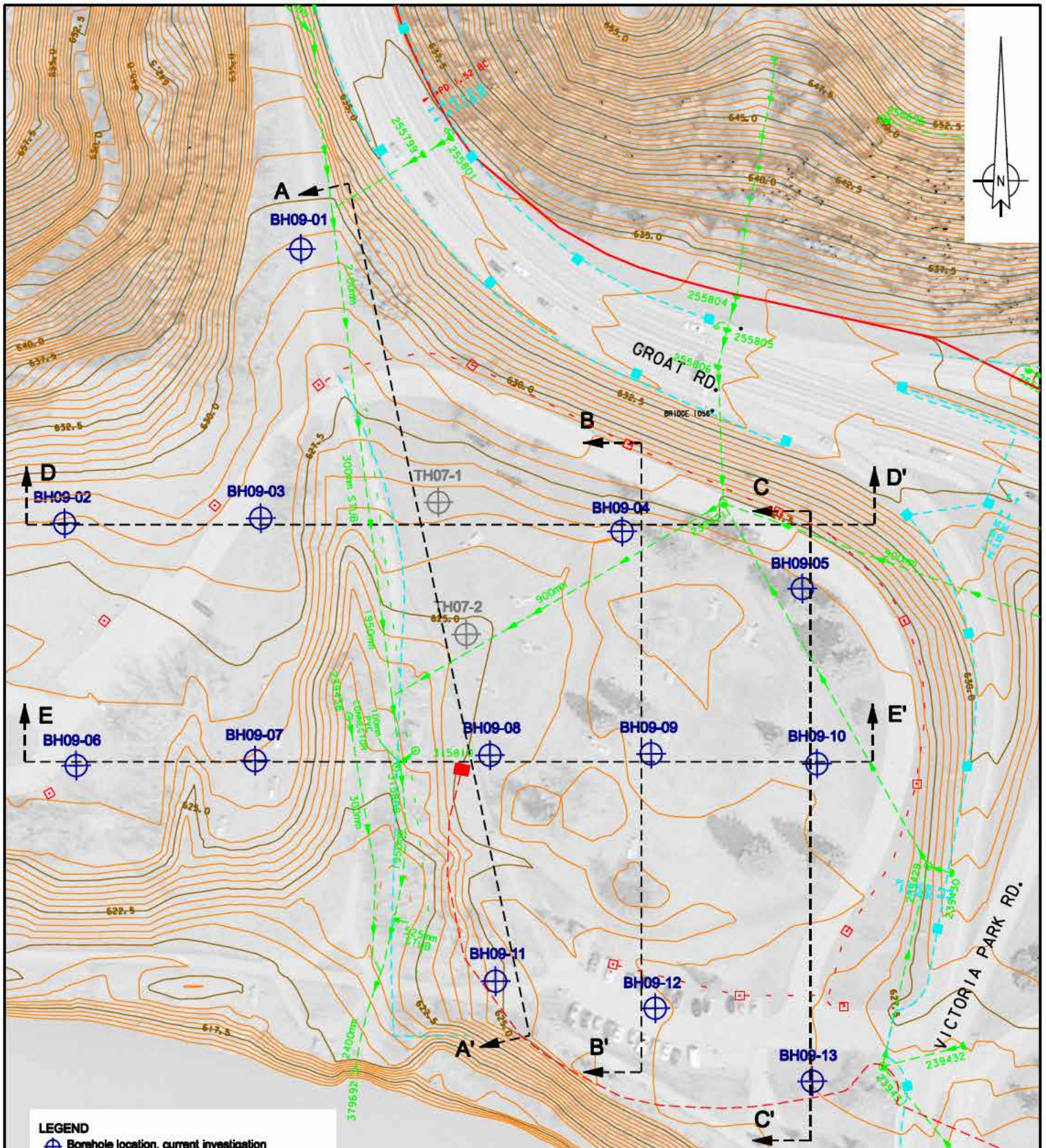
LOGGED BY: DD
REVIEWED BY: KMT

COMPLETION DEPTH: 21.40 m
COMPLETION DATE: 2010/09/16

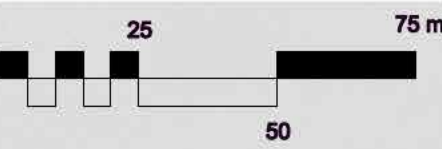
**PROPOSED GROAT SURFACE WETLAND
GEOTECHNICAL INVESTIGATION**

***Government House Park
Southwest of Groat Road at Victoria Park Road***

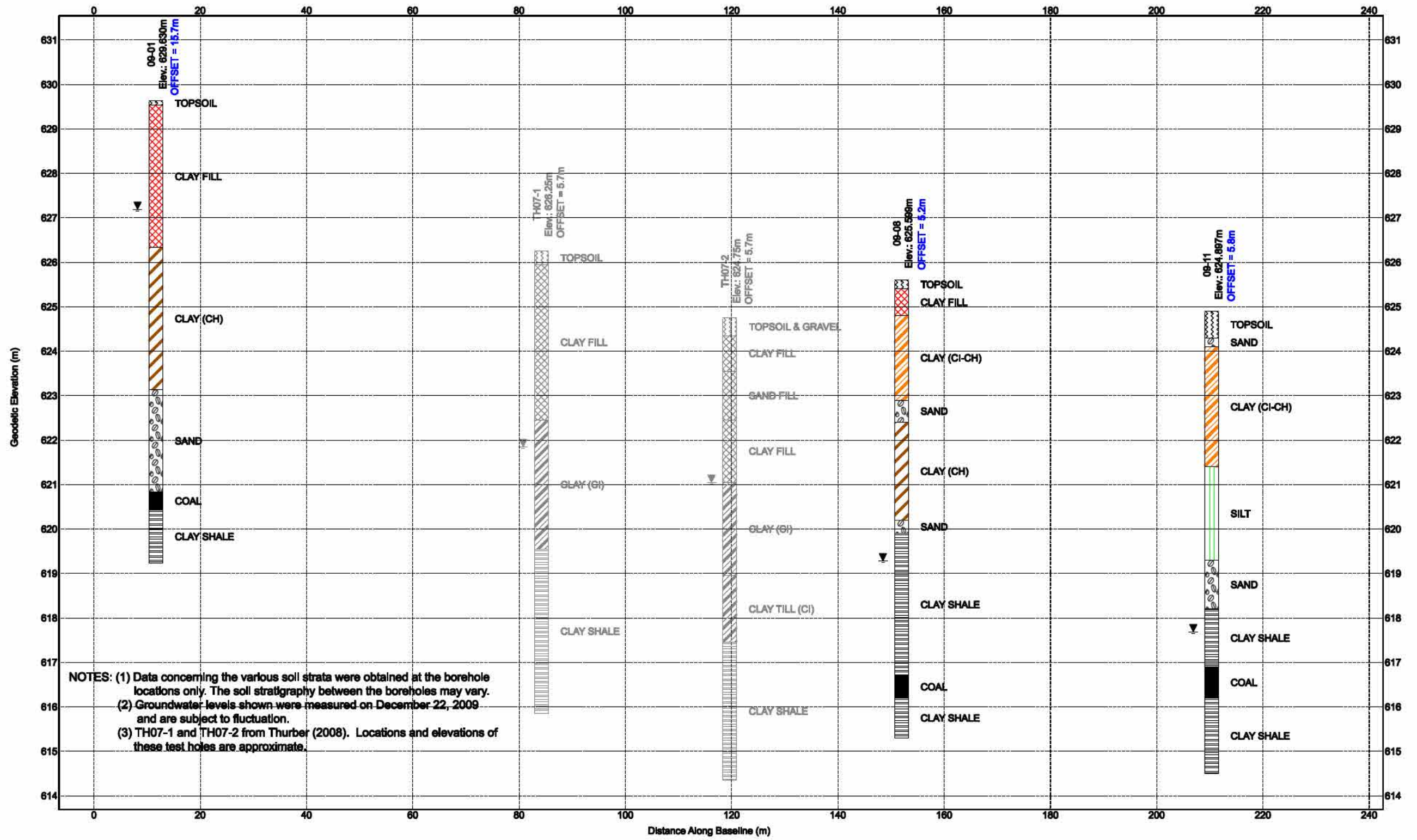
February 2010



- LEGEND**
- Borehole location, current investigation
 - Borehole location from previous Thurber (2008) investigation for oil/grit separator
 - Line of section
 - Ground surface contours from City of Edmonton geographic based information system



PROJECT GROAT SURFACE WETLAND PROJECT GEOTECHNICAL BOREHOLE LOCATIONS	
DRAWN BY	KMT
CHECKED	PRL
APPROVED	DML
DATE	FEBRUARY 2010
FILE	SCALE AS SHOWN
DRAWING	PLATE 2



NOTES: (1) Data concerning the various soil strata were obtained at the borehole locations only. The soil stratigraphy between the boreholes may vary.
 (2) Groundwater levels shown were measured on December 22, 2009 and are subject to fluctuation.
 (3) TH07-1 and TH07-2 from Thurber (2008). Locations and elevations of these test holes are approximate.

LEGEND:

TOPSOIL	SILT (LOW PLASTIC)	CLAY (MEDIUM PLASTIC)	COAL	GRAVEL (POORLY GRADED)	CLAY SHALE (BEDROCK)
GROUND WATER	FILL	CLAY (HIGH PLASTIC)	CLAY (LOW PLASTIC)	SAND	GRAVEL (WELL GRADED)

LOOKING WEST

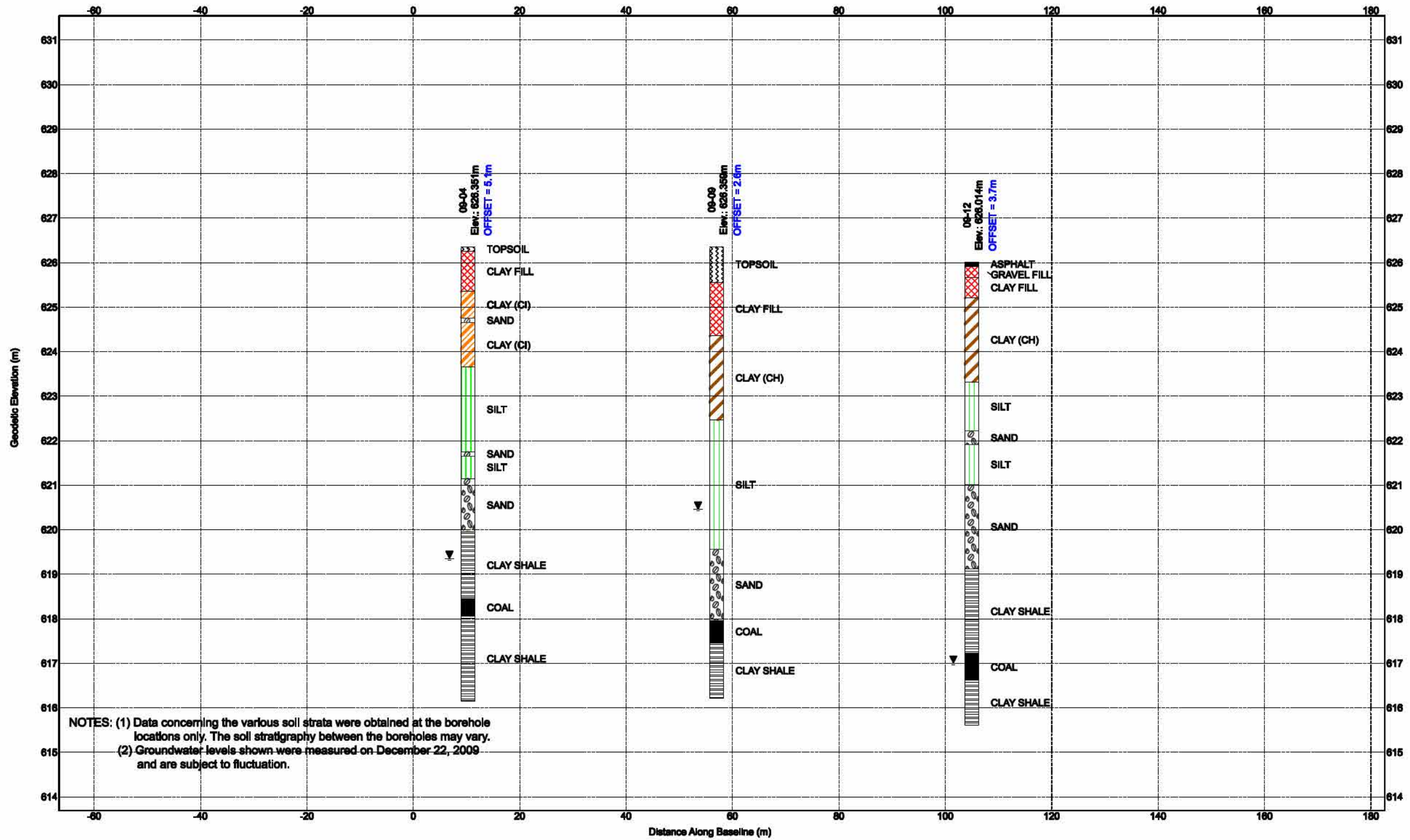


Drawing	PLATE 4
Checked	PRL

Drawn By	KMT
Date	FEBRUARY 2010
Scale	AS SHOWN



PROPOSED GROAT WETLAND
 GEOTECHNICAL INVESTIGATION
 PLATE 4: CROSS SECTION A-A'



NOTES: (1) Data concerning the various soil strata were obtained at the borehole locations only. The soil stratigraphy between the boreholes may vary.
 (2) Groundwater levels shown were measured on December 22, 2009 and are subject to fluctuation.

LEGEND:

TOPSOIL	SILT	CLAY (MEDIUM PLASTIC)	COAL	GRAVEL (POORLY GRADED)	CLAY SHALE (BEDROCK)
GROUND WATER	FILL	CLAY (HIGH PLASTIC)	CLAY (LOW PLASTIC)	SAND	GRAVEL (WELL GRADED)

LOOKING WEST



Drawing **PLATE 5**

Checked **PRL**

Drawn By **KMT**

Date **FEBRUARY 2010**

Scale **AS SHOWN**

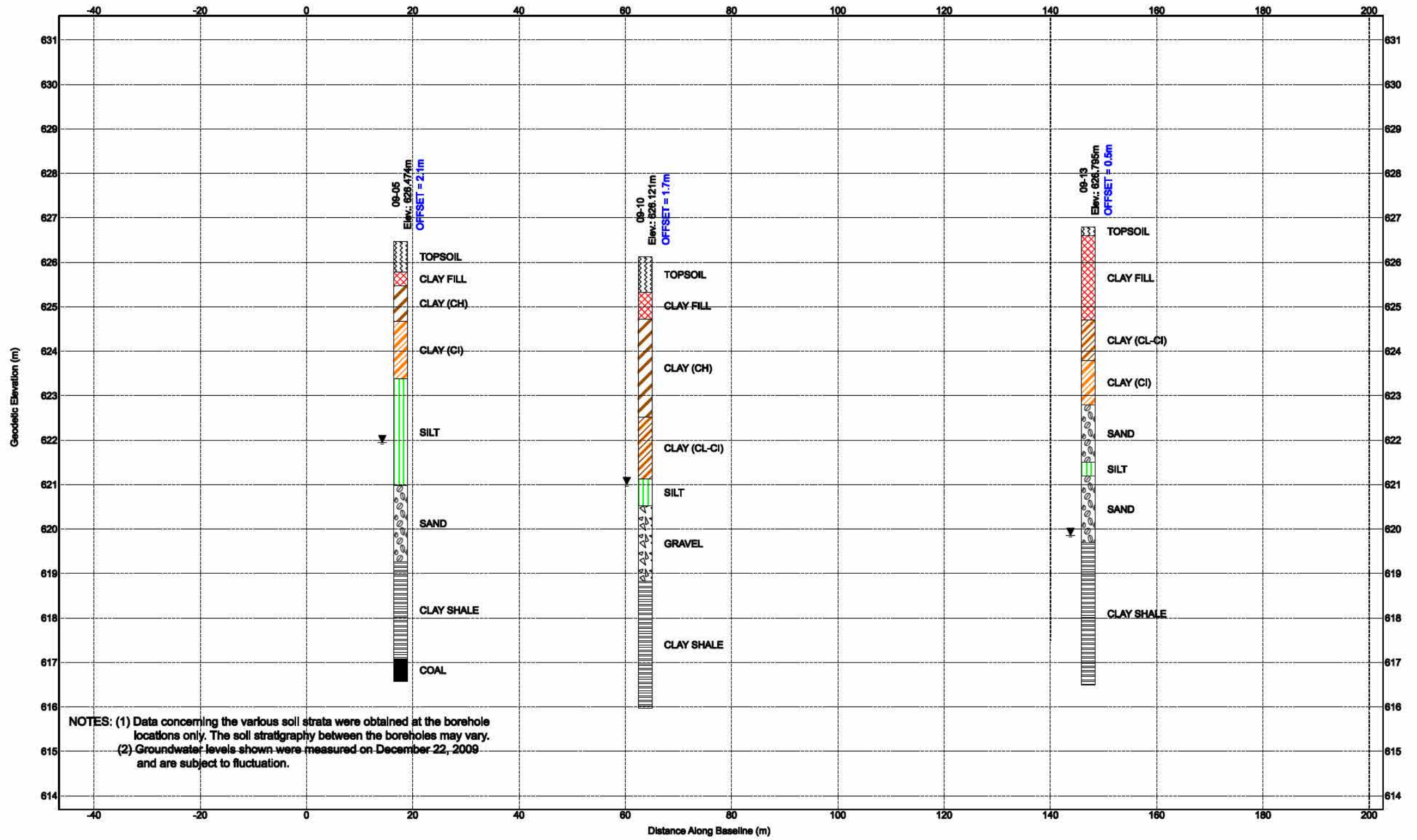


Transportation Department
Engineering Services Section

PROPOSED GROAT WETLAND

GEOTECHNICAL INVESTIGATION

PLATE 5: CROSS SECTION B-B'



NOTES: (1) Data concerning the various soil strata were obtained at the borehole locations only. The soil stratigraphy between the boreholes may vary.
 (2) Groundwater levels shown were measured on December 22, 2009 and are subject to fluctuation.

LEGEND:

- | | | | | | |
|--------------|------|-----------------------|--------------------|------------------------|----------------------|
| TOPSOIL | SILT | CLAY (MEDIUM PLASTIC) | COAL | GRAVEL (POORLY GRADED) | CLAY SHALE (BEDROCK) |
| GROUND WATER | FILL | CLAY (HIGH PLASTIC) | CLAY (LOW PLASTIC) | SAND | GRAVEL (WELL GRADED) |

LOOKING WEST



Drawing **PLATE 6**

Checked **PRL**

Drawn By **KMT**

Date **FEBRUARY 2010**

Scale **AS SHOWN**

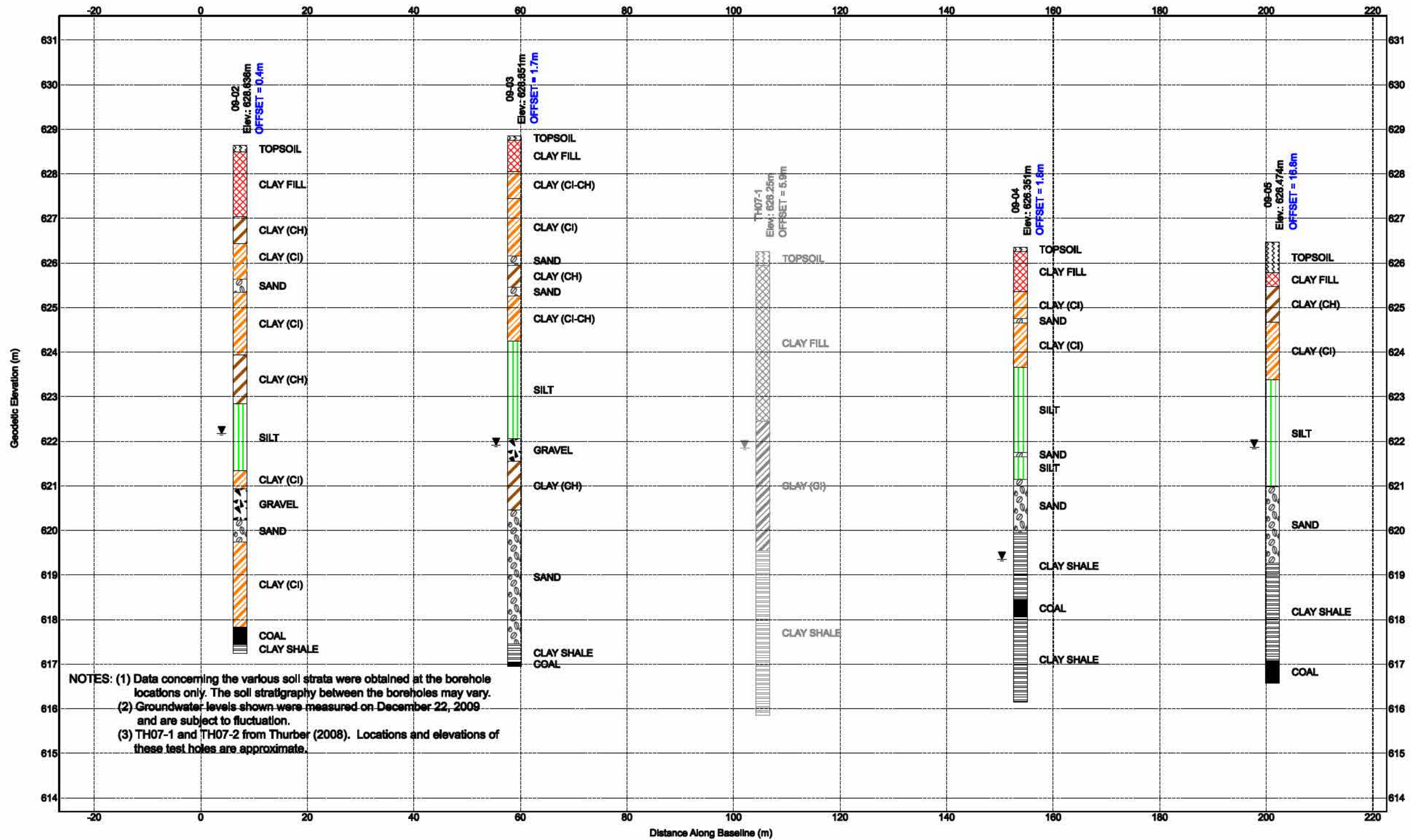


Transportation Department
Engineering Services Section

PROPOSED GROAT WETLAND

GEOTECHNICAL INVESTIGATION

PLATE 6: CROSS SECTION C-C'



NOTES: (1) Data concerning the various soil strata were obtained at the borehole locations only. The soil stratigraphy between the boreholes may vary.
 (2) Groundwater levels shown were measured on December 22, 2009 and are subject to fluctuation.
 (3) TH07-1 and TH07-2 from Thurber (2008). Locations and elevations of these test holes are approximate.

LEGEND:

TOPSOIL	SILT (LOW PLASTIC)	CLAY (MEDIUM PLASTIC)	COAL	GRAVEL (POORLY GRADED)	CLAY SHALE (BEDROCK)
GROUND WATER	FILL	CLAY (HIGH PLASTIC)	CLAY (LOW PLASTIC)	SAND	GRAVEL (WELL GRADED)

LOOKING NORTH



Drawing **PLATE 7**

Checked **PRL**

Drawn By **KMT**

Date **FEBRUARY 2010**

Scale **AS SHOWN**

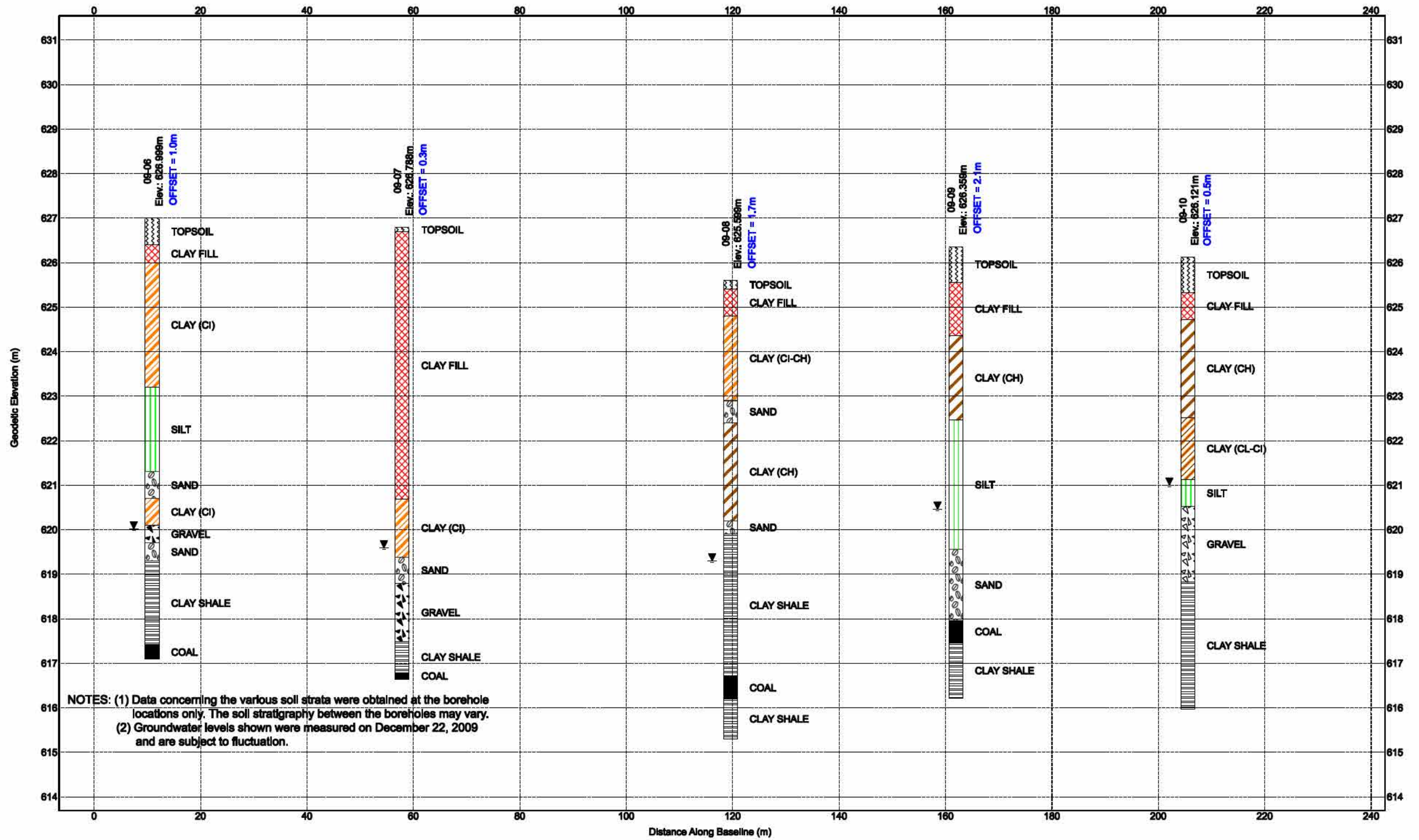


Transportation Department
Engineering Services Section

PROPOSED GROAT WETLAND

GEOTECHNICAL INVESTIGATION

PLATE 7: CROSS SECTION D-D'



LEGEND:

TOPSOIL	SILT (LOW PLASTIC)	CLAY (MEDIUM PLASTIC)	COAL	GRAVEL (POORLY GRADED)	CLAY SHALE (BEDROCK)
GROUND WATER	FILL	CLAY (HIGH PLASTIC)	CLAY (LOW PLASTIC)	SAND	GRAVEL (WELL GRADED)

LOOKING NORTH



Drawing **PLATE 8**

Checked **PRL**

Drawn By **KMT**

Date **FEBRUARY 2010**

Scale **AS SHOWN**



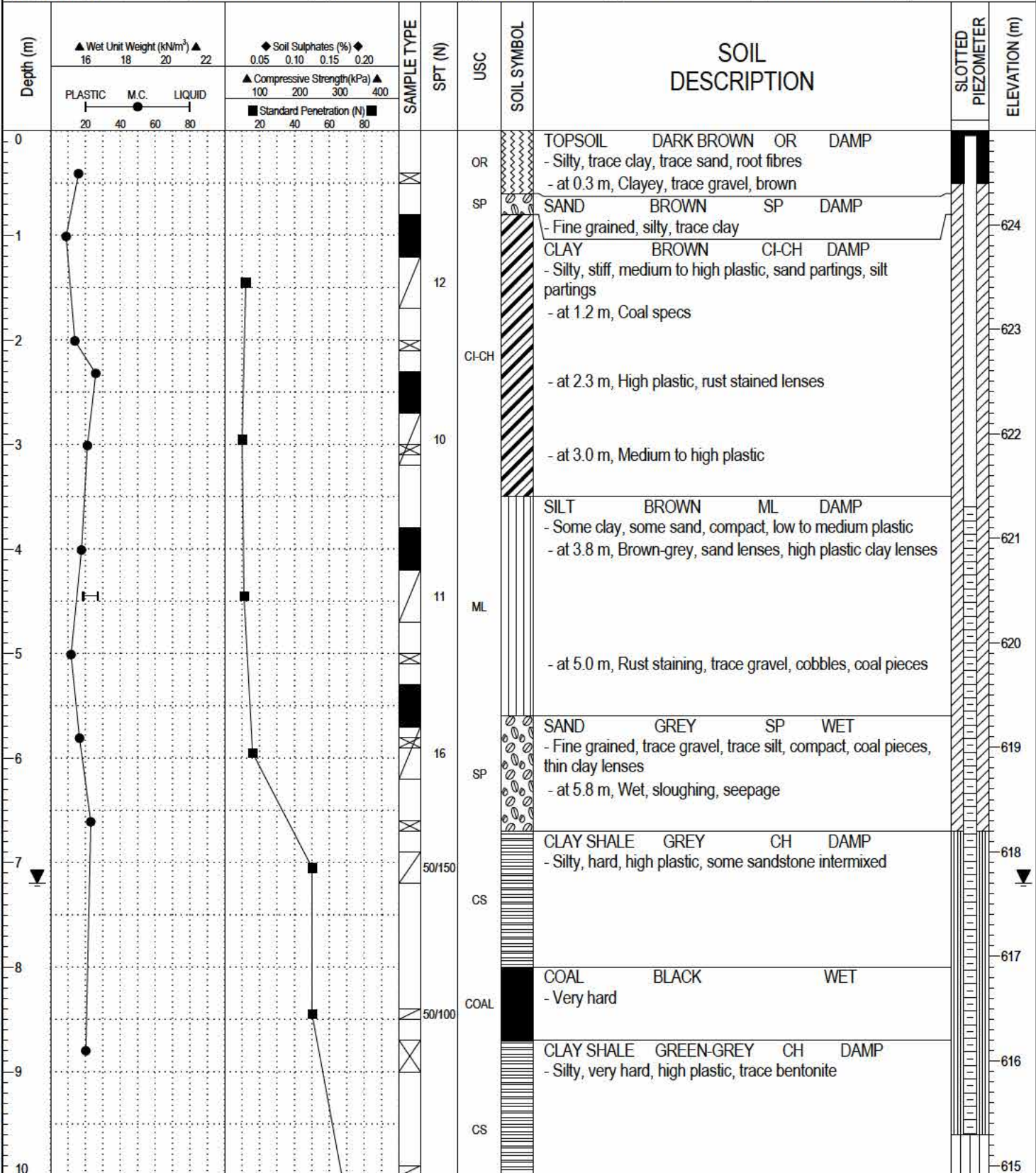
Transportation Department
Engineering Services Section

PROPOSED GROAT WETLAND

GEOTECHNICAL INVESTIGATION

PLATE 8: CROSS SECTION E-E'

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-11
DRAINAGE SERVICES	UTM ZONE: - N5934107.39 E30444.67	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 624.897 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	



STAND P GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.40 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
Page 1 of 2	

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-11
DRAINAGE SERVICES	UTM ZONE: - N5934107.39 E30444.67	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 624.897 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input checked="" type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input checked="" type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	

Depth (m)	▲ Wet Unit Weight (kN/m ³) ▲ 16 18 20 22 PLASTIC M.C. LIQUID 20 40 60 80	◆ Soil Sulphates (%) ◆ 0.05 0.10 0.15 0.20 ▲ Compressive Strength(kPa) ▲ 100 200 300 400 ■ Standard Penetration (N) ■ 20 40 60 80	SAMPLE TYPE	SPT (N)	USC	SOIL SYMBOL	SOIL DESCRIPTION	SLOTTED PIEZOMETER	ELEVATION (m)
10				69			CLAY SHALE GREEN-GREY CH DAMP		
11							End of Borehole at 10.4 m - Water level at 6.1 m, slough at 6.7 m on completion - Water level at 7.2 m on December 22, 2009 - Installed 25 mm PVC standpipe to 9.6 m - Backfilled with drill cuttings, bentonite surface seal		614
12									613
13									612
14									611
15									610
16									609
17									608
18									607
19									606
20									605

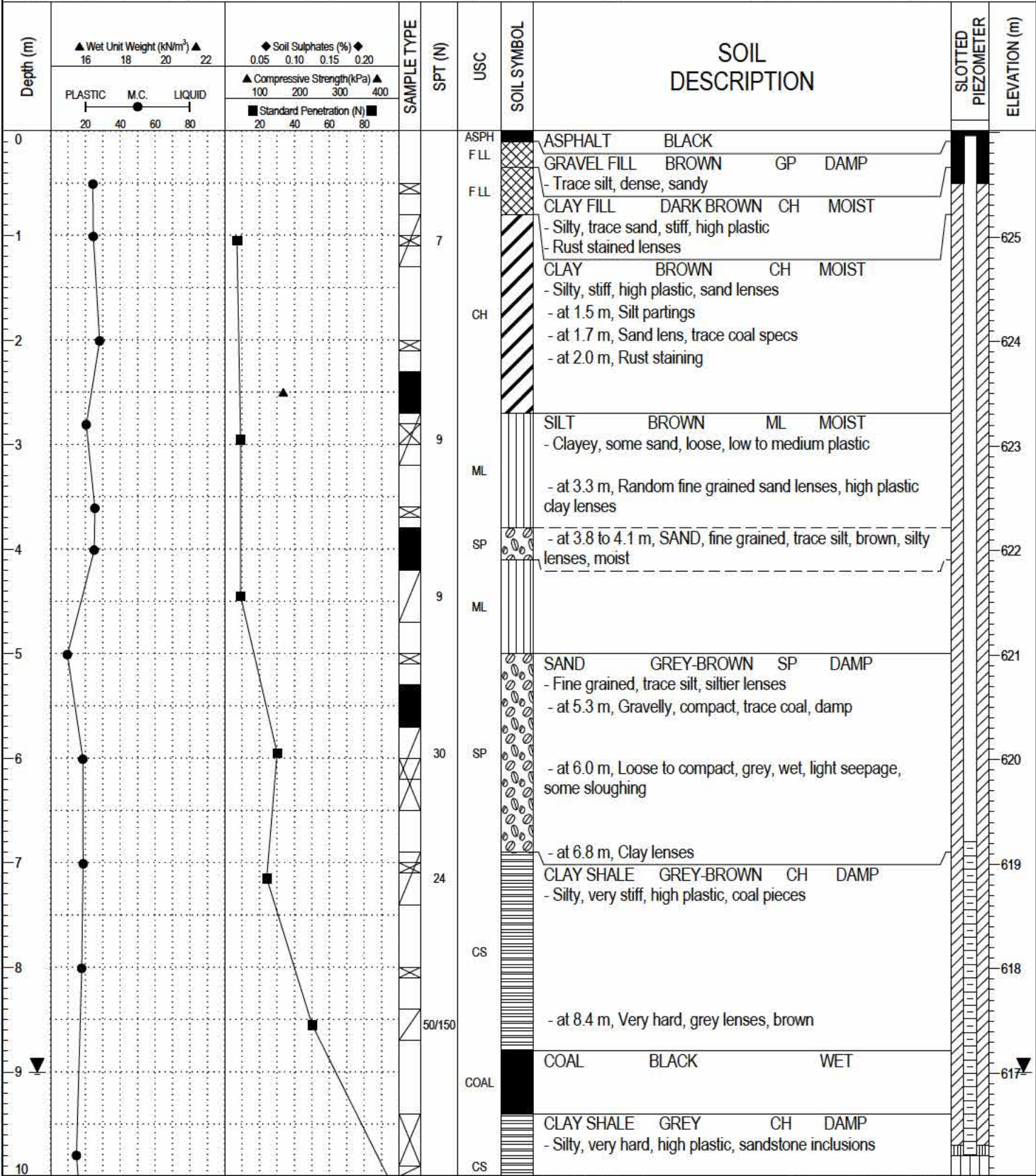
STANDP P GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.40 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
	Page 2 of 2

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-12
DRAINAGE SERVICES	UTM ZONE: - N5934100.29 E30486.64	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 626.014 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	



STAND P. GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.40 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
Page 1 of 2	

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-12
DRAINAGE SERVICES	UTM ZONE: - N5934100.29 E30486.64	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 626.014 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input checked="" type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input checked="" type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	

Depth (m)	▲ Wet Unit Weight (kN/m ³) ▲ 16 18 20 22 PLASTIC M.C. LIQUID 20 40 60 80	◆ Soil Sulphates (%) ◆ 0.05 0.10 0.15 0.20 ▲ Compressive Strength (kPa) ▲ 100 200 300 400 ■ Standard Penetration (N) ■ 20 40 60 80	SAMPLE TYPE	SPT (N)	USC	SOIL SYMBOL	SOIL DESCRIPTION	SLOTTED PIEZOMETER	ELEVATION (m)
10				98		CLAY SHALE GREY CH DAMP			
11							End of Borehole at 10.4 m - Water level at 6.9 m, slough at 9.7 m on completion - Water level at 9.0 m on October 5, 2009 - Installed 25 mm PVC standpipe to 9.8 m - Backfilled with drill cuttings, bentonite surface seal		615
12									614
13									613
14									612
15									611
16									610
17									609
18									608
19									607
20									

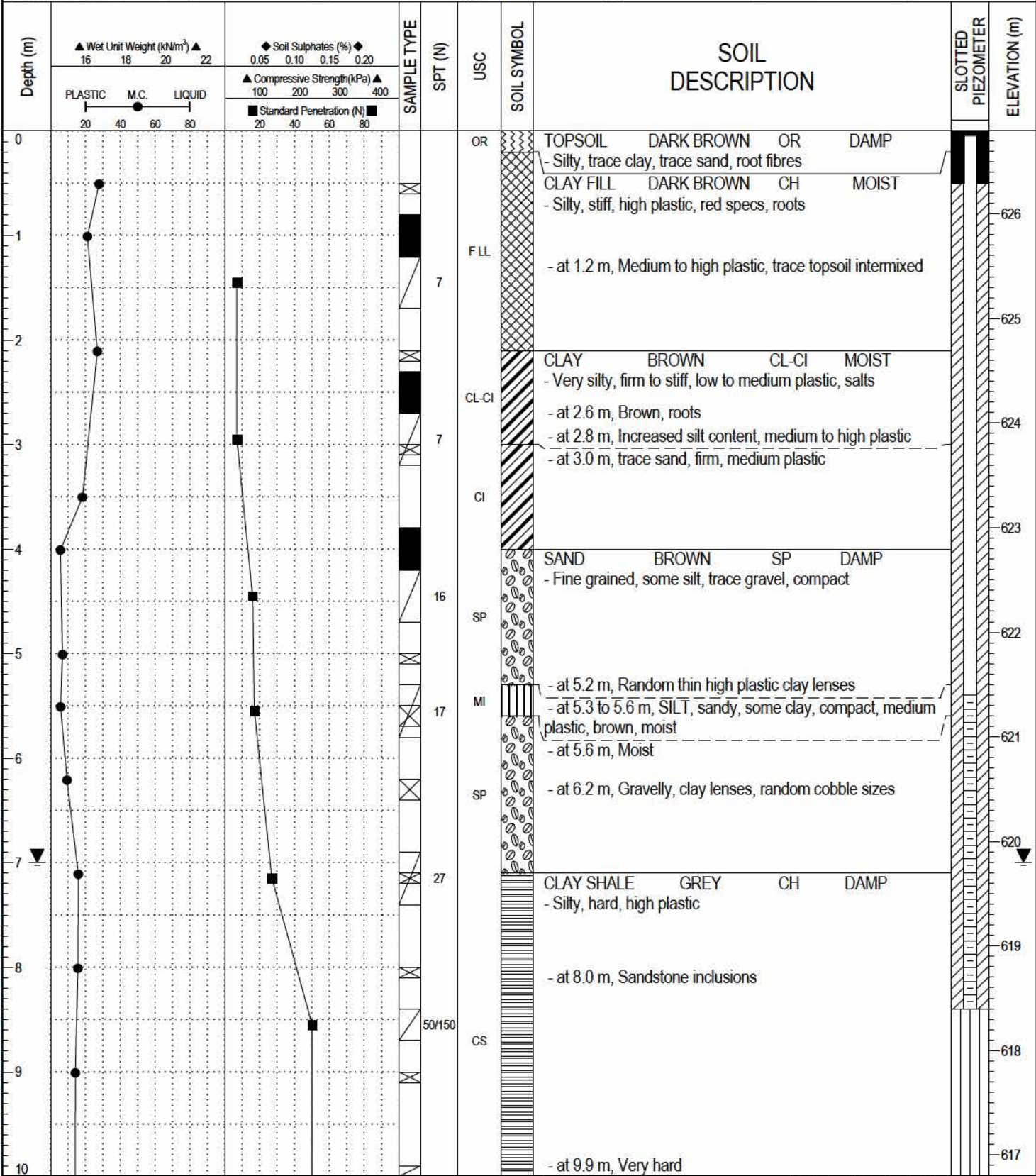
STANDP P GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.40 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
	Page 2 of 2

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-13
DRAINAGE SERVICES	UTM ZONE: - N5934081.08 E30527.91	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 626.795 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	



STAND P GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.30 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
Page 1 of 2	

GROAT SURFACE WETLAND PROJECT	West of Groat Road North Side of Sask. River	BOREHOLE NO: 09-13
DRAINAGE SERVICES	UTM ZONE: - N5934081.08 E30527.91	PROJECT NO: 60007944 - 0010
START DATE: 2009/09/30	934 + 32 + 02 / 934 + 32 + 03	ELEVATION: 626.795 m
SAMPLE TYPE	<input checked="" type="checkbox"/> Shelby Tube <input type="checkbox"/> Drive Sample <input checked="" type="checkbox"/> Auger Sample <input type="checkbox"/> No Recovery <input type="checkbox"/> A Casing <input type="checkbox"/> Cored Sample	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input checked="" type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	

Depth (m)	▲ Wet Unit Weight (kN/m ³) ▲ 16 18 20 22 PLASTIC M.C. LIQUID 20 40 60 80	◆ Soil Sulphates (%) ◆ 0.05 0.10 0.15 0.20 ▲ Compressive Strength(kPa) ▲ 100 200 300 400 ■ Standard Penetration (N) ■ 20 40 60 80	SAMPLE TYPE	SPT (N)	USC	SOIL SYMBOL	SOIL DESCRIPTION	SLOTTED PIEZOMETER	ELEVATION (m)
10				50/125			CLAY SHALE GREY CH DAMP		
11							End of Borehole at 10.3 m - Borehole dry, slough at 8.4 m on completion - Water level at 7.0 m on December 22, 2009 - Installed 25 mm PVC standpipe to 8.4 m - Backfilled with drill cuttings, bentonite surface seal		616
12									615
13									614
14									613
15									612
16									611
17									610
18									609
19									608
20									607

STANDP P GROAT WETLANDS SURFACE PROJECT.GPJ EDMONTON.GDT 2/8/10



Transportation Engineering Services Section

LOGGED BY: DD	COMPLETION DEPTH: 10.30 m
REVIEWED BY: KMT	COMPLETION DATE: 2009/09/30
	Page 2 of 2

**Groat Road Bridges Rehabilitation Project:
Roadworks at Groat Road Interchange
Environmental Impact Assessment**

Draft Report

Prepared for:

**City of Edmonton Transportation Planning & Design and Transportation
Infrastructure Delivery**
Edmonton, Alberta

Prepared by:

**Spencer Environmental
Management Services Ltd.**
Edmonton, Alberta

Under contract to:




DIALOG
Edmonton, Alberta

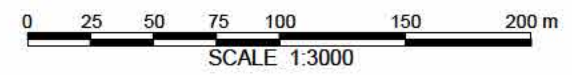
Project Number EP 667

March 2017



LEGEND

-  APPROXIMATE TEST HOLE LOCATION (2016)
-  APPROXIMATE TEST HOLE LOCATION (2015)
-  PROPOSED WESTBOUND VICTORIA PARK ROAD TO NORTHBOUND GROAT ROAD RAMP



BASE PLAN PROVIDED BY CITY OF EDMONTON TRANSPORTATION DEPARTMENT



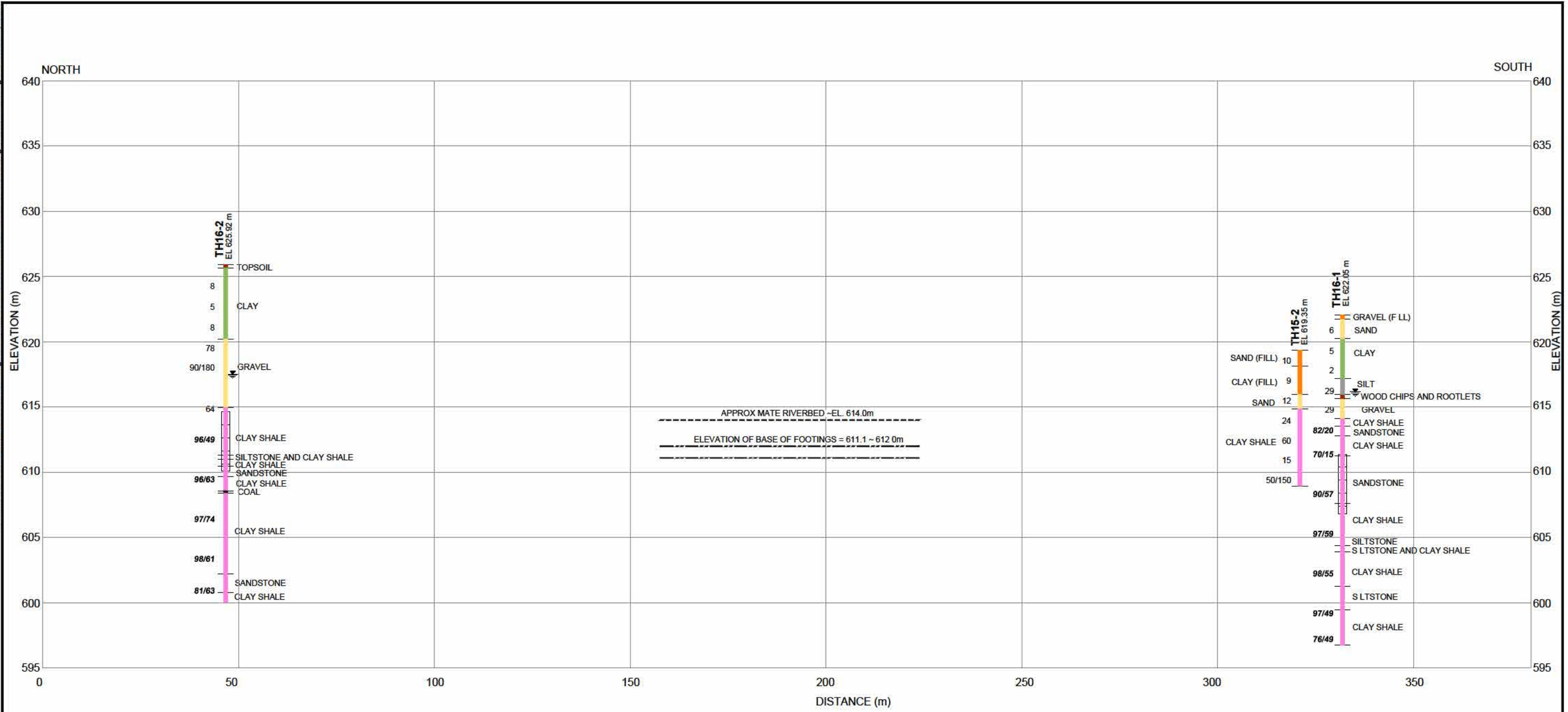
GROAT ROAD BRIDGE REHABILITATION


SITE PLAN SHOWING TEST HOLE LOCATIONS

DWG No. 10298-1

DRAWN BY	ML
DESIGNED BY	SEC
APPROVED BY	HER
SCALE	1:3000
DATE	JUNE 2016
FILE No.	10298








GROAT ROAD BRIDGE REHABILITATION

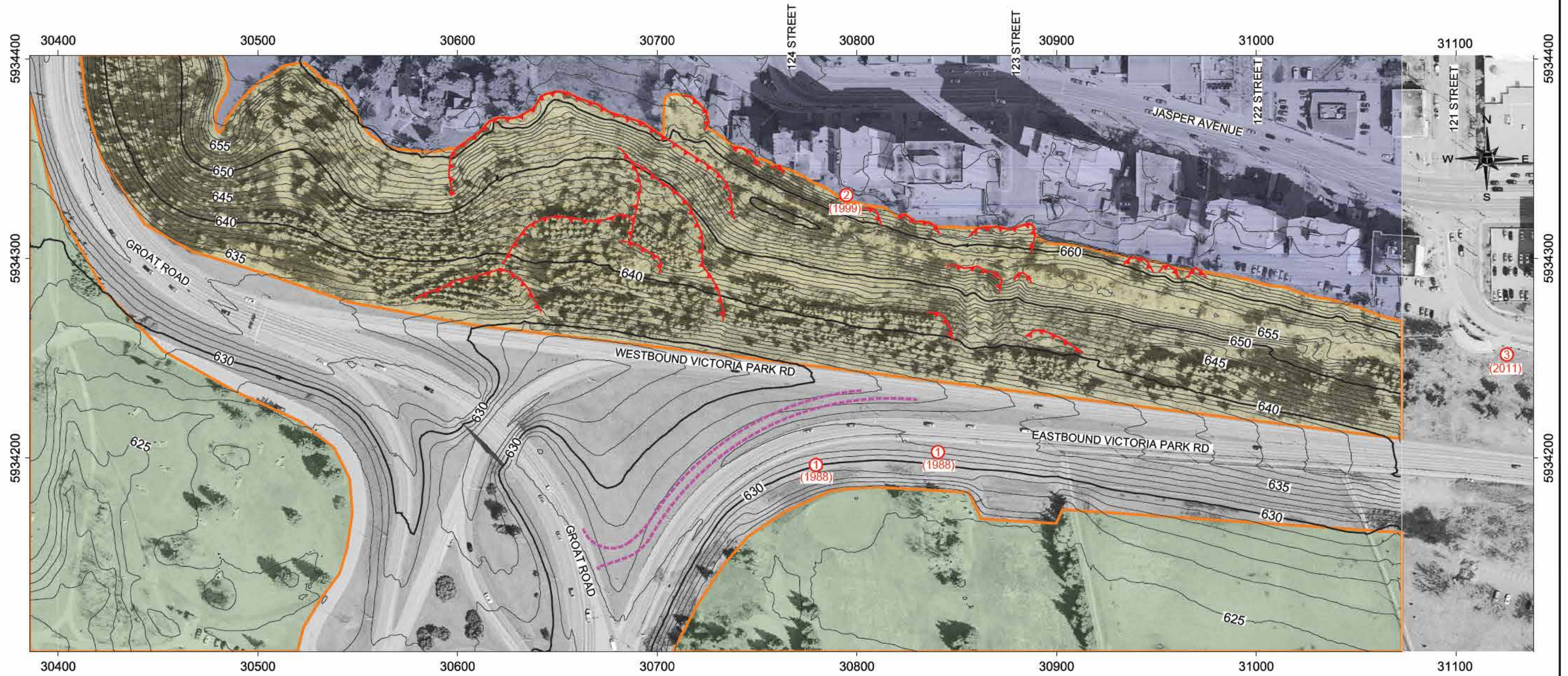
STRATIGRAPHIC CROSS - SECTION

DWG No. 10298-2

DRAWN BY	ML
DESIGNED BY	SEC
APPROVED BY	HER
SCALE	H 1:1000 V 1:300
DATE	JUNE 2016
FILE No.	10298



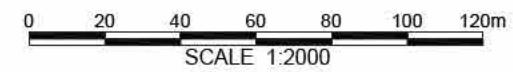
THURBER ENGINEERING LTD.




LEGEND

- ROADS, FILL
- ALLUVIUM DEPOSITS
- COLLUVIUM
- GLACIOLACUSTRINE DEPOSITS; SILT, CLAY, SAND
- SCARP
- GROUND SURFACE (CONTOURS 1m)
- 1
(1988) SLOPE INSTABILITY REPORTED IN 1988
- PROPOSED WESTBOUND VICTORIA PARK ROAD TO NORTHBOUND GROAT ROAD RAMP

Reference:
L. A. Bayrock. Surficial Geology Edmonton. NTS 83H A berta Research 1972.






GROAT ROAD BRIDGE REHABILITATION

SURFICIAL GEOLOGY MAP

DWG NO. 10298-3

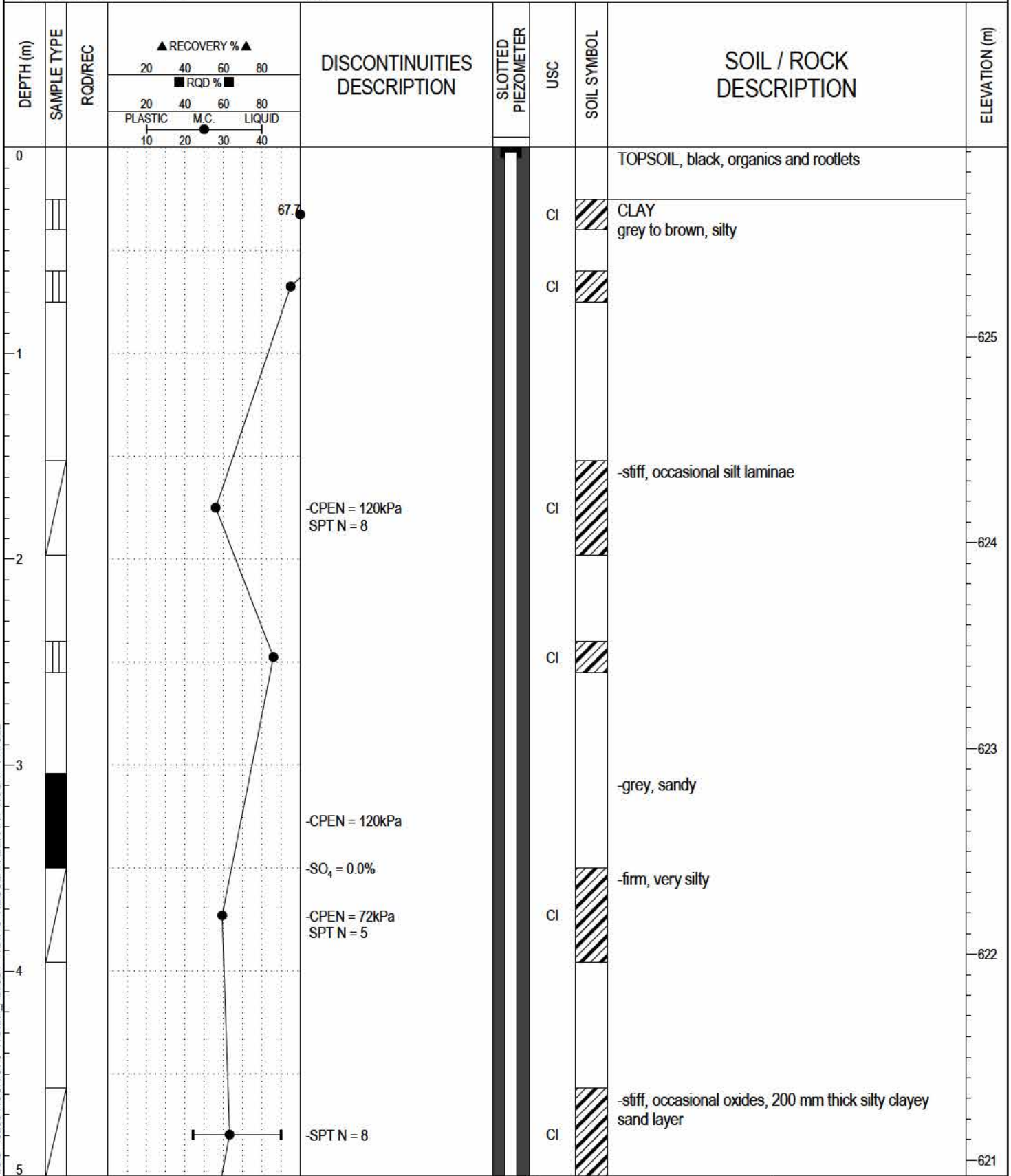
DRAWN BY	ML
DESIGNED BY	MJB
APPROVED BY	HER
SCALE	1:2000
DATE	JUNE 2016
FILE No.	10298



THURBER ENGINEERING LTD.

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input checked="" type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND		



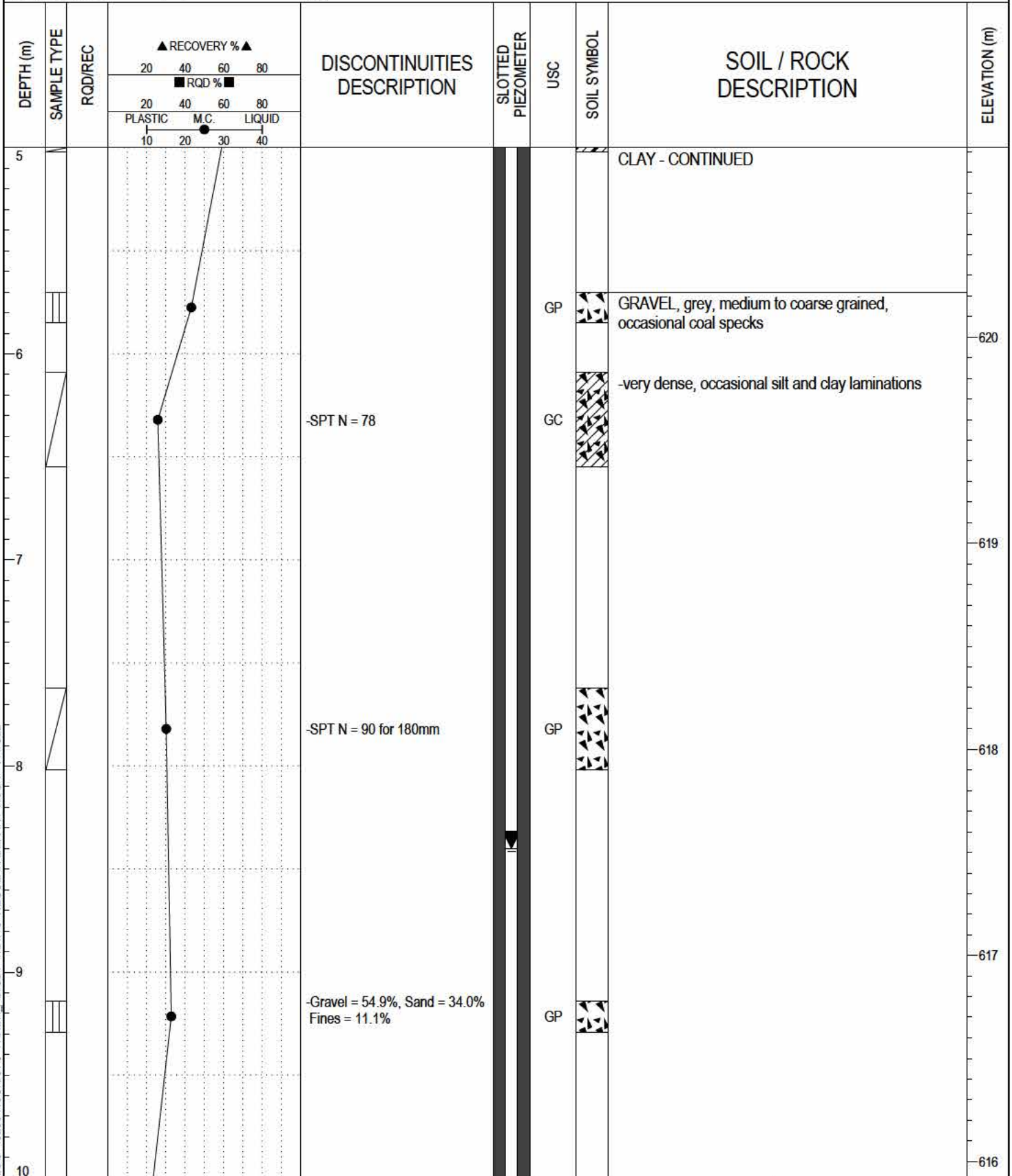
BOREHOLE LOG: 10298-ROCK.GPJ, THRBR_AB.GDT, 7/21/16-REGULAR-LIBRARY-ROCK-VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 1 of 6

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND		



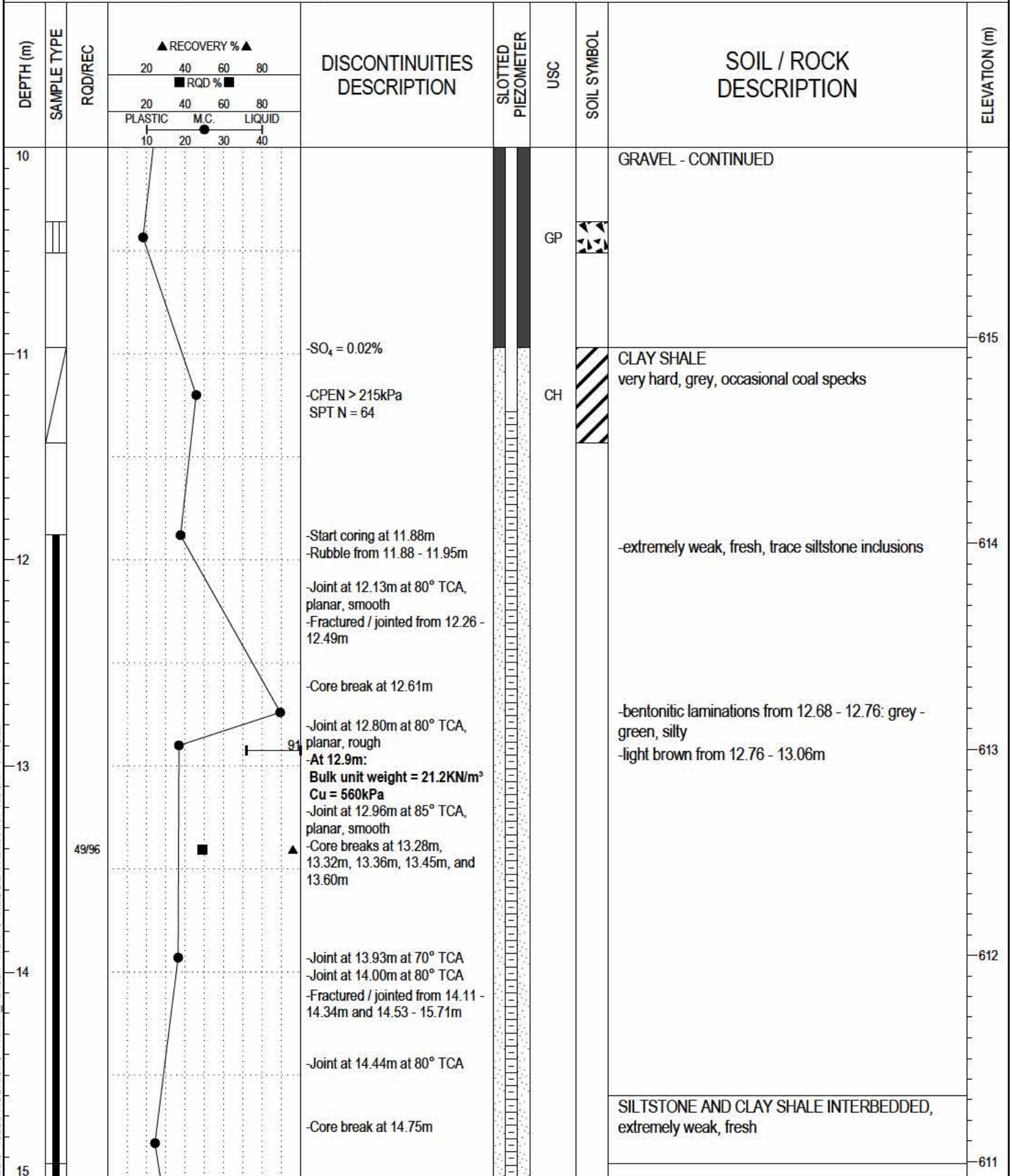
BOREHOLE LOG 10298:ROCK.GPJ,THRBR_AB.GDT,7/21/16-REGULAR LIBRARY-ROCK-VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 2 of 6

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE	
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND			



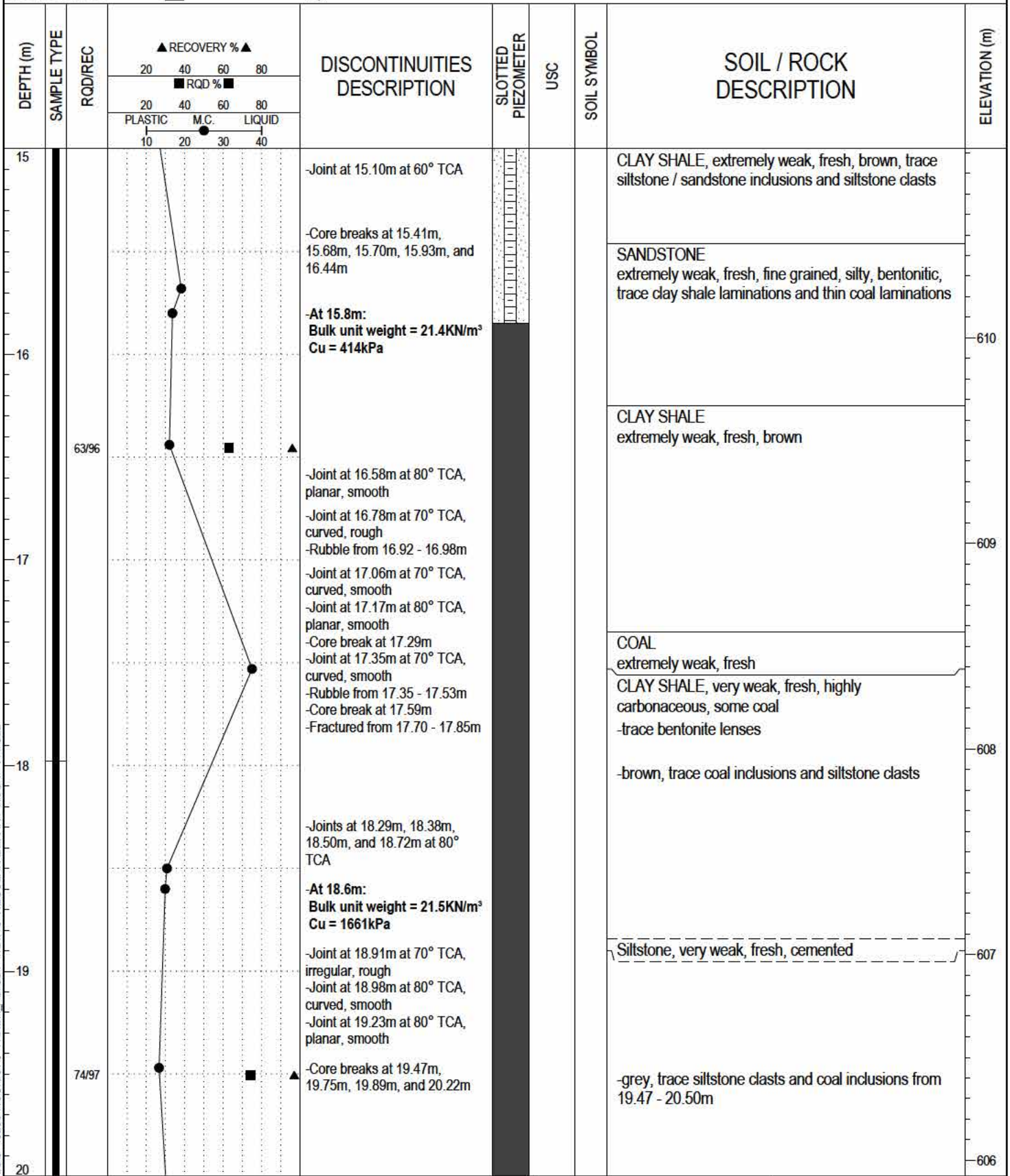
BOREHOLE LOG: 10298-ROCK.GPJ, THRR, AB.GDT, 7/21/16-REGULAR-LIBRARY-ROCK-VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 3 of 6

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND		



BOREHOLE LOG: 10298-ROCK.GPJ, THRB, AB.GDT, 7/21/16 - REGULAR LIBRARY-ROCK - VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 4 of 6

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND		

DEPTH (m)	SAMPLE TYPE	RQD/REC	RECOVERY %			DISCONTINUITIES DESCRIPTION	SLOTTED PIEZOMETER	USC	SOIL SYMBOL	SOIL / ROCK DESCRIPTION	ELEVATION (m)
			20	40	60						
20									CLAY SHALE - CONTINUED		
21						-Joint at 20.30m at 60° TCA, curved, rough, slickensided -Joint at 20.38m at 60° TCA, curved, smooth -Joint at 20.47m at 50° TCA, curved, smooth -Core break at 20.60m -Joint at 20.84m at 80° TCA, curved, smooth -Joints at 20.93m and 21.38m at 70° TCA, stepped, smooth			Siltstone, medium strong, fresh, cemented -trace siltstone and coal inclusions	605	
22						-Fractured / jointed from 21.78 - 21.98m -Joint at 21.84m at 50° TCA, curved, smooth -Joint at 21.93m at 40° TCA, curved, smooth -Joints from 21.98 - 22.15m at 10° TCA, irregular, rough -Joint at 22.16m at 80° TCA, planar, rough -Joints from 22.16 - 22.31m at 15° TCA, closed -Joint at 22.33m at 60° TCA, curved, smooth -Joints from 22.37 - 22.52m at 25° TCA, curved, smooth -Core break at 22.60m -Joint at 22.64m at 60° TCA, undulating, smooth -Joint at 23.20m at 80° TCA, planar, smooth -Core break at 23.25m -Joint at 23.52m at 80° TCA, curved, rough			-carbonaceous -highly carbonaceous from 21.98 - 22.15m	604	
23		61/98				-Joint at 22.16m at 80° TCA, planar, rough -Joints from 22.16 - 22.31m at 15° TCA, closed -Joint at 22.33m at 60° TCA, curved, smooth -Joints from 22.37 - 22.52m at 25° TCA, curved, smooth -Core break at 22.60m -Joint at 22.64m at 60° TCA, undulating, smooth -Joint at 23.20m at 80° TCA, planar, smooth -Core break at 23.25m -Joint at 23.52m at 80° TCA, curved, rough			Sandstone very weak, fresh, fine grained, bentonitic, trace coal inclusions and clay shale / siltstone laminations	603	
24						-Joint at 23.89m at 80° TCA -Core break at 24.27m			SANDSTONE very weak, fresh, fine grained, bentonitic, trace thin coal laminations -trace siltstone inclusions and clay shale laminations -calcareous from 24.27 - 24.43m	602	
25						-Joint at 24.63m at 85° TCA, planar, smooth -Joint at 24.84m at 70° TCA, curved, rough				601	

BOREHOLE LOG: 10298-ROCK.GPJ, THRR-AB.GDT, 7/21/16-REGULAR-LIBRARY-ROCK-VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 5 of 6

CLIENT: DIALOG	PROJECT: Groat Road River Bridge Rehabilitation & Associated Road Work	BOREHOLE NO: TH16-2
DRILLING COMPANY: Garrity & Baker	DATE DRILLED: April 19, 2016	PROJECT NO: 10298
DRILL/METHOD: Wet Rotary / Coring	LOCATION: N5933991.67, E30656.47	ELEVATION: 625.92 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> SAND		

DEPTH (m)	SAMPLE TYPE	RQD/REC	RECOVERY %		DISCONTINUITIES DESCRIPTION	SLOTTED PIEZOMETER	USC	SOIL SYMBOL	SOIL / ROCK DESCRIPTION	ELEVATION (m)															
			▲	■																					
25		63/81	<table border="1"> <tr> <td>20</td> <td>40</td> <td>60</td> <td>80</td> </tr> <tr> <td>20</td> <td>40</td> <td>60</td> <td>80</td> </tr> <tr> <td>PLASTIC</td> <td>M.C.</td> <td colspan="2">LIQUID</td> </tr> <tr> <td>10</td> <td>20</td> <td>30</td> <td>40</td> </tr> </table>	20	40	60	80	20	40	60	80	PLASTIC	M.C.	LIQUID		10	20	30	40	- Joints from 24.99 - 25.12m at 5° TCA, closed - Fractured / jointed from 25.12 - 25.22m - Joint at 25.56m at 40° TCA, curved, smooth				- medium strong, cemented, calcareous from 24.99 - 25.12m CLAY SHALE, very weak, fresh, brown - grey - cemented siltstone clasts	600
20	40	60	80																						
20	40	60	80																						
PLASTIC	M.C.	LIQUID																							
10	20	30	40																						
26								END OF TEST HOLE AT 25.9m UPON COMPLETION: Standpipe piezometer installed WATER LEVEL BELOW GROUND SURFACE: - May 3, 2016 = 7.9m - May 18, 2016 = 8.4m	599																
27									598																
28									597																
29									596																
30																									

BOREHOLE LOG: 10298:ROCK.GPJ, THRBR_AB.GDT, 7/21/16-REGULAR LIBRARY-ROCK-VW.GLB



FIELD LOGGED BY: NR	COMPLETION DEPTH: 25.9 m
PREPARED BY: SEC	COMPLETION DATE: 4/19/16
REVIEWED BY: HER	Page 6 of 6



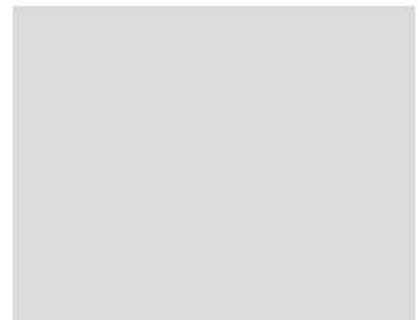
THURBER ENGINEERING LTD.

**WALTERDALE BRIDGE REPLACEMENT
EDMONTON, ALBERTA
GEOTECHNICAL INVESTIGATION**

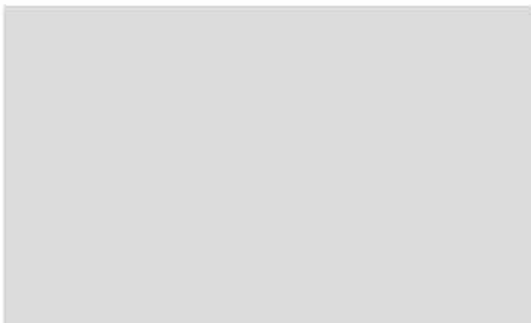
Report

to

ISL Engineering and Land Services



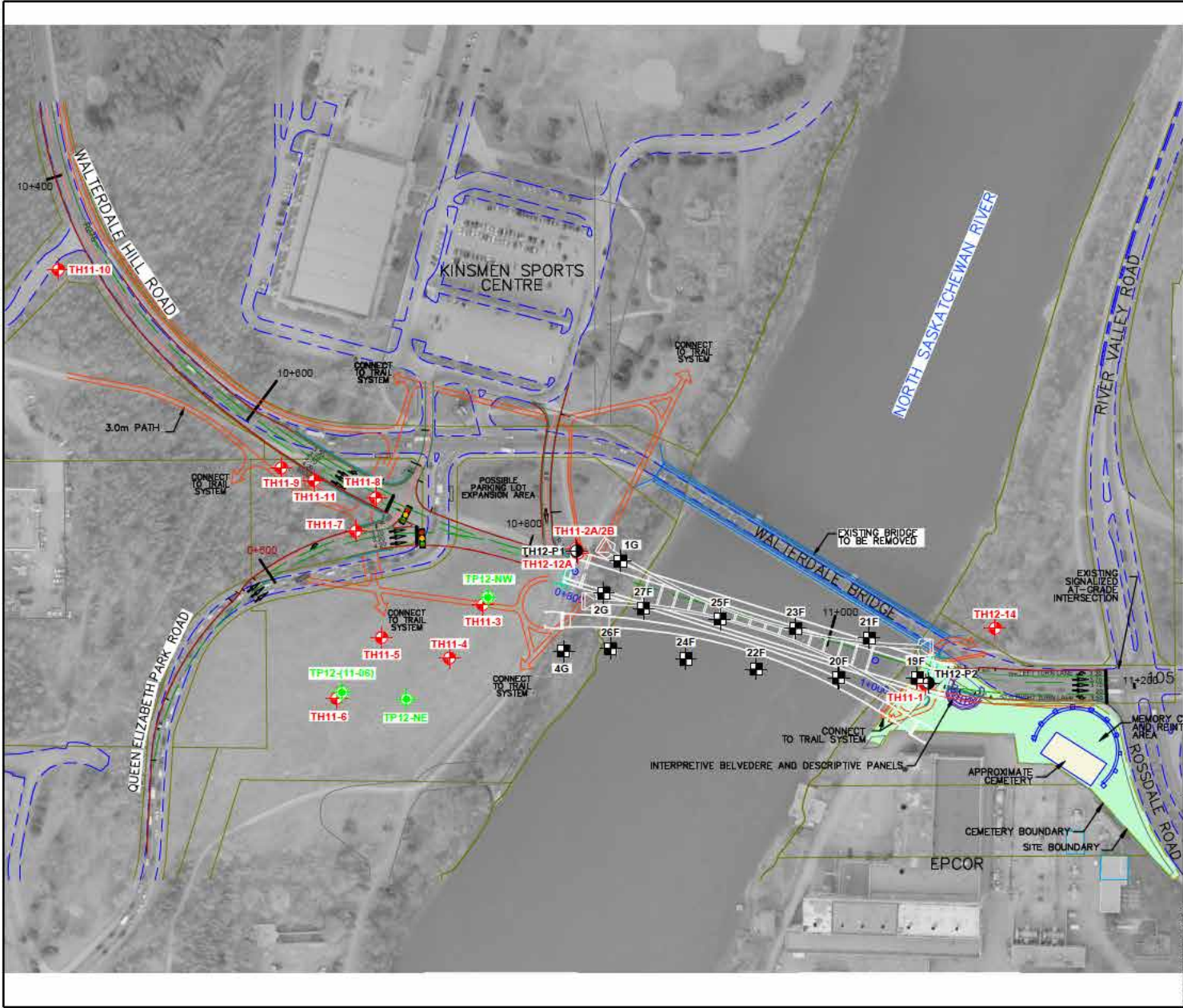
Xiaobo Wang, Ph.D., P.Eng.
Senior Project Engineer



Hassan El-Ramly, P.Eng., Ph.D.
Review Principal

Date: January 31, 2013
File: 19-598-370

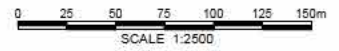
Z:\1919-598-370\19-598-370-181A August 15 2012.dwg - 1 - Dec 11, 2012



LEGEND

- ◆ RECENT GEOTECHNICAL TEST HOLE LOCATION (THURBER, 2011/2012)
- PREVIOUS GEOTECHNICAL TEST HOLE LOCATION - APPROXIMATE (R. M. HARDY & ASSOCIATES, 1965)
- ◆ GEOTECHNICAL TEST PIT LOCATION (THURBER 2012)
- ⊗ PRESSUREMETER TEST LOCATION

NOTE:
BASE PLAN PROVIDED BY AL-TERRA ENGINEERING LTD. IN AUGUST 2011



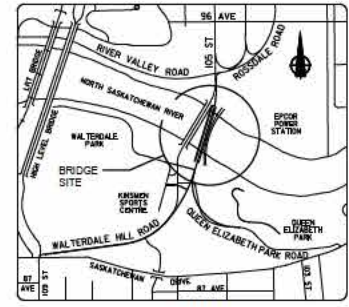
**WALTERDALE BRIDGE REPLACEMENT
DETAILED DESIGN & CONSTRUCTION**

**SITE PLAN SHOWING GEOTECHNICAL
TEST HOLE LOCATIONS**

19-598-370-1

DRAWN BY	ML
DESIGNED BY	RFM
APPROVED BY	HER
SCALE	1:2500
DATE	JULY 2012
FILE No.	19-598-370





KEY PLAN
1:10000

EXISTING SITE PLAN
1:1000

WALTERDALE BRIDGE OVER THE NORTH SASKATCHEWAN RIVER
 WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
 EXISTING SITE PLAN
 11 OCT 2013
 WALT 131 S005

NO	REVISED	DATE	BY	APPROVED

PROGRAM NO.	
CONTRACT NO.	
ISSUE NO.	
ISSUE DATE	
ISSUE BY	
ISSUE DATE	

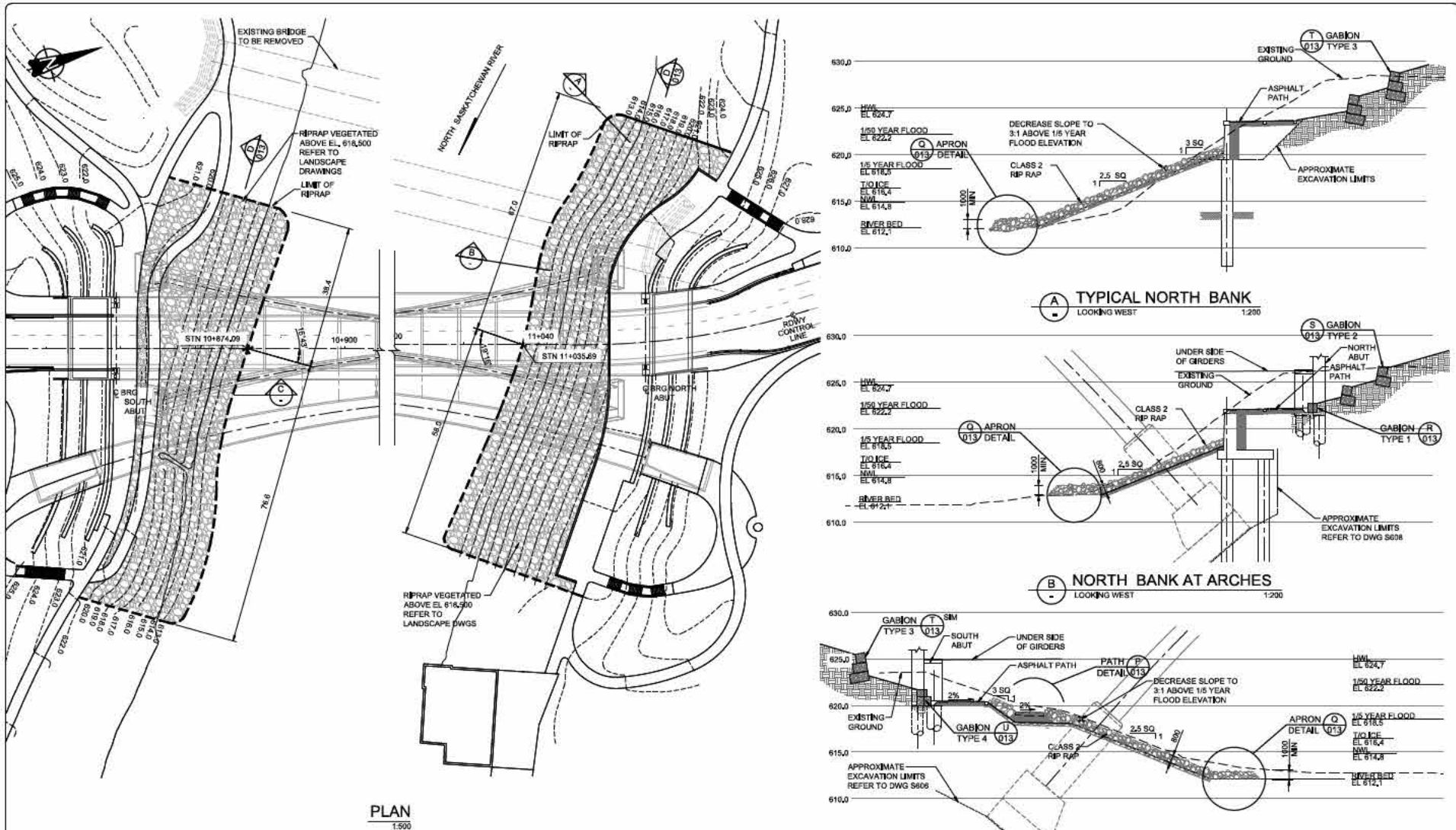
CONSTRUCTION RETURN	
DESIGNER	
CHECKER	
APPROVED FOR CONSTRUCTION	

DESIGNER	
CHECKER	
APPROVED FOR CONSTRUCTION	

DESIGNER	
CHECKER	
APPROVED FOR CONSTRUCTION	

DATE		BY	

TRANSPORTATION SERVICES DEPARTMENT
 ROAD DESIGN AND CONSTRUCTION BRANCH
WALTERDALE BRIDGE
 OVER THE NORTH SASKATCHEWAN RIVER
 WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
 EXISTING SITE PLAN
WALT 131 S005



NOTE:
 1. FOR GENERAL NOTES REFER TO DWG S002 TO S004
 2. REFER TO LANDSCAPE DWGS FOR PATH AND GABION WALL LAYOUT INFORMATION

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PROGRAM NO.	12-66-1466
CONTRACT NO.	1331
CONSTRUCTION RETURN	
CONTRACTOR	
SURVEYOR	
DATE	
REVISIONS	
ISSUED FOR TENDER	
BY	
DATE	
APPROVED FOR CONSTRUCTION	
DATE	



PERMIT TO PRACTICE
 ISL Engineering and Services Ltd.
 Signature: [Signature]
 Date: [Date]
 Incorporated in Alberta, Canada
 Approved for Construction

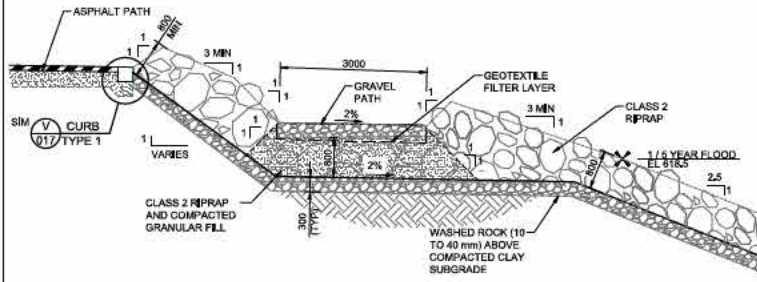


DESIGNER	DATE
CHECKER	DATE
NO. OF REVISIONS	DATE
REVISION	DATE
DATE	DATE
AS NOTED	DATE
DATE	DATE
DATE	DATE

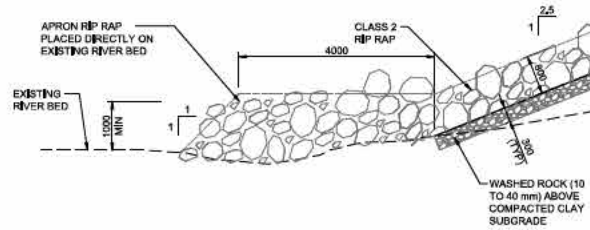
Edmonton TRANSPORTATION SERVICES
 ROAD DESIGN AND CONSTRUCTION DIVISION

WALTERDALE BRIDGE REPLACEMENT
 OVER THE NORTH SASKATCHEWAN RIVER
 WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
SLOPE PROTECTION

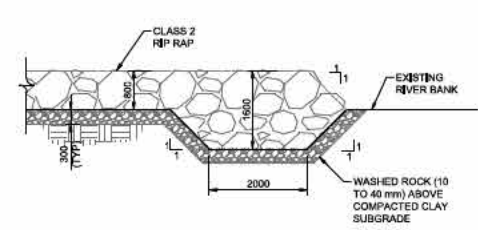
WALT 131 S012



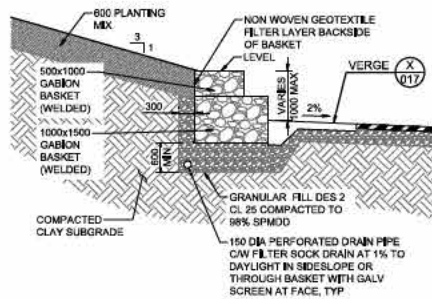
P PATH DETAIL
1:50



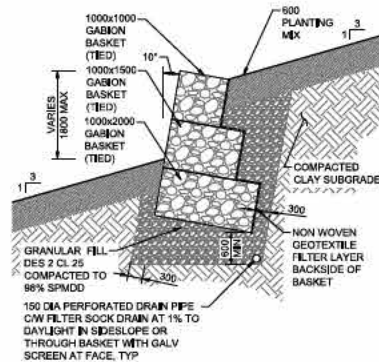
Q APRON DETAIL
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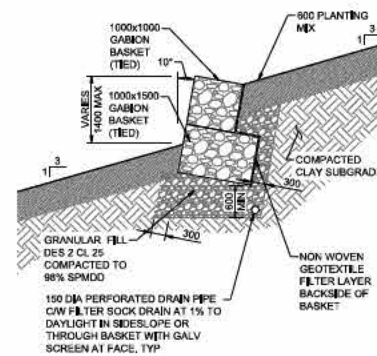
D UPSTREAM EDGE
1:50



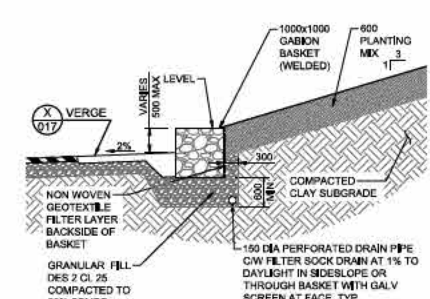
U GABION WALL - TYPE 4
1:50



T GABION WALL - TYPE 3
1:50



S GABION WALL - TYPE 2
1:50

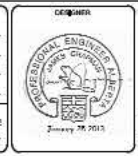


R GABION WALL - TYPE 1
1:50

NOTE:
1. FOR GENERAL NOTES REFER TO DWG S002 TO S004
2. REFER TO LANDSCAPE DWGS FOR INFORMATION ON GABION BASKET ROCK FILL
3. REFER TO LANDSCAPE DWGS FOR PLANTING MIX AND REQUIREMENTS FOR ORGANIC MIX IN CLAY SUBGRADE

1	ISSUED FOR TENDER	JL	JK	JL
2	REVISIONS	BY	DATE	APPROVED

PROGRAM NO.	12-66-1466
CONTRACT NO.	1331
CONSTRUCTION RETURN	
CONTRACTOR	
SURVEYOR	
DATE	
REVISIONS	
CONSTRUCTION PERFORMANCE DATE	
TERMINAL REPORT DATE	



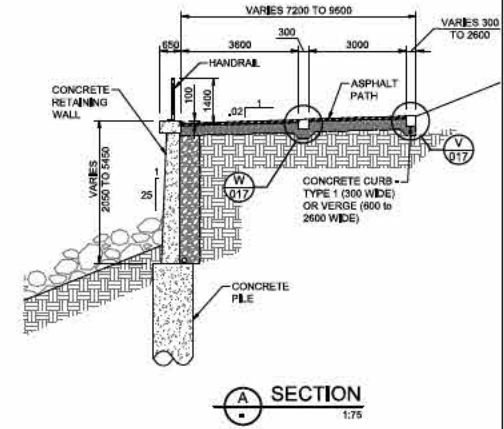
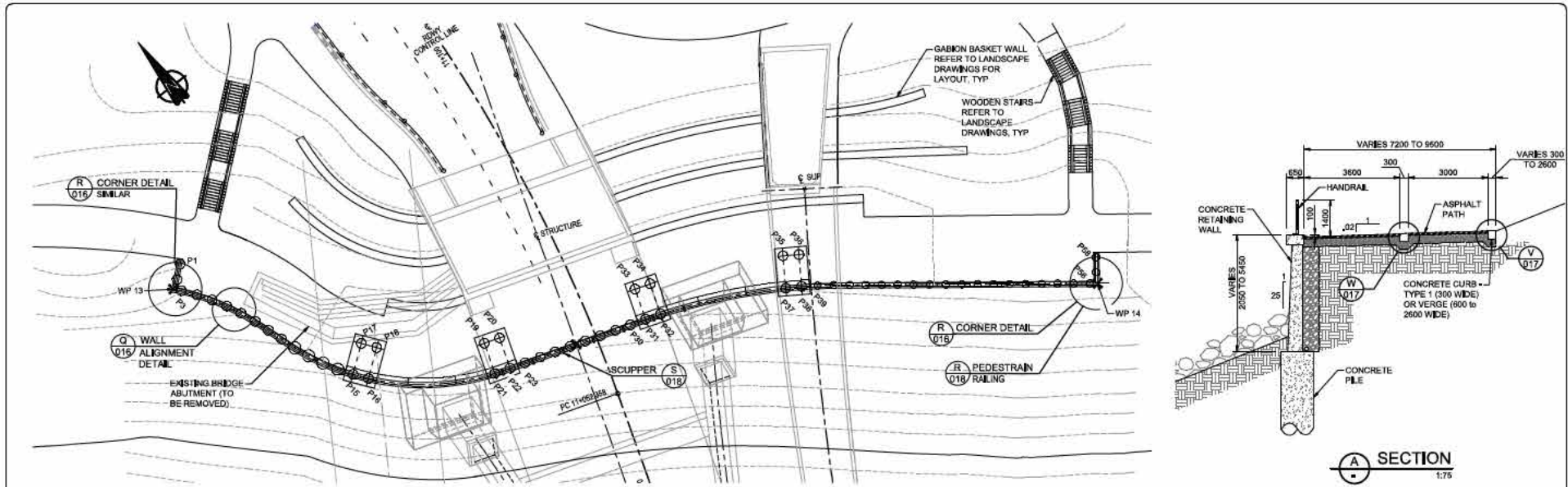
PERMIT TO PRACTICE
ISI Engineering and Services Ltd.
Signature: _____
Date: _____
Professional Engineer
No. 123456789
Approved for Construction



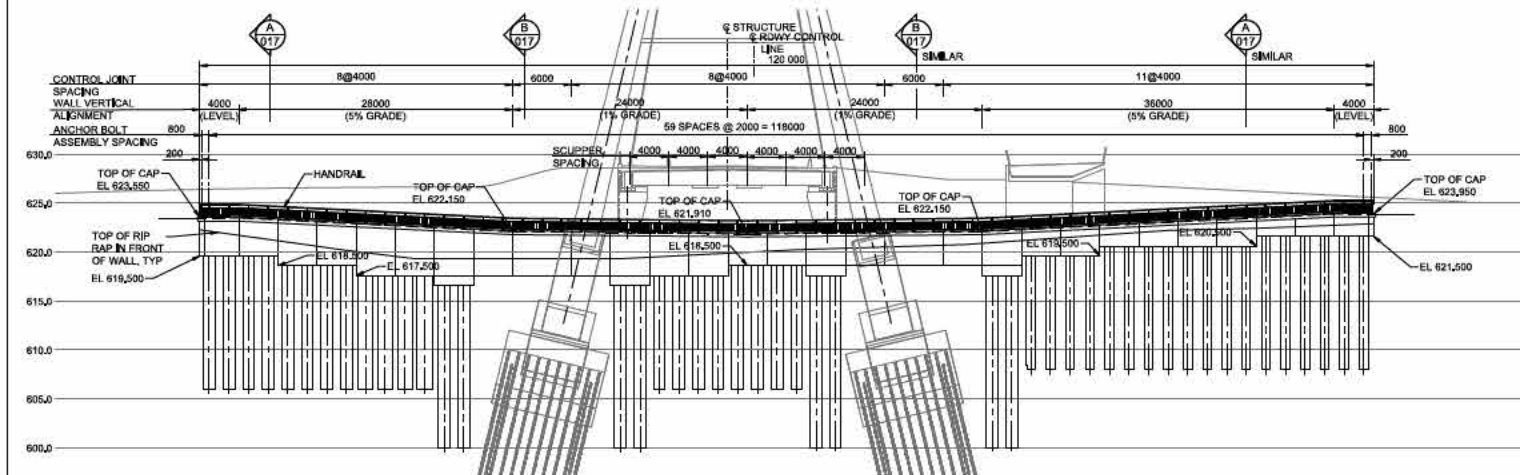
ISL Engineering and Services
DIALOG
BUCKLAND & TAYLOR
AL-TERRA

DATE	2013/06/11
DATE	2013/06/11
DATE	2013/06/11
DATE	2013/06/11

Edmonton TRANSPORTATION SERVICES
WALTERDALE BRIDGE REPLACEMENT
OVER THE NORTH SASKATCHEWAN RIVER
WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
SLOPE PROTECTION DETAILS
WALT 131 S013



WALL PLAN
1:250



WALL ELEVATION
(DEVELOPED VIEW ALONG Q OF WALL) 1:250

NOTE:
1. FOR GENERAL NOTES REFER TO DWG S002 TO S004
2. CONTRACTOR TO BE TRAINED BY MANUKAL ON INSTALLATION OF ANCHORS

1	ISSUED FOR TENDER	JC	JC	JC
2	REVISIONS	BY	DATE	APPROVED

PROGRAM NO.	12-66-1466
CONTRACT NO.	1331
1	ISSUED
2	ISSUED
3	ISSUED
4	ISSUED
5	ISSUED
6	ISSUED
7	ISSUED
8	ISSUED
9	ISSUED
10	ISSUED

CONSTRUCTION RETURN	DESIGNER
CONTRACTOR	PERMIT TO PRACTICE
SURVEYOR	DATE
DATE	FILE NUMBER
FILE NUMBER	CONSTRUCTION/ENGINEER DATE
GENERAL SUPERVISOR DATE	



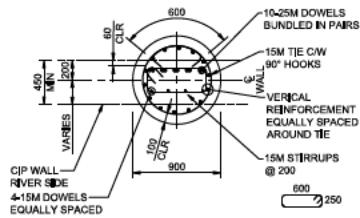
PERMIT TO PRACTICE
ISI Engineering and Services Ltd.
Signature: [Signature]
Date: [Date]
Professional Engineer
The Association of Professional Engineers and Geoscientists of Alberta
APPROVED FOR CONSTRUCTION



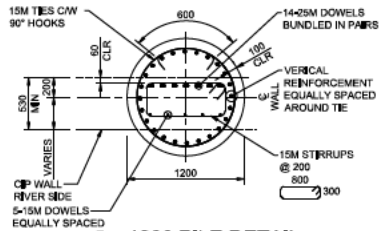
ISL Engineering and Services
BUCKLAND & TAYLOR
a COWI company
DIALOG
AL-TERRA

DESIGNER	DATE
NUMBER OF REVISIONS AND DATE	DATE
REVISION	DATE
DATE	DATE
DATE	DATE
DATE	DATE
DATE	DATE
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DATE	DATE
DATE	DATE

City of Edmonton TRANSPORTATION SERVICES
ROAD DESIGN AND CONSTRUCTION DIVISION
WALTERDALE BRIDGE REPLACEMENT
OVER THE NORTH SASKATCHEWAN RIVER
WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
PROMENADE RETAINING WALL LAYOUT
WALT 131 S014

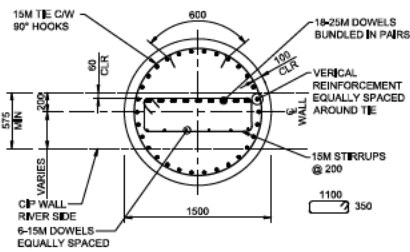


900 PILE SECTION
1:25

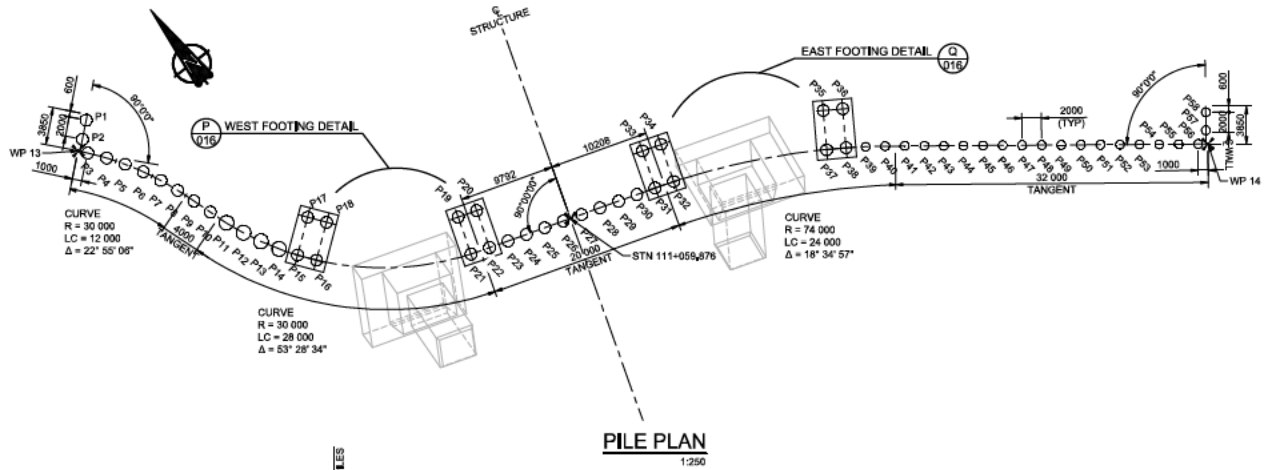


1200 PILE DETAIL
1:25

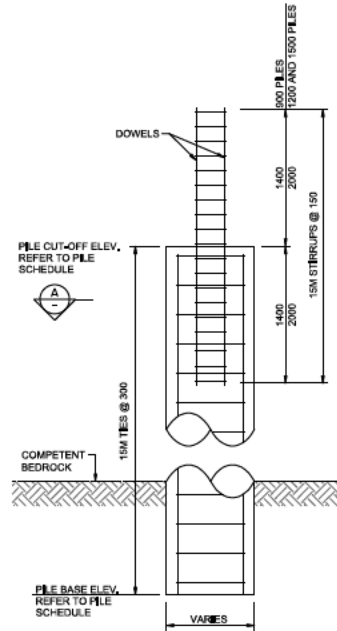
NOTE: REFER TO BS5017 FOR DOWEL REQUIREMENTS FOR PILES P15 TO P22 AND P31 TO P38



1500 PILE DETAIL
1:25



PILE PLAN
1:250



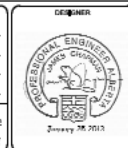
PILE DETAIL
1:25

RETAINING WALL PILE SCHEDULE									
MARK	SHAFT DIA. (mm)	BASE ELEVATION (m)	CUT-OFF ELEVATION (m)	SHAFT VERT. REINF.	MARK	SHAFT DIA. (mm)	BASE ELEVATION (m)	CUT-OFF ELEVATION (m)	SHAFT VERT. REINF.
P1	1200	606,000	619,500	24-30M	P30	1200	606,000	618,500	24-30M
P2	1200	606,000	619,500	24-30M	P31	1200	600,000	617,400	24-30M
P3	1200	606,000	619,500	24-30M	P32	1200	600,000	617,400	24-30M
P4	1200	606,000	619,500	24-30M	P33	1200	600,000	617,400	24-30M
P5	1200	606,000	619,500	24-30M	P34	1200	600,000	617,400	24-30M
P6	1200	606,000	619,500	24-30M	P35	1200	600,000	617,400	24-30M
P7	1200	606,000	618,500	24-30M	P36	1200	600,000	617,400	24-30M
P8	1200	606,000	618,500	24-30M	P37	1200	600,000	617,400	24-30M
P9	1200	606,000	618,500	24-30M	P38	1200	600,000	617,400	24-30M
P10	1200	606,000	618,500	24-30M	P39	900	608,000	619,500	14-30M
P11	1500	606,000	617,500	30-30M	P40	900	608,000	619,500	14-30M
P12	1500	606,000	617,500	30-30M	P41	900	608,000	619,500	14-30M
P13	1500	606,000	617,500	30-30M	P42	900	608,000	619,500	14-30M
P14	1500	606,000	617,500	30-30M	P43	900	608,000	620,500	14-30M
P15	1200	800,000	616,400	24-30M	P44	900	608,000	620,500	14-30M
P16	1200	800,000	616,400	24-30M	P45	900	608,000	620,500	14-30M
P17	1200	800,000	616,400	24-30M	P46	900	608,000	620,500	14-30M
P18	1200	800,000	616,400	24-30M	P47	900	608,000	620,500	14-30M
P19	1200	800,000	616,400	24-30M	P48	900	608,000	620,500	14-30M
P20	1200	800,000	616,400	24-30M	P49	900	608,000	620,500	14-30M
P21	1200	800,000	616,400	24-30M	P50	900	608,000	620,500	14-30M
P22	1200	800,000	616,400	24-30M	P51	900	608,000	621,500	14-30M
P23	1200	806,000	617,500	24-30M	P52	900	608,000	621,500	14-30M
P24	1200	806,000	617,500	24-30M	P53	900	608,000	621,500	14-30M
P25	1200	806,000	617,500	24-30M	P54	900	608,000	621,500	14-30M
P26	1200	806,000	617,500	24-30M	P55	900	608,000	621,500	14-30M
P27	1200	806,000	616,500	24-30M	P56	900	608,000	621,500	14-30M
P28	1200	806,000	616,500	24-30M	P57	900	608,000	621,500	14-30M
P29	1200	806,000	616,500	24-30M	P58	900	608,000	621,500	14-30M

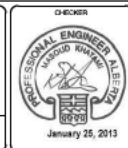
NOTE:
1, FOR GENERAL NOTES REFER TO DWG S002 TO S004

1	ISSUED FOR TENDER	JC	2014/01/13	JC	
2	REVISIONS	BY	DATE	APPRO	

PROGRAM NO.	12-66-1466
CONTRACT NO.	1331
CONSTRUCTION RETURN	
CONTRACTOR	
SURVEYOR	
DATE	
FILE NUMBER	
CONSTRUCTION ENGINEER DATE	
GENERAL SUPERVISOR DATE	



PERMIT TO PRACTICE
ISI Engineering
and Land Services Ltd.
Signature: _____
Date: _____
The Association of Professional Engineers
and Technicians of Alberta



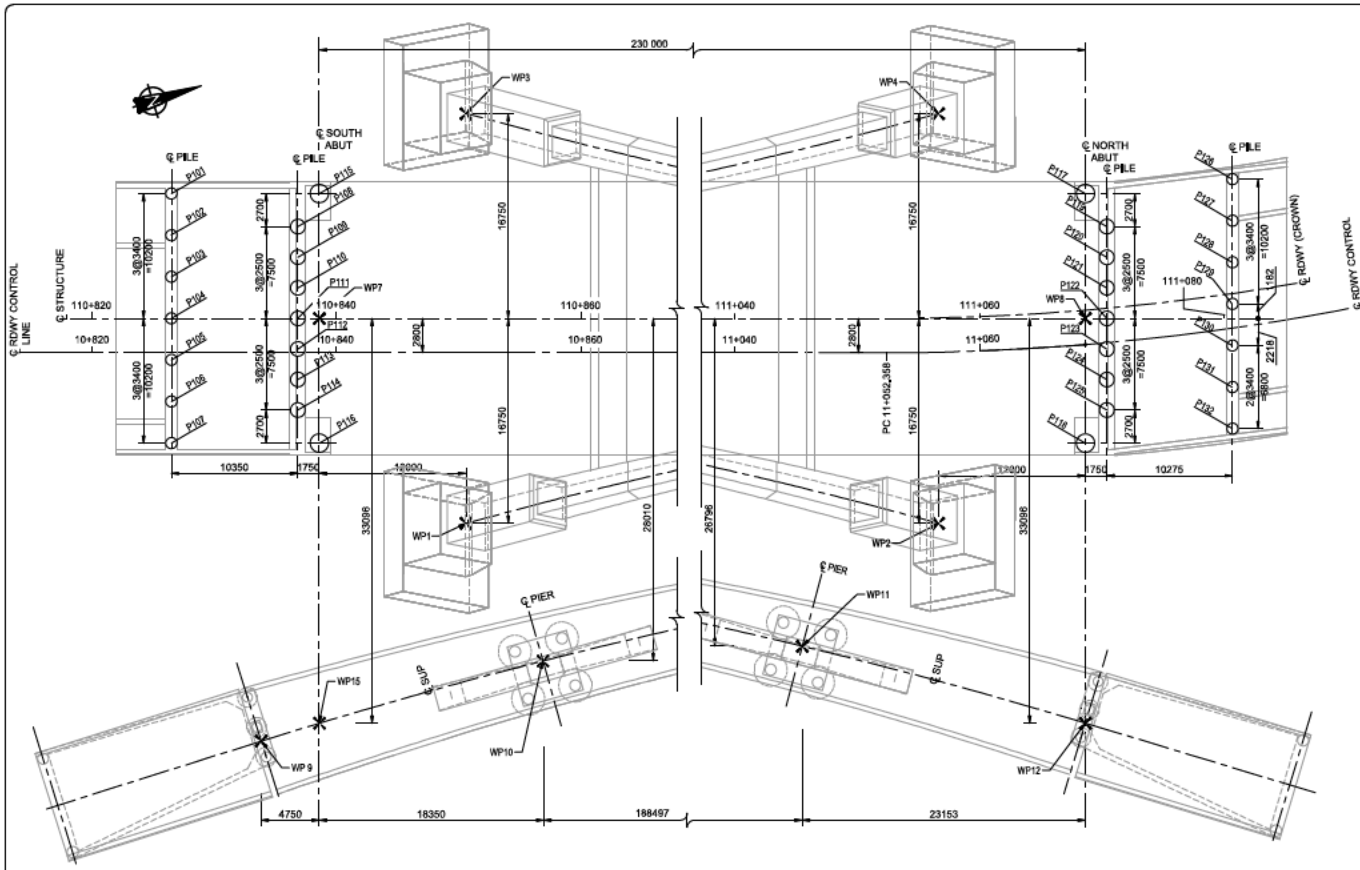
ISL Engineering and Land Services
DIALOG
BUCKLAND & TAYLOR
a COWI company
AL-TERRA

DESIGNER	DATE
CHECKER	DATE
DESIGNED BY	DATE
DESIGNED DATE	DATE
DESIGNED BY	DATE
DESIGNED DATE	DATE

THE CITY OF **Edmonton** TRANSPORTATION SERVICES
ROADS DESIGN AND CONSTRUCTION BRANCH

WALTERDALE BRIDGE REPLACEMENT
OVER THE NORTH SASKATCHEWAN RIVER
WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
PROMENADE RETAINING WALL - FOUNDATIONS

WALT 131 S015

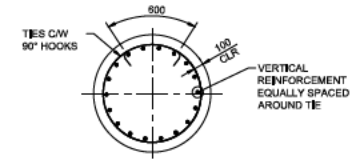


ROAD BRIDGE PILE SCHEDULE						
MARK	SHAFT DIA (mm)	BELL DIA (mm)	BASE ELEVATION (m)	CUT-OFF ELEVATION (m)	SHAFT VERT REINF	TIES
P101	900	-	665,500	624,600	14-25M	15M TIES @ 300
P102	900	-	665,500	624,600	14-25M	15M TIES @ 300
P103	900	-	665,500	624,600	14-25M	15M TIES @ 300
P104	900	-	665,500	624,600	14-25M	15M TIES @ 300
P105	900	-	665,500	624,600	14-25M	15M TIES @ 300
P106	900	-	665,500	624,600	14-25M	15M TIES @ 300
P107	900	-	665,500	624,600	14-25M	15M TIES @ 300
P108	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P109	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P110	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P111	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P112	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P113	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P114	1200	-	662,500	620,000	18-30M	15M TIES @ 300
P115	1500	-	598,000	620,000	26-30M	15M TIES @ 300
P116	1500	-	598,000	620,000	26-30M	15M TIES @ 300
P117	1500	-	662,500	621,500	26-30M	15M TIES @ 300
P118	1500	-	662,500	621,500	26-30M	15M TIES @ 300
P119	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P120	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P121	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P122	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P123	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P124	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P125	1200	-	665,500	621,500	18-30M	15M TIES @ 300
P126	900	-	608,500	626,350	14-25M	15M TIES @ 300
P127	900	-	608,500	626,350	14-25M	15M TIES @ 300
P128	900	-	608,500	626,350	14-25M	15M TIES @ 300
P129	900	-	608,500	626,350	14-25M	15M TIES @ 300
P130	900	-	608,500	626,350	14-25M	15M TIES @ 300
P131	900	-	608,500	626,350	14-25M	15M TIES @ 300
P132	900	-	608,500	626,350	14-25M	15M TIES @ 300

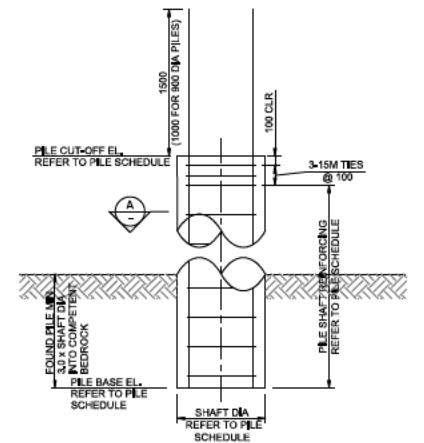
WORK POINTS				
MARK	STATION ON Q STRUCTURE	OFFSET	NORTHING	EASTING
WP1	110 + 850.632	16 750	5932943.527	33027.740
WP2	111 + 056.594	16 750	5933040.260	33088.704
WP3	110 + 850.632	16 750	5932853.441	32995.747
WP4	111 + 056.594	16 750	5933050.174	33056.711
WP5	110 + 953.603	200	5932946.081	33044.708
WP6	110 + 953.603	5400	5932947.621	33039.742
WP7	110 + 838.634	0	5932837.024	33006.192
WP8	111 + 068.561	0	5933056.677	33076.259
WP9	110 + 833.885	34 562	5932822.259	33039.794
WP10	110 + 856.961	28 000	5932946.245	33040.349
WP11	111 + 045.461	26 798	5933026.534	33094.997
WP12	111 + 068.592	33 098	5933046.881	33107.868
WP13	111 + 083.399	45 039	5933084.142	33037.655
WP14	111 + 039.993	63 917	5933015.214	33130.297
WP15	110 + 838.634	33 096	5932827.230	33039.799

FOUNDATION PLAN
1:200

- NOTES:**
1. FOR GENERAL NOTES REFER TO DWG S002 TO S004
 2. OFFSETS ARE HORIZONTAL DIMENSIONS PERPENDICULAR TO Q STRUCTURE AND ARE REFERENCED TO GROUND.
 3. NORTHINGS AND EASTINGS ARE REFERENCED TO GRID AND SCALED ABOUT THE ORIGIN (0,0)
 4. WPS AND WP6 ARE LOCATED AT TOP OF STEEL ARCHES (NOT SHOWN ON THIS DRAWING)
 5. WP13 AND WP14 ARE LOCATED AT THE ENDS OF PROMENADE RETAINING WALL (NOT SHOWN ON THIS DRAWING)
 6. REFER TO THE UTILITIES DWGS FOR EXISTING UTILITIES IN THE VICINITY OF THE NEW BRIDGE CONSTRUCTION



TYPICAL PILE SECTION
1:25



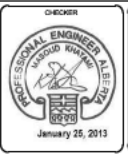
STRAIGHT SHAFT PILE DETAIL
1:25

REV	BY	DATE	APPROVED

PROGRAM NO.	12-66-1466
CONTRACT NO.	1331
CONSTRUCTION RETURN	
CONTRACTOR	
SURVEYOR	
DATE	
BY NUMBER	
CONSTRUCTION/REVISION DATE	
REVISIONS	



PERMIT TO PRACTICE
ISL Engineering and Land Services Ltd.
Signature: _____
Date: _____
The Association of Professional Engineers and Technicians of Alberta
APPROVED FOR CONSTRUCTION



ISL Engineering and Land Services
DIALOG
BUCKLAND & TAYLOR Inc.
a COWI company
AL-TERRA

DESIGNER	DATE
CHECKER	DATE
NUMBER OF PILES DESIGNED AND CONSTRUCTED	DATE
DESIGNED	DATE
APPROVED	DATE

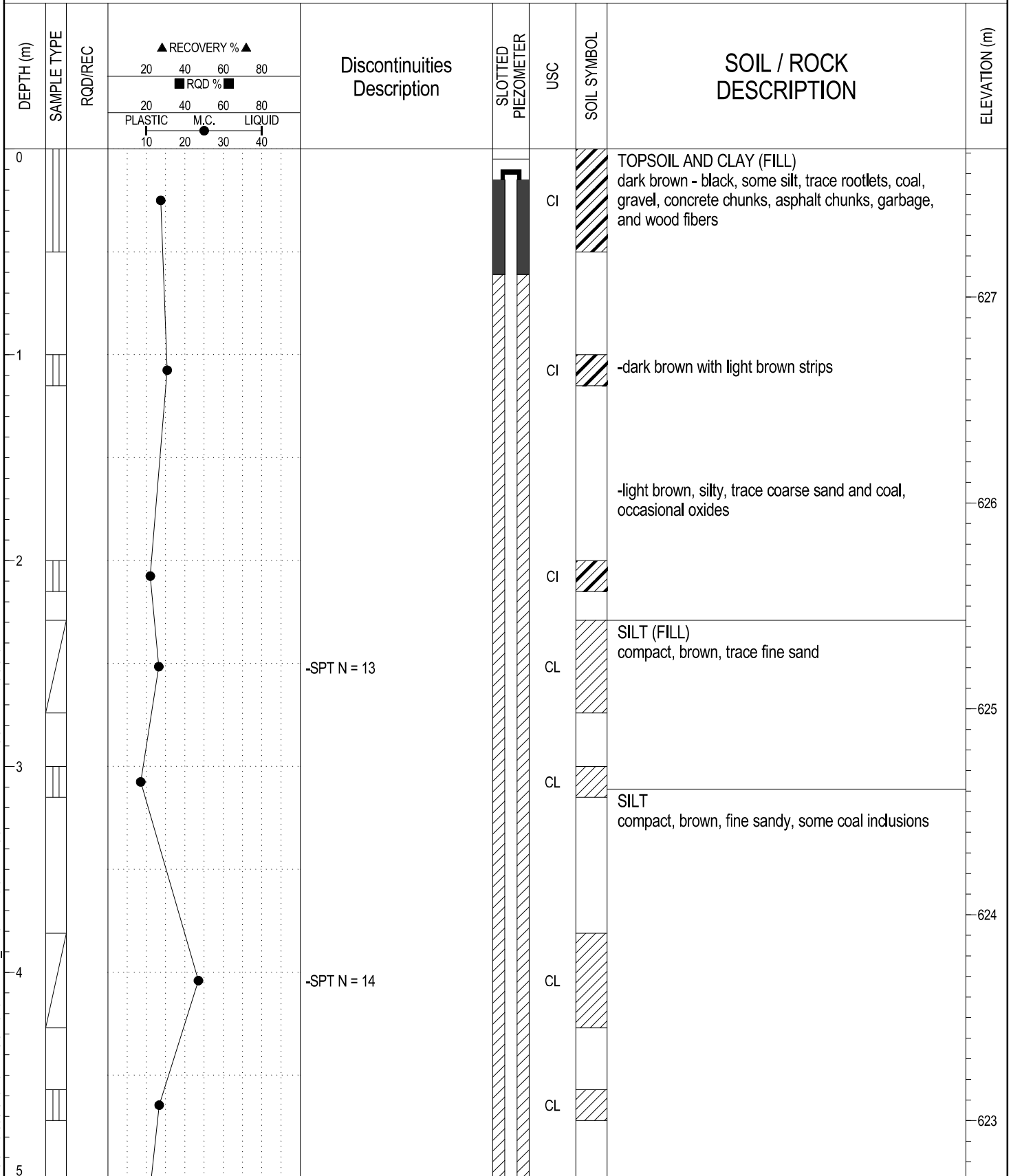
Edmonton TRANSPORTATION SERVICES
ROAD DESIGN AND CONSTRUCTION BRANCH

WALTERDALE BRIDGE REPLACEMENT
OVER THE NORTH SASKATCHEWAN RIVER
WALTERDALE HILL ROAD / QUEEN ELIZABETH PARK ROAD
FOUNDATION LAYOUT - ROAD BRIDGE

WALT 131 S101

CLIENT: ISL ENGINEERING & LAND SERVICES LTD	PROJECT: WALTERDALE BRIDGE REPLACEMENT	BOREHOLE NO: TH12-14
DRILLING COMPANY: Mobile Augers & Research Ltd.	DATE DRILLED: July 4 to 6, 2012	PROJECT NO: 19-598-370
DRILL/METHOD: M11 XLT / Solid Stem Augers	LOCATION: N5933098.849, E33044.779	ELEVATION: 627.720 (m)

SAMPLE TYPE	<input type="checkbox"/> GRAB SAMPLE	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> DRILL CUTTINGS	



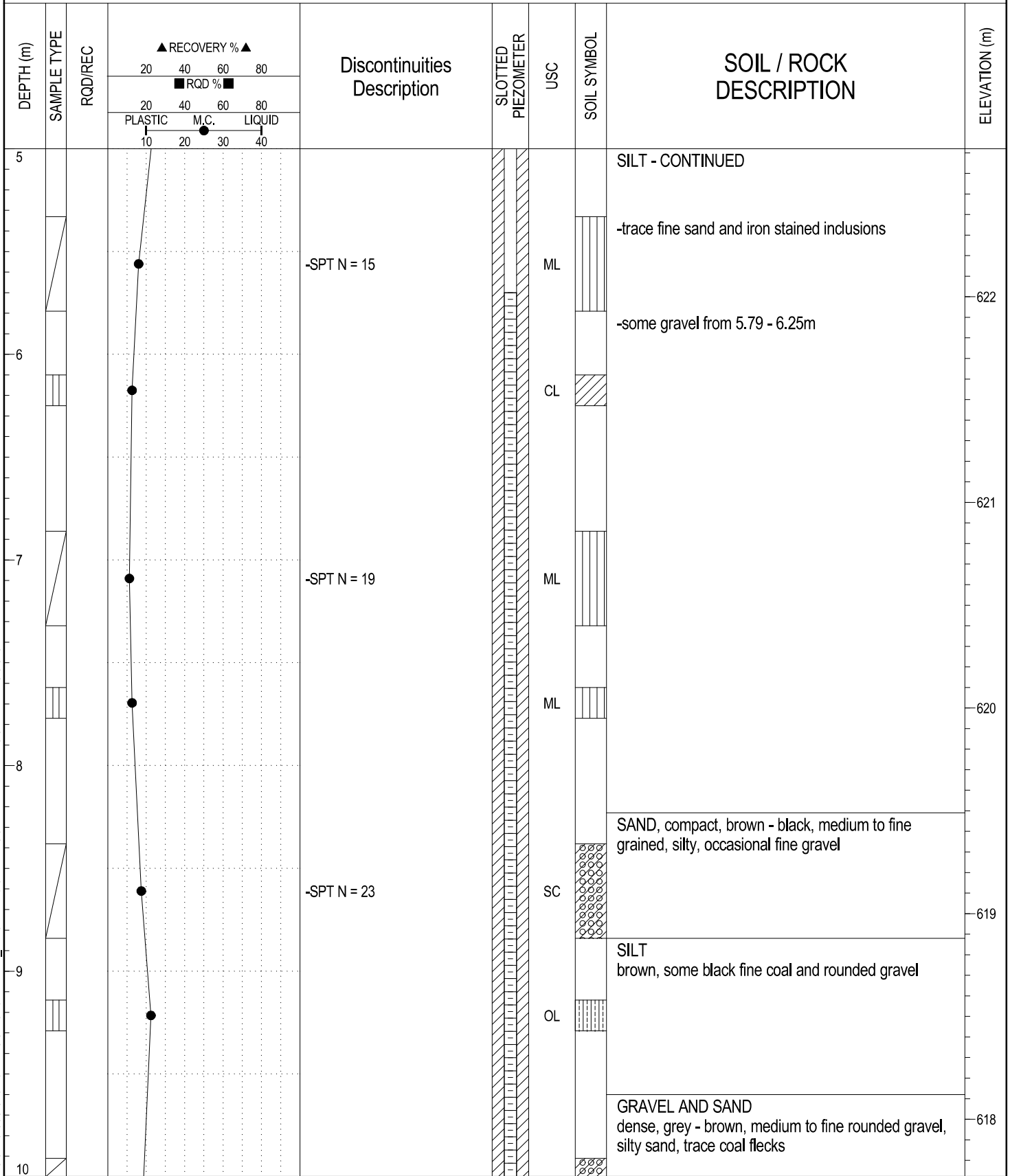
BOREHOLE LOG 19-598-370-2012-ROCK.GPJ_THRBR_AB.GDT_12/4/12_REGULAR_LIBRARY-ROCK-NEW_LOGO.GLB



FIELD LOGGED BY: AKL / TDC	COMPLETION DEPTH: 24.5 m
PREPARED BY: XW	COMPLETION DATE: 7/6/12
REVIEWED BY: HER	

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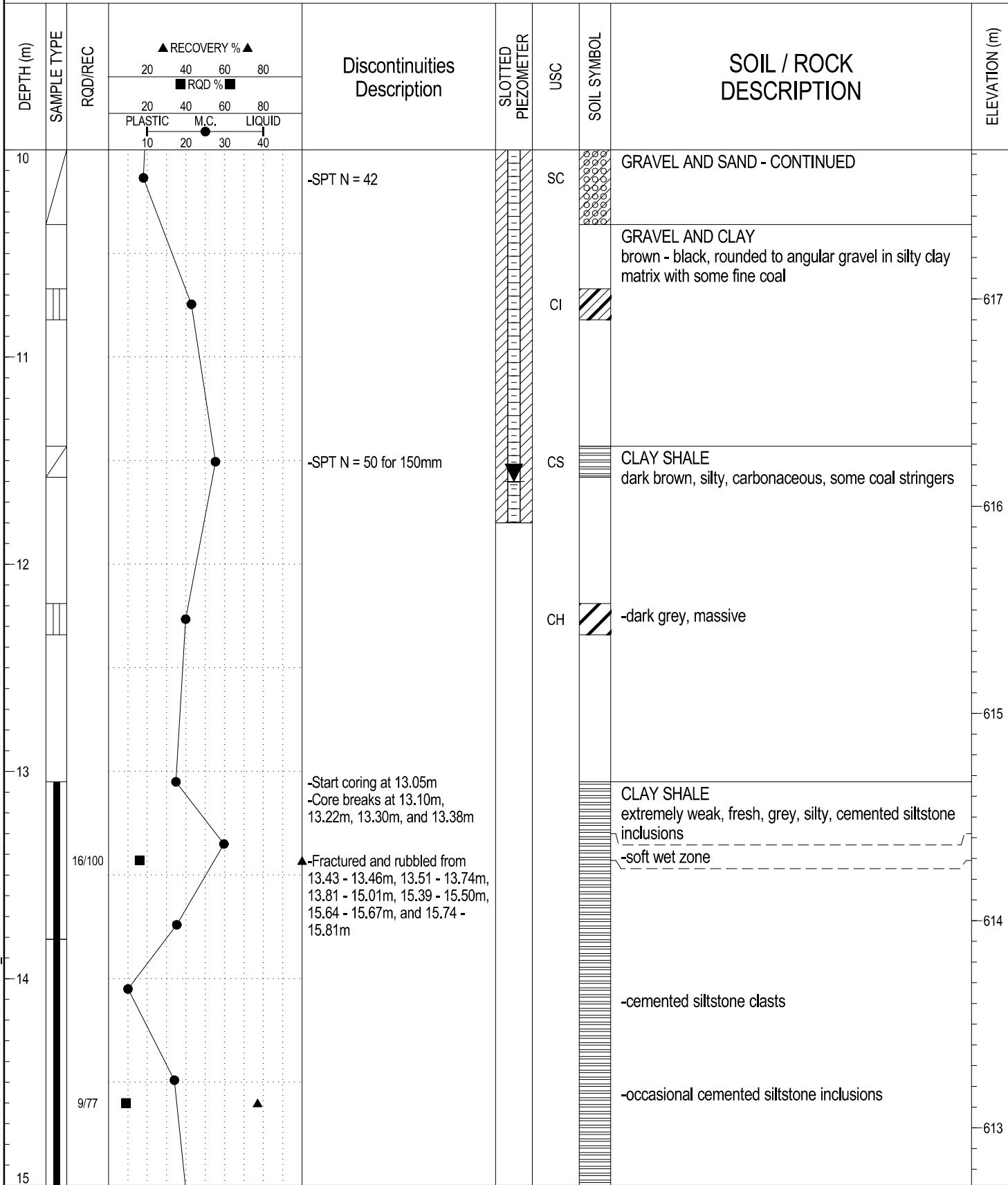
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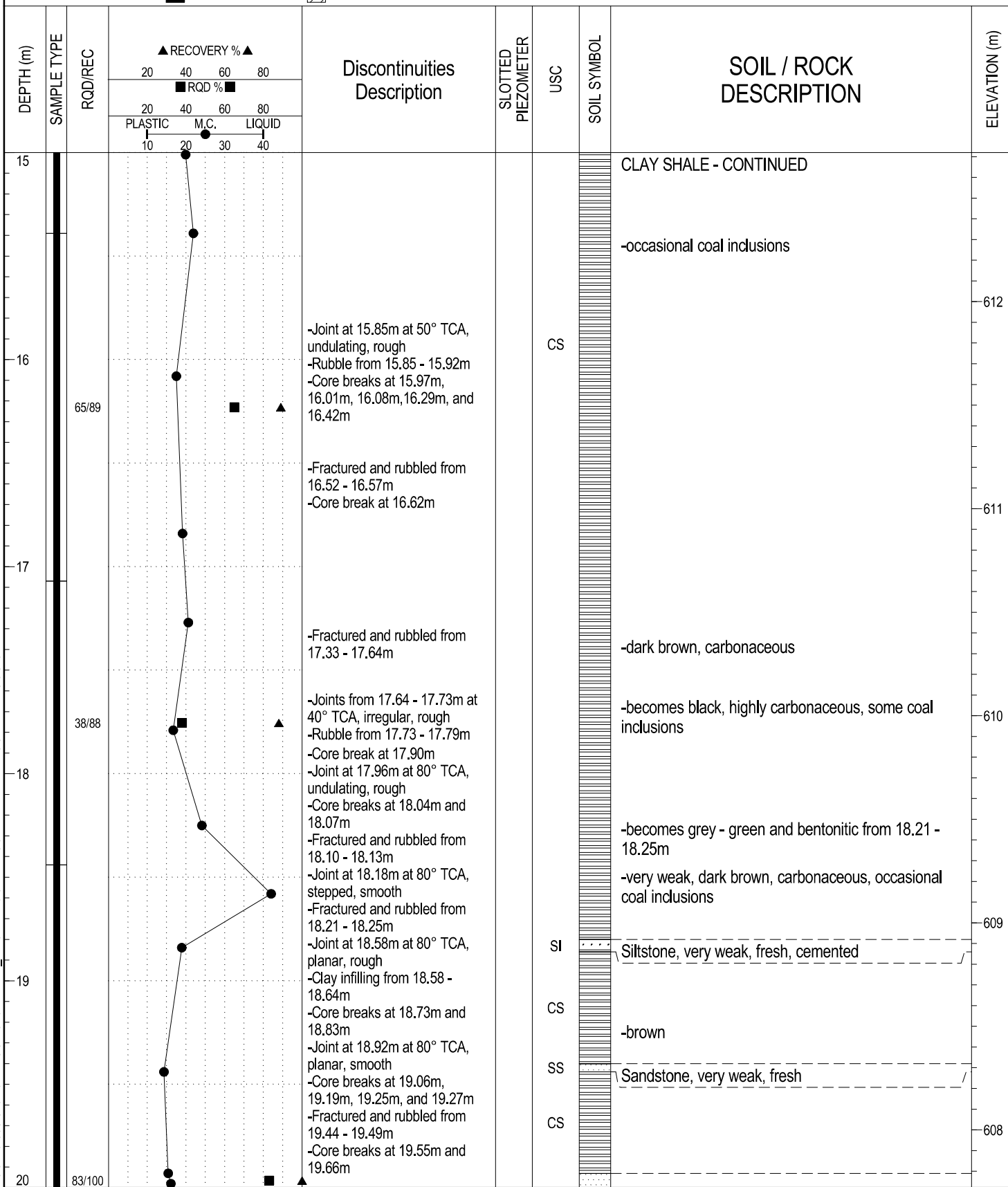
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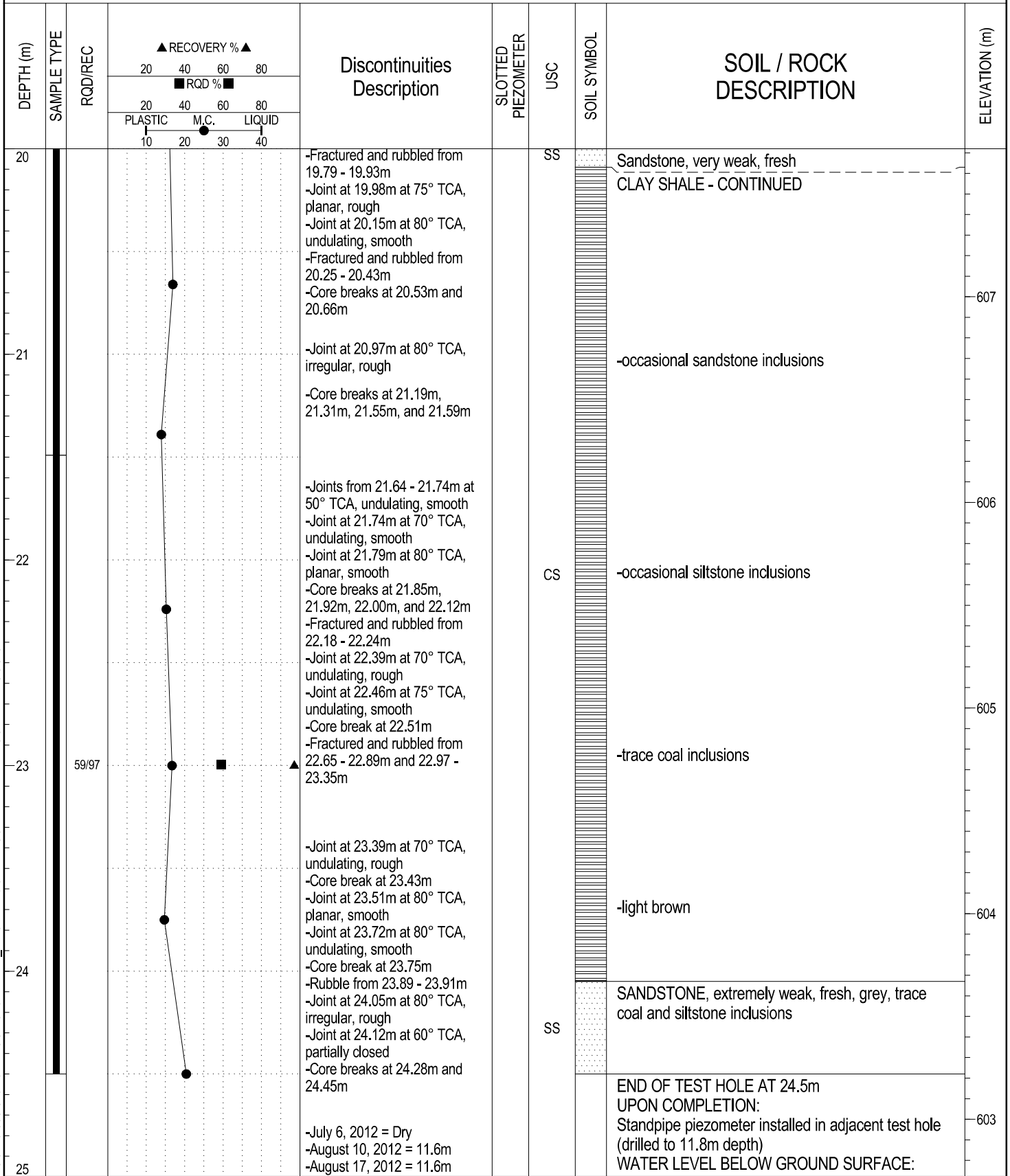
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BOREHOLE LOG 19-598-370-2012-ROCK.GPJ_THRBR_AB.GDT_12/4/12_REGULAR_LIBRARY-ROCK-NEW_LOGO.GLB



Location of Additional Retaining Wall West of Legislature Power Plant









